

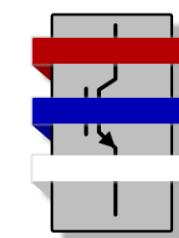
The logo for TAL TECH, featuring the words "TAL" in white and "TECH" in blue, stacked vertically.

EMERGING POWER CONVERTERS TOPOLOGIES FOR DC BUILDINGS APPLICATION

Tutorial 3



Centre of Excellence
in Energy Efficiency



International
Conference on
DC Microgrids

TUTORIAL 3: INSTRUCTORS



Edivan Laercio Carvalho (Senior Member, IEEE), received the B.Sc. and M.Sc. degrees in electrical engineering from the Federal University of Technology – Paraná (UTFPR), Brazil, in 2015, and 2018, respectively, and the Ph.D. degree in electrical engineering from Federal University of Santa Maria (UFSM), Brazil. He is currently a Researcher with the Power Electronics Group, Tallinn University of Technology. His research interests include high-frequency DC-DC power converter topologies, net-zero energy buildings, grid-connected converters, and power management systems.



Sachin Chauhan (Member, IEEE) received the B.Tech. degree in electrical and electronics engineering from Dr. A. P. J. Abdul Kalam Technical University, Lucknow, India, in 2014, the M.Tech. degree in power electronics and drives from Madan Mohan Malaviya University Of Technology, Gorakhpur, India, in 2017, and the Ph.D. degree in electrical engineering from the Indian Institute of Technology Mandi, Mandi, India, in 2023. He is currently a Postdoctoral Researcher with the Power Electronics Group, Tallinn University of Technology, Tallinn, Estonia. His research interests include the new topologies, control, and modulation of DC-DC power converters for electric vehicle, wireless power transfer, and renewable energy integration applications.



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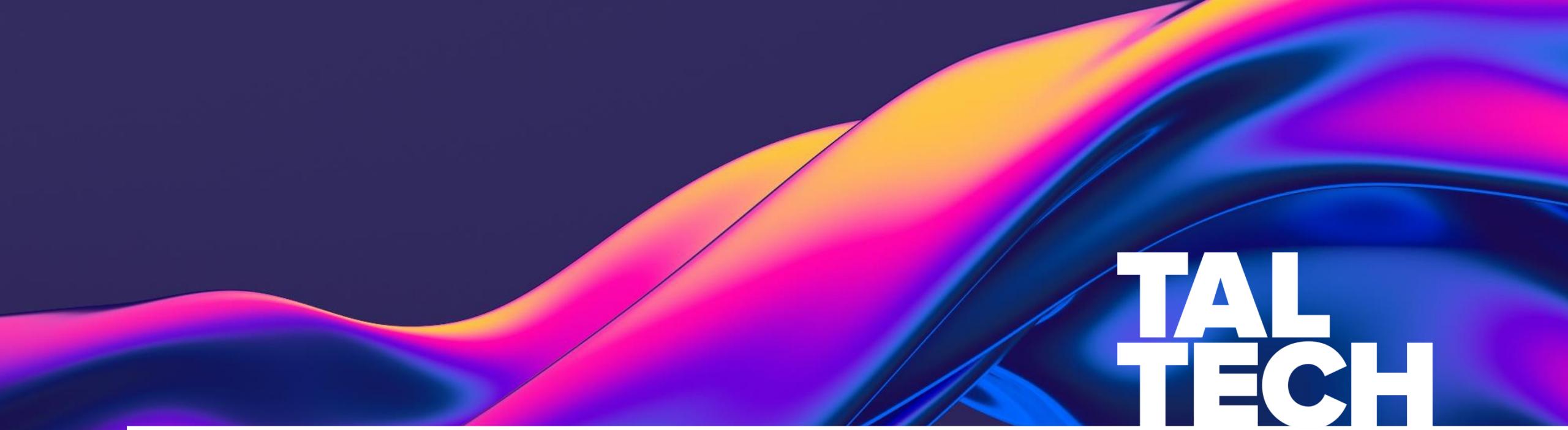
Niwton Gabriel Feliciani dos Santos (Member, IEEE) was born in Rosário do Sul, Brazil, in 1995. He received the B.S. degree (Hons.) in electrical engineering from the Federal University of Pampa, Alegrete, Brazil, in 2018, and both the M.S. and Ph.D. degrees in electrical engineering from the Federal University of Santa Maria, Santa Maria, Brazil, in 2020 and 2024, respectively. He is currently a Postdoctoral Researcher with the Power Electronics Group, Tallinn University of Technology, Tallinn, Estonia. His current research interests include active and nonactive power processing, dc-dc conversion systems, partial power converters, battery chargers for electric vehicles (EVs), and photovoltaic (PV) systems.



i³ DC
Accelerates Energy Transition



Centre of Excellence
in Energy Efficiency



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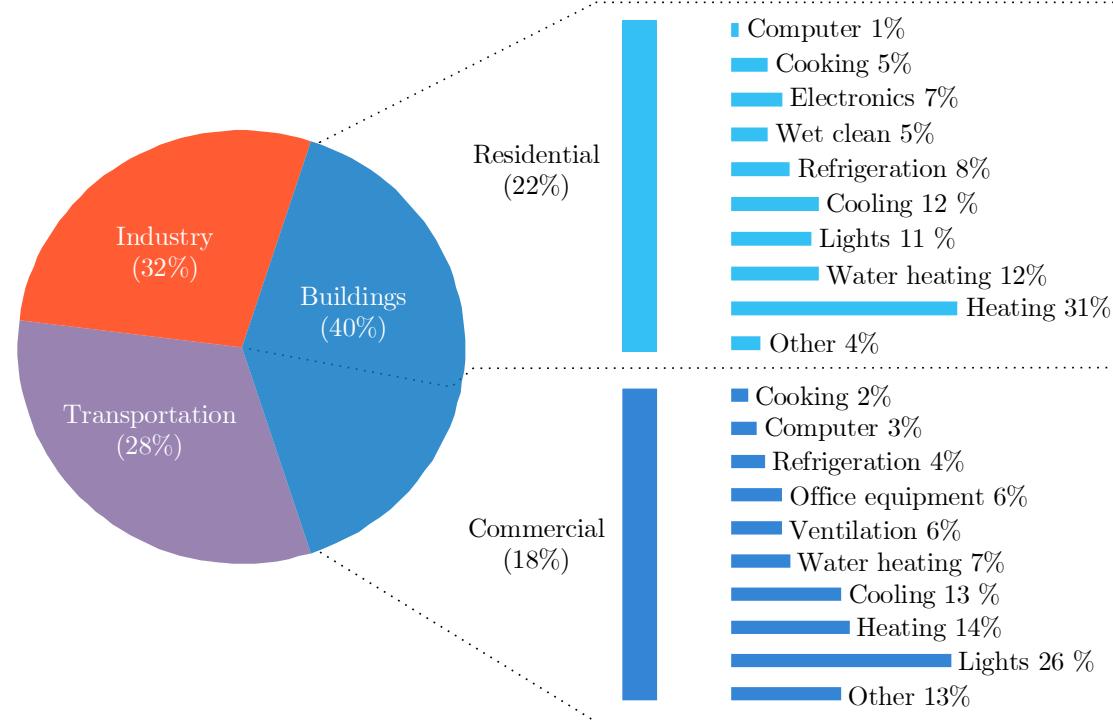
INTRODUCTION, STANDARDS, AND REQUIREMENTS FOR RESIDENTIAL DC ELECTRICAL INSTALLATIONS

Tutorial 3



ENERGY EFFICIENCY OF BUILDINGS: AN ISSUE

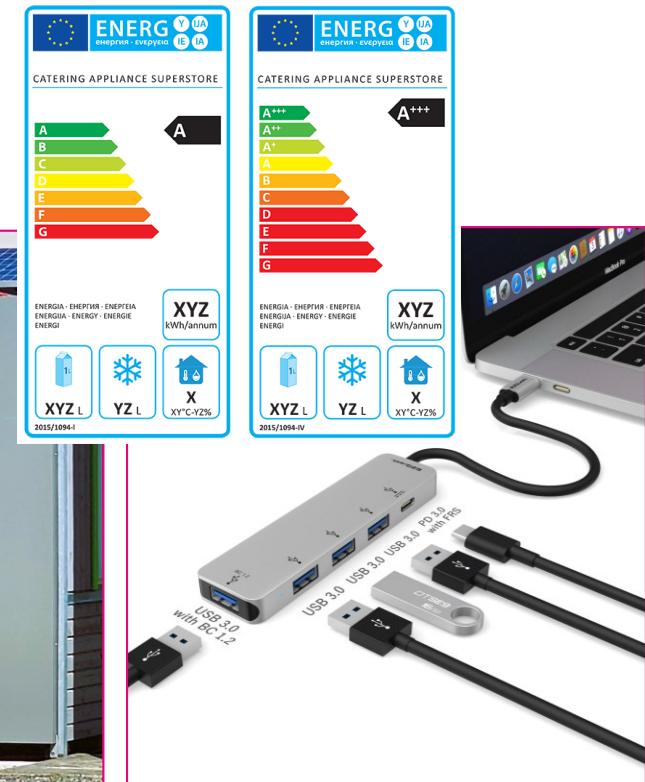
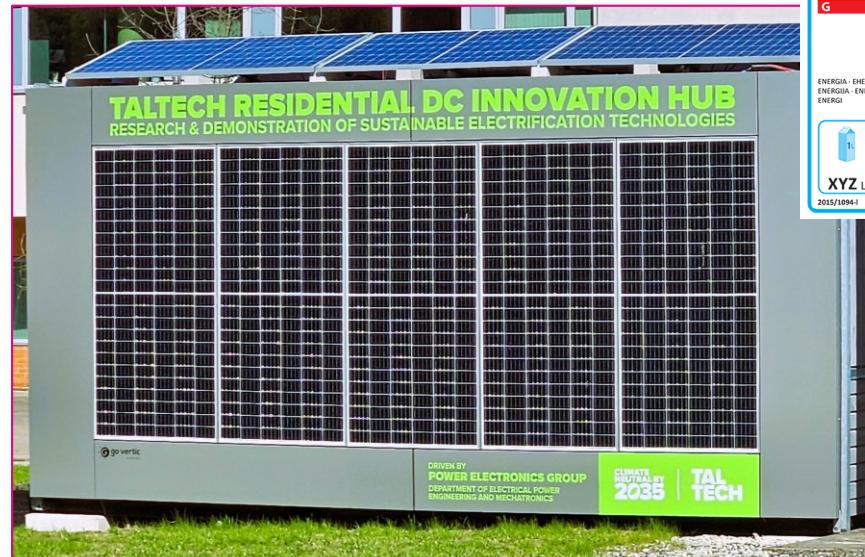
- Buildings consume (and waste!!!) too much energy:
 - Annual energy consumption in Estonia 33...34 TWh/y
 - Share of buildings 50% (w/o industrial buildings)
 - EU average 40%
- Currently, roughly 75% of buildings in the EU are not energy efficient:
 - 85–95% of today's buildings will still be in use in 2050
- To boost decarbonization the EU requires all new buildings from 2021 to be nearly zero-energy buildings (NZEB)
- NZEB (or class A building) :
 - fully covered by energy from renewable sources and without on-site carbon emissions from fossil fuels



NEARLY ZERO-ENERGY BUILDINGS TODAY

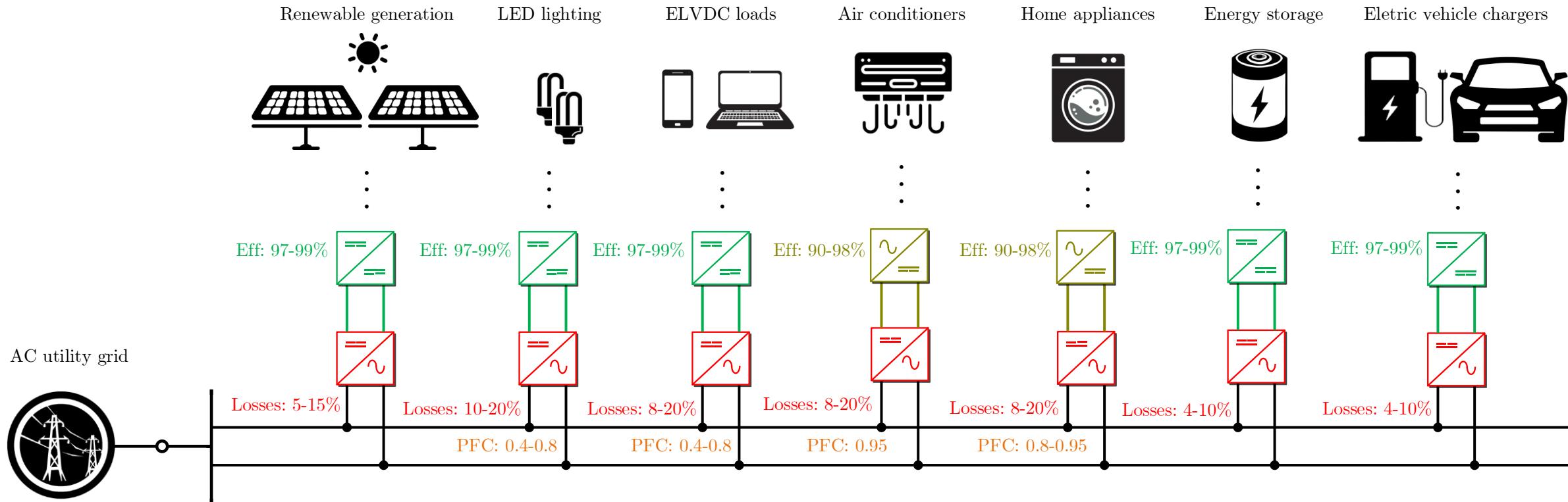


- In practice, NZEB consumes up to 4 times less energy than the traditional ones
- Energy efficiency is the main feature of ZEB - PV installation (backed up with energy storage), heat pump, heat recovery ventilation, energy-efficient appliances and lighting, smart control of loads
- NZEB:
 - High energy performance (low energy consumption)
 - Local renewable generation
 - Most of energy saving technologies are based on power electronics



POWER ELECTRONICS FOR AC-BASED NZEB TODAY

- AC is rectified in every appliance, reducing efficiency, reliability, and power factor
- Power factor is an issue



POWER ELECTRONICS FOR AC-BASED NZEB TODAY



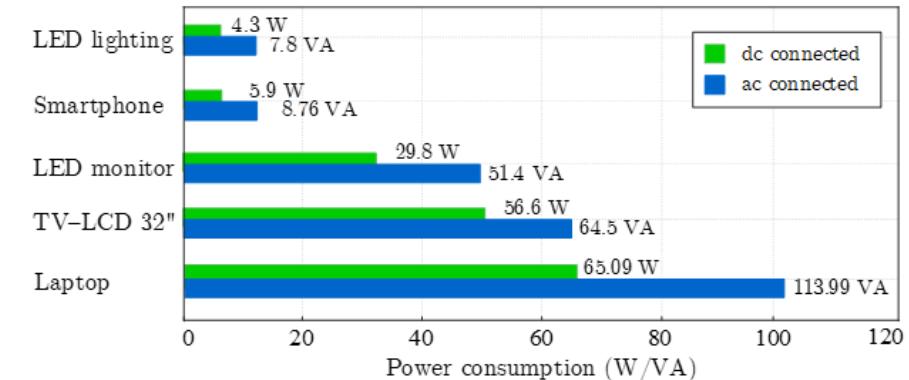
- Power Factor Correction (PFC) is required only above 75 W, and the energy efficiency is further affected by a non-unity power factor
- Cumulative energy waste could become significant, even in installations where low-power devices are dominant



1	Urms	232.37	V
2	Irms	0.5766	A
3	P	65.09	W
4	S	133.99	VA
5	Q	117.12	var
6	Uthd	1.122	%
7	Ithd	86.841	%
8	PF	0.4858	
9	Udc	19.243	V
10	Idc	-3.022	A
11	P	-58.16	W

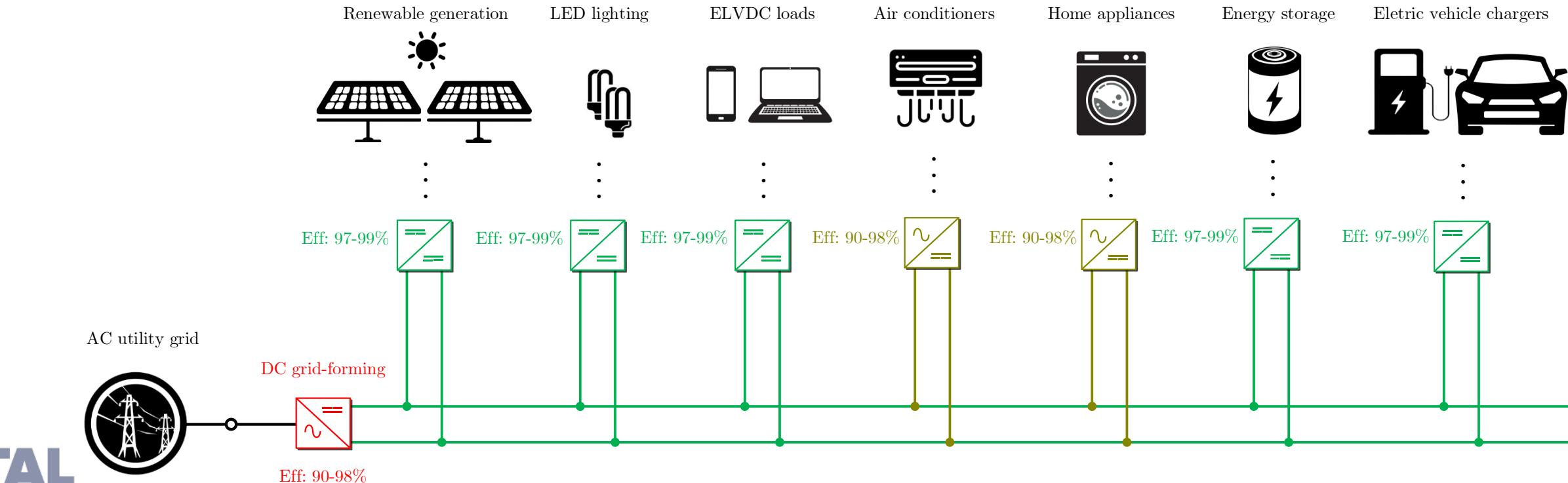
MEASURED POWER FACTOR FOR DIFFERENT HOME APPLIANCES

Appliance	Measured power factor	Power consumption
LED light bulb	0.5534	7.82 VA
Smartphone charger	0.5814	8.76 VA
LED monitor	0.5797	51.4 VA
TV – LCD 32"	0.8775	64.5 VA
Laptop Charger	0.4858	113.99 VA



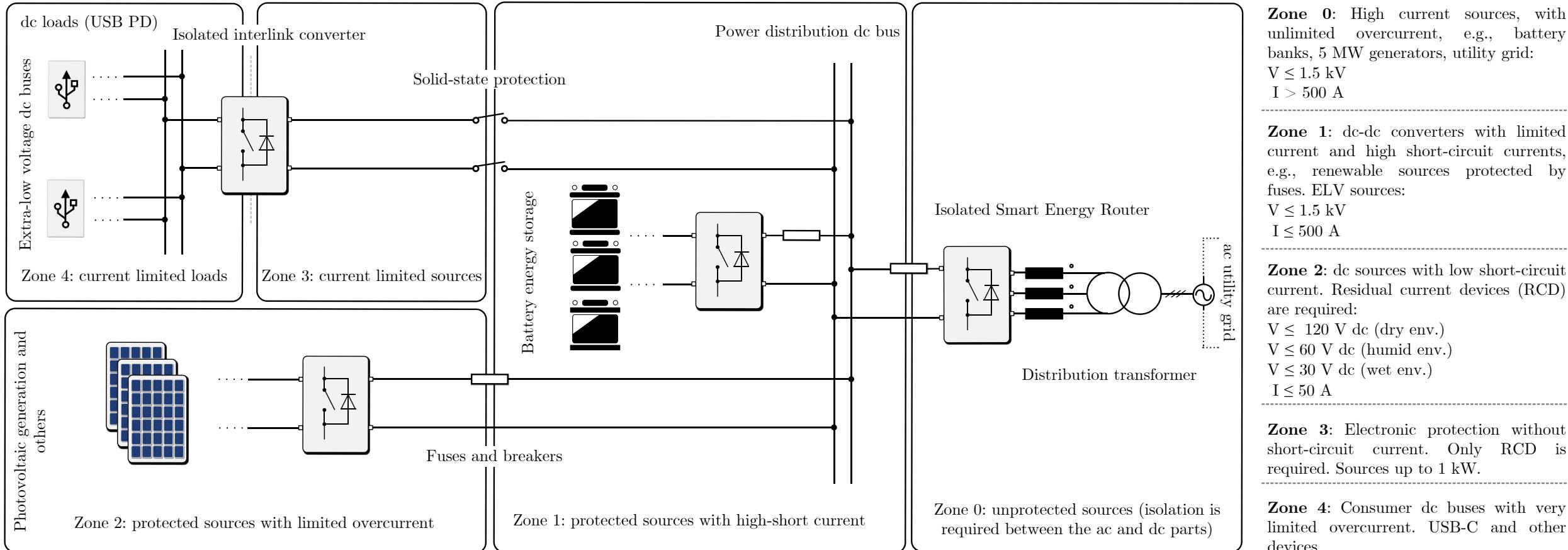
DC-POWERED BUILDINGS: THE NEXT-GENERATION OF NZEB

- Increased efficiency and **maximized self-consumption** of renewable energy due to the less energy conversion stages (DC can save up to 30 % of energy waste)
- No reactive power** – only active energy is delivered
- Simple coordination and control, better resilience, and energy security (**droop control based**)



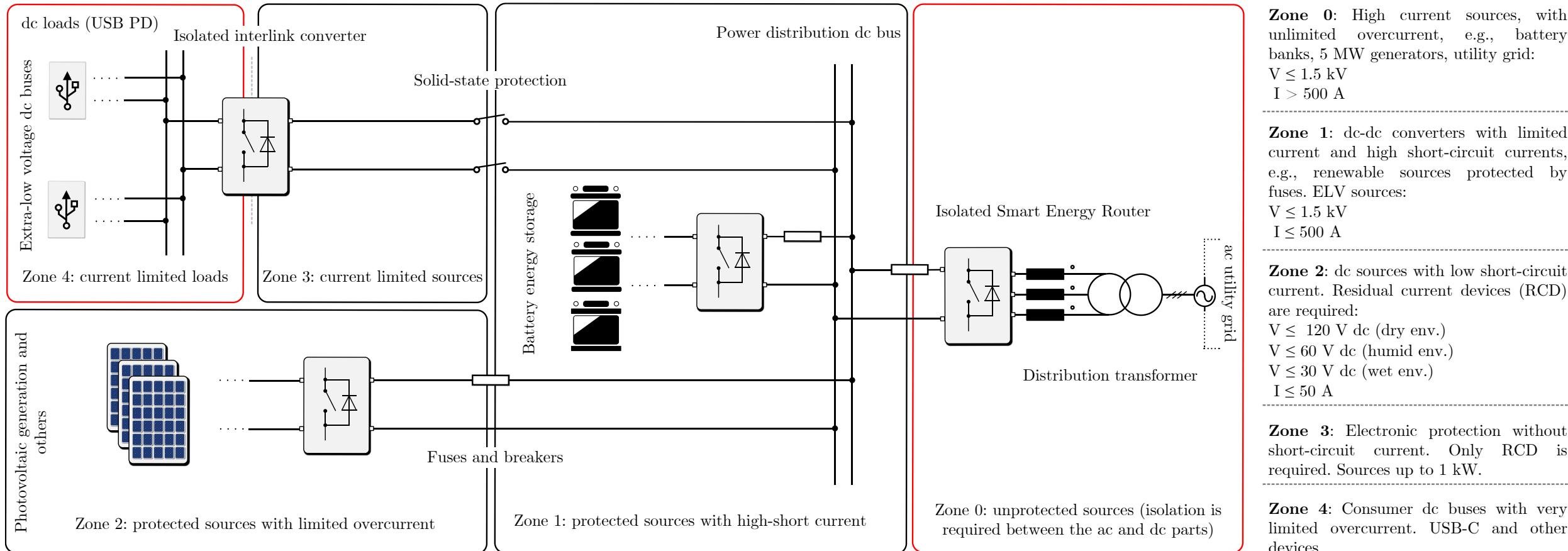
MAIN INITIATIVES TOWARDS DC

- Current/OS Foundation: protocols under development
- NPR9090: first national practice guidelines for DC (2018)



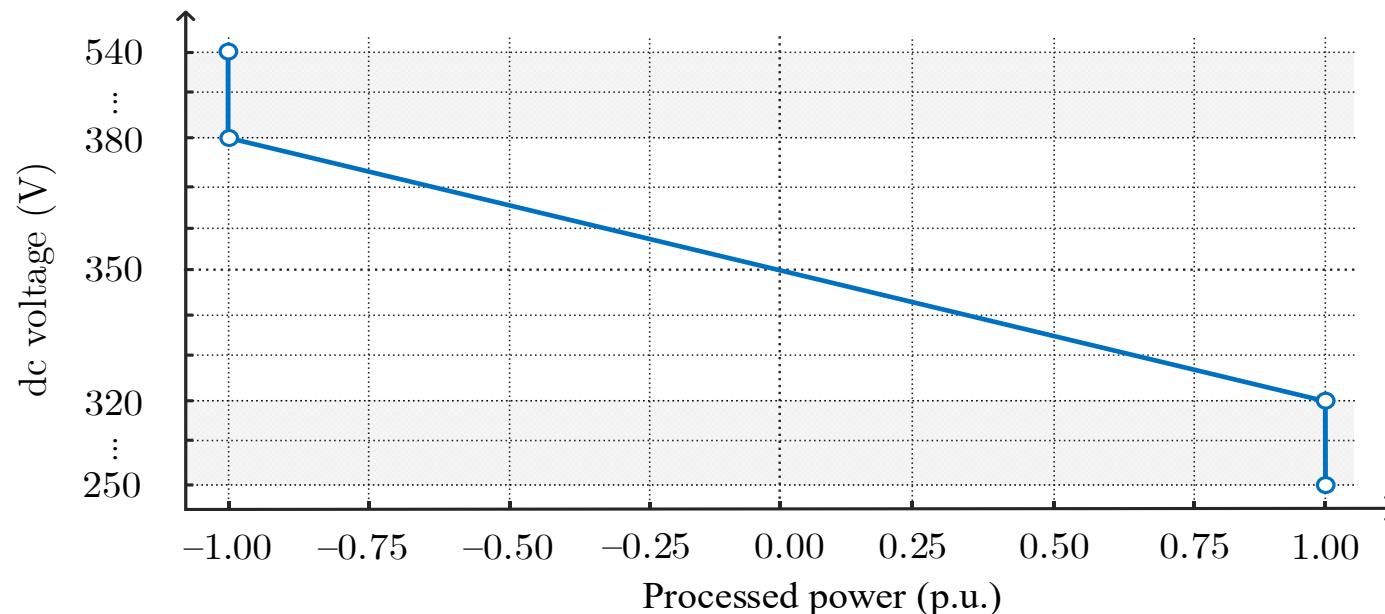
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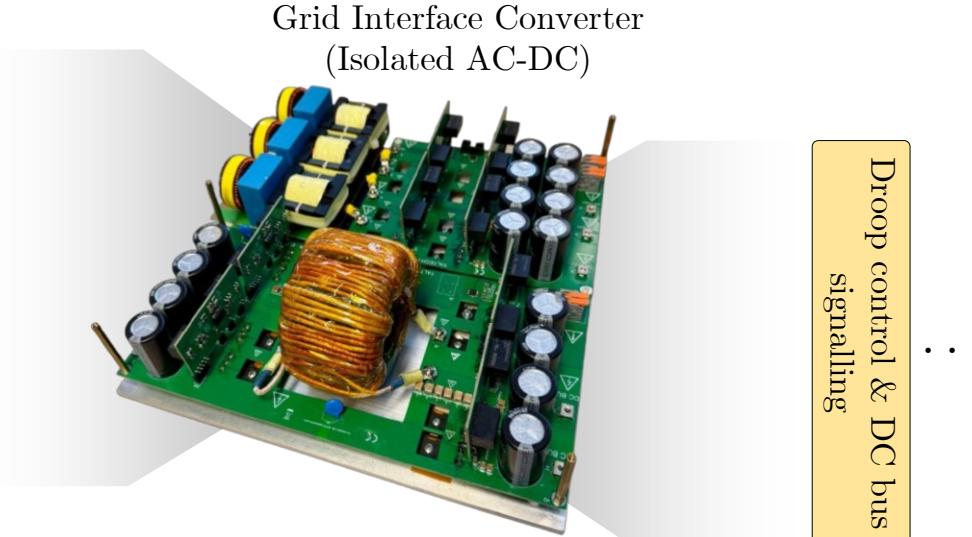
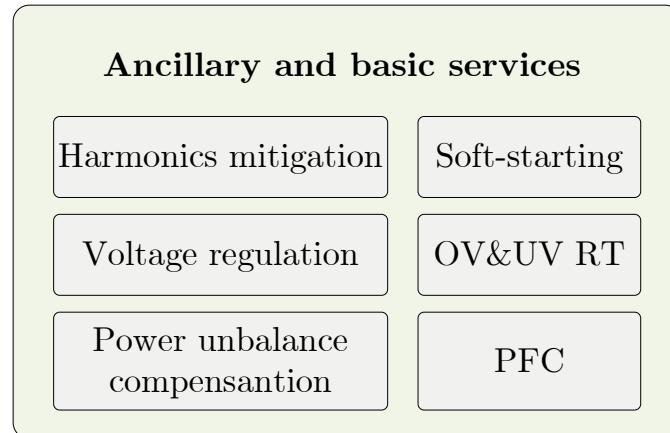
VOLTAGE LEVELS ACCORDING TO CURRENT/OS

- Voltage levels and bands are selected according to the application
 - Industrial-scale: $640 - 760 \text{ } V_{dc}$
 - Building scale: $320 - 380 \text{ } V_{dc}$
 - ELVDC: $24 - 57 \text{ } V_{dc}$
- **Droop control** is essential to ensure **compatibility** between different sources and loads



INTERLINKING CONVERTERS (GRID-INTERFACE)

- Enabling technology for DC microgrids: operates as a DC grid-forming converter
- Provides **galvanic isolation** (between AC and DC parts)
- Bidirectional power transfer – improved management to **increase self-consumption**
- Droop control operation – easy **compatibility** with DERs and loads
- Ancillary services **for both**, AC and DC grids



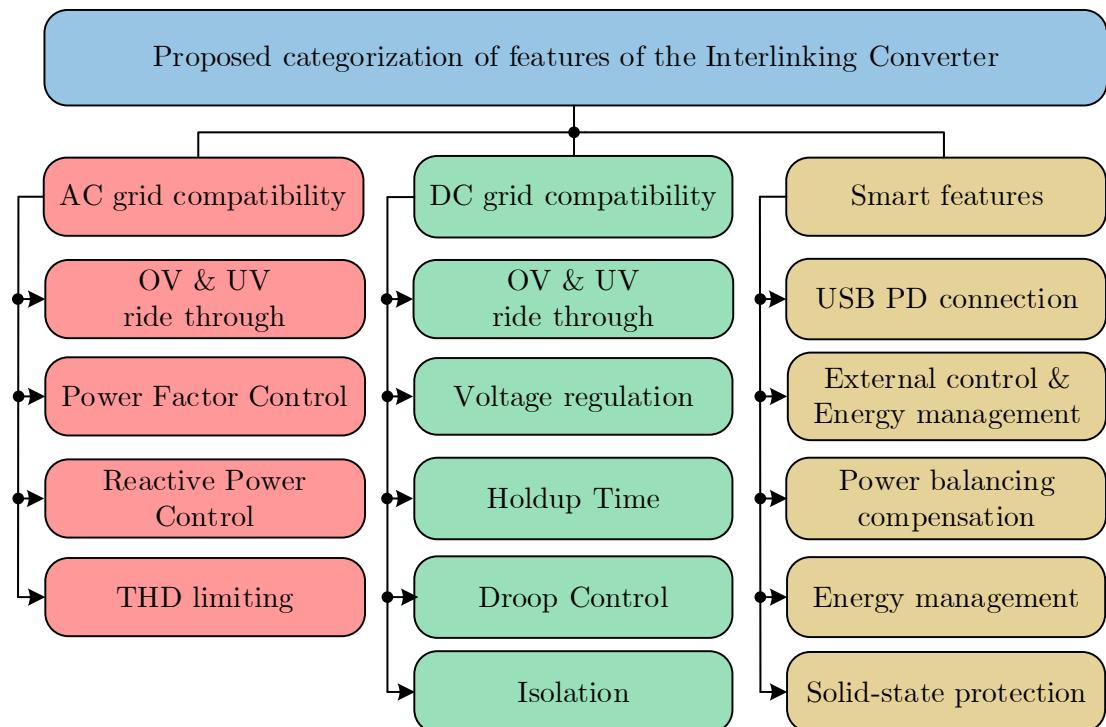
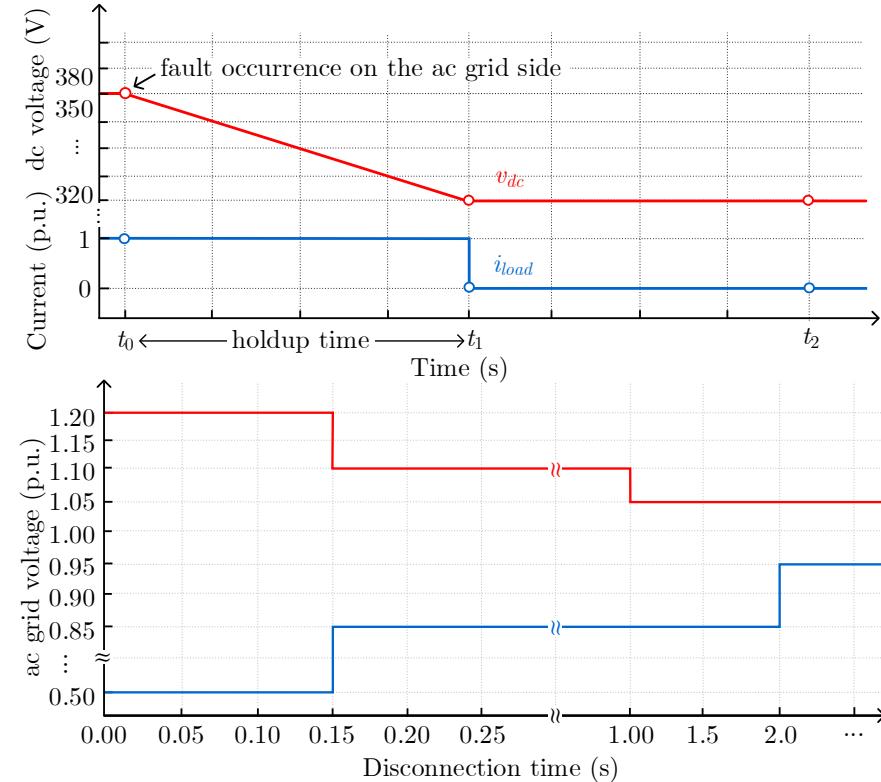
Droop control & DC bus signalling

How many new fuctionalities whould be needed for DC?

How can a proper and optimized device be designed to implement such functions?

STANDARDIZATION RELATED TO INTERLINKING CONVERTERS

- Grid-interface/interlinking converters are multifunctional devices
- Main functions should accomplish with both
- Standardization/certification procedures for GIC are complex topic and still an open to be discussed





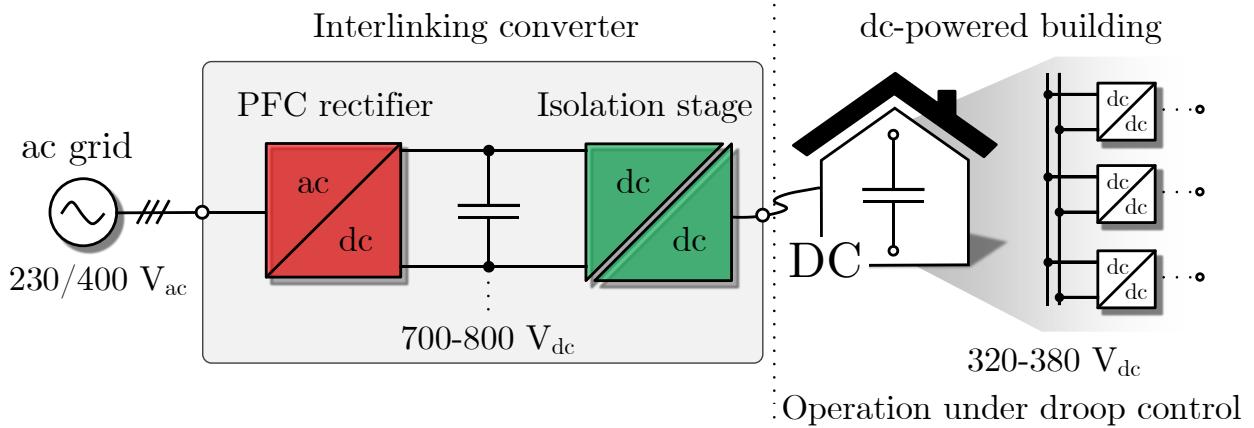
POWER CONVERTER TOPOLOGIES FOR AC-GRID INTEGRATION THE ENABLING TECHNOLOGY FOR DC-POWERED BUILDINGS

Dr. Edivan Laercio Carvalho

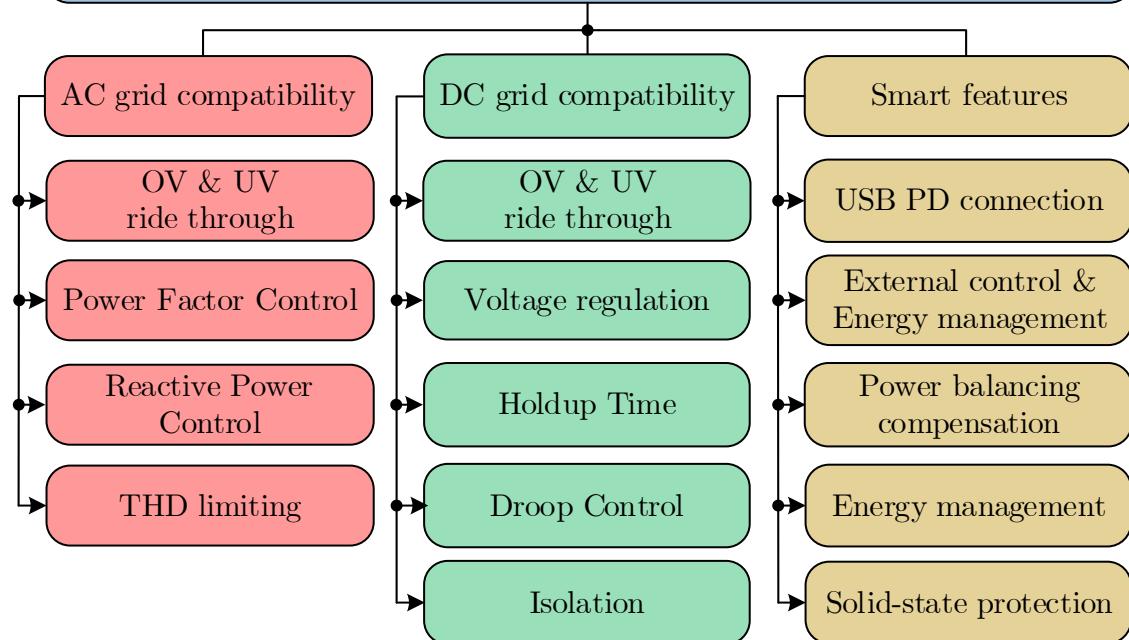


POWER CONVERTERS SOLUTIONS FOR GIC

- Isolated active front-end converter (i-AFE)
- Main function: interlink between AC and DC grids
- Basic topology: AC-DC + DC-DC
- Well-defined roles according to each power processing stage
- Efficiency is the main challenge



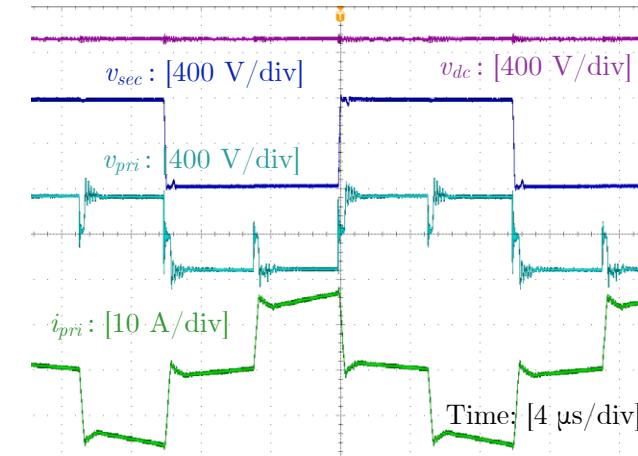
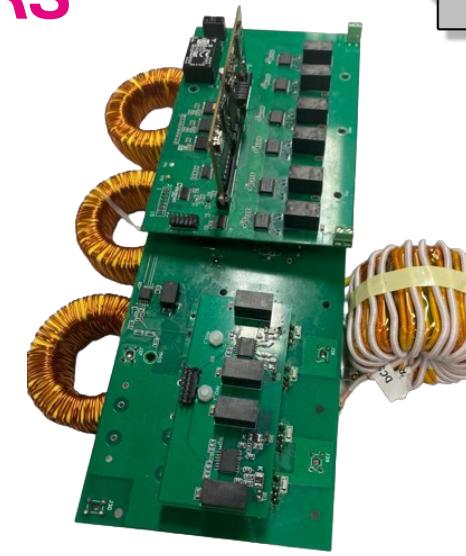
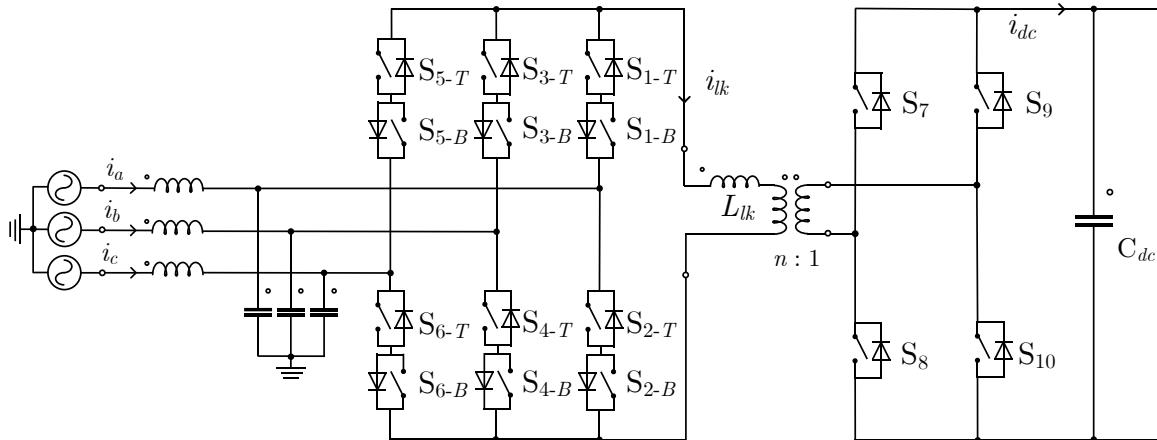
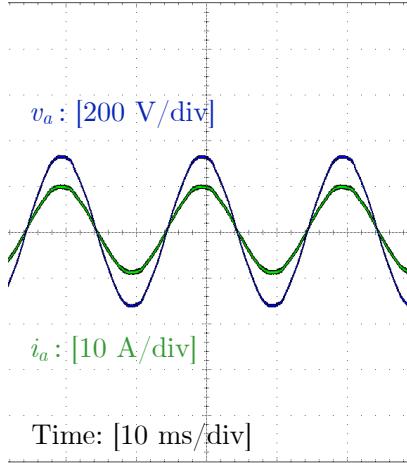
Proposed categorization of features of the Interlinking Converter



POWER CONVERTERS SOLUTIONS FOR GIC

SINGLE-STAGE / MATRIX-BASED CONVERTERS

- Lower number of sensors/feedback loops
- No intermediate dc link
- Complex modulation strategy
- Higher THD (for voltage-fed topologies)
- High efficiency: 96.7 % peak (3.5 kW)

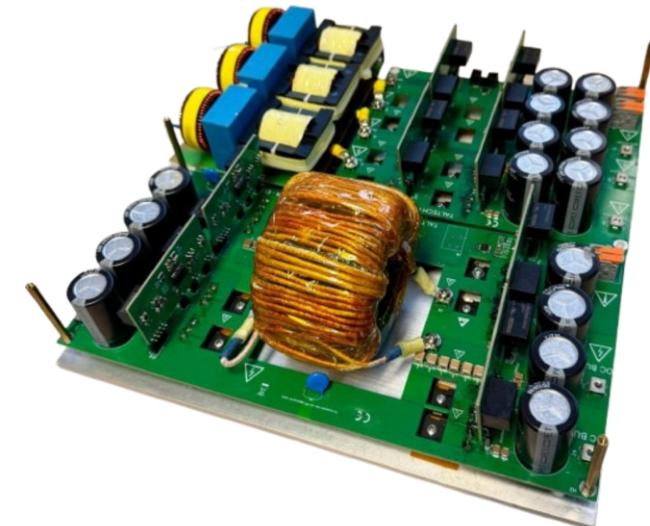
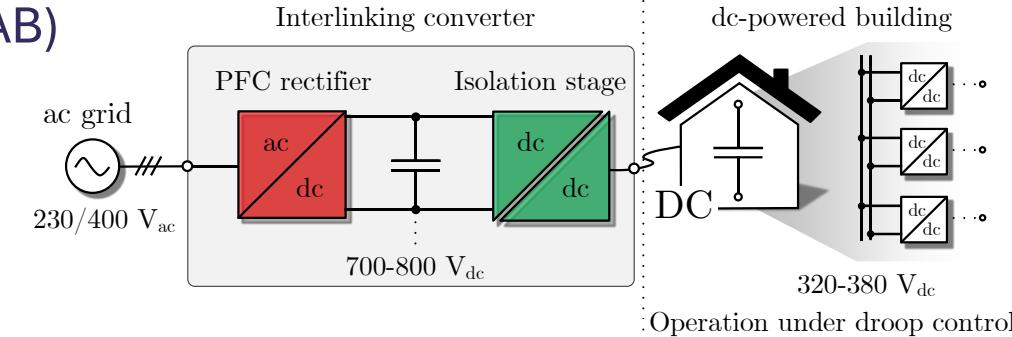
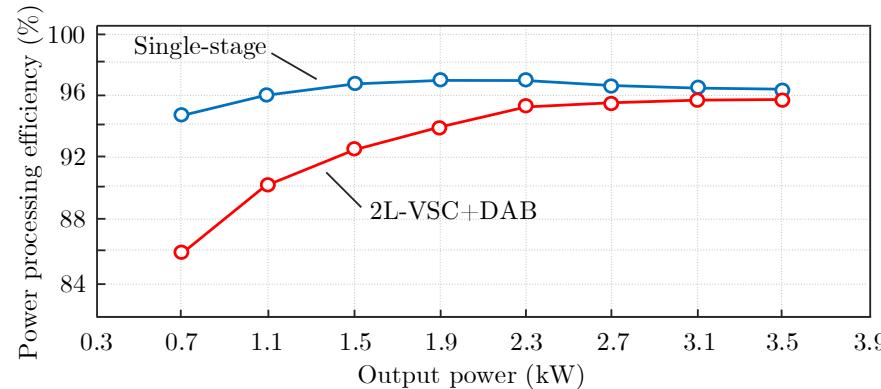
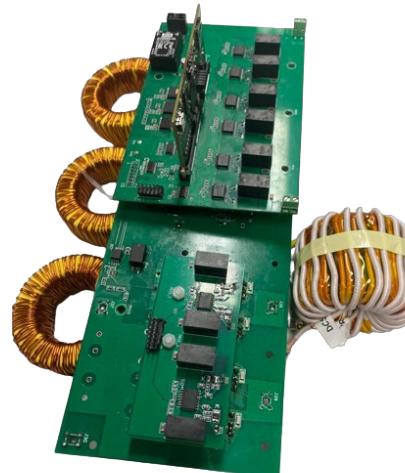


POWER CONVERTERS SOLUTIONS FOR GIC

TWO-STAGE AC-DC CONVERTERS

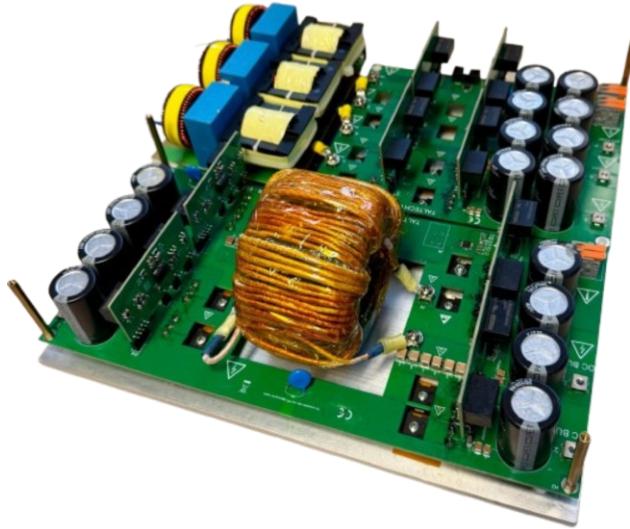


- Based on voltage source (2L-VSC) + Dual Active Bridge (DAB)
- Bulking intermediate DC bus for decoupling both stages
- Flexible solution – allows to develop different functions for grid interaction
- Flat efficiency is the main challenge

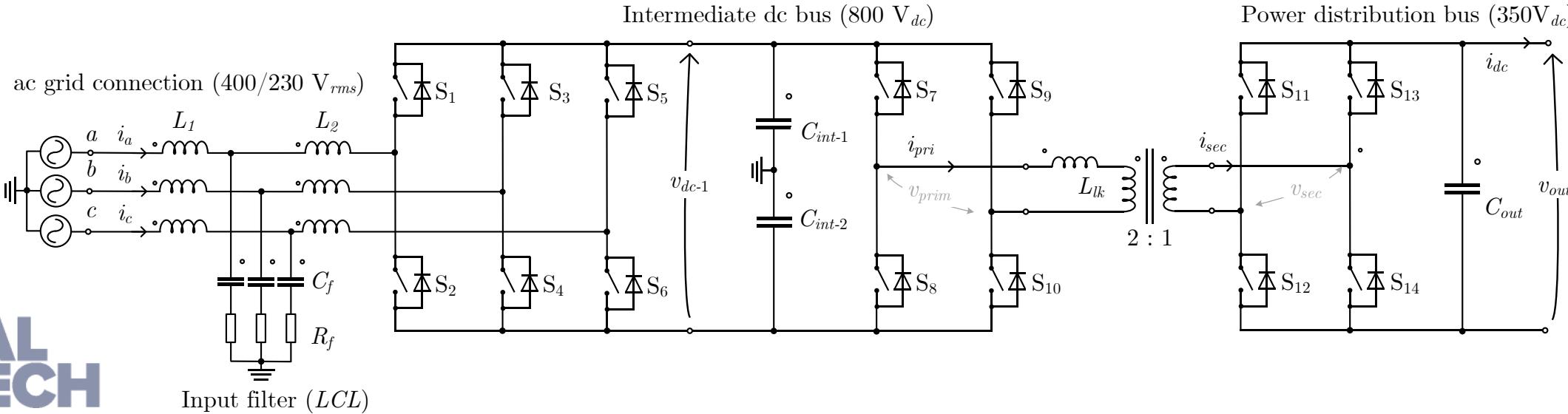


POWER CONVERTERS SOLUTIONS FOR GIC

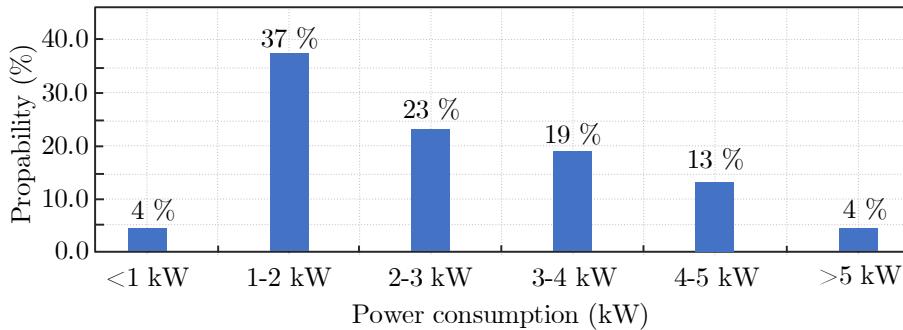
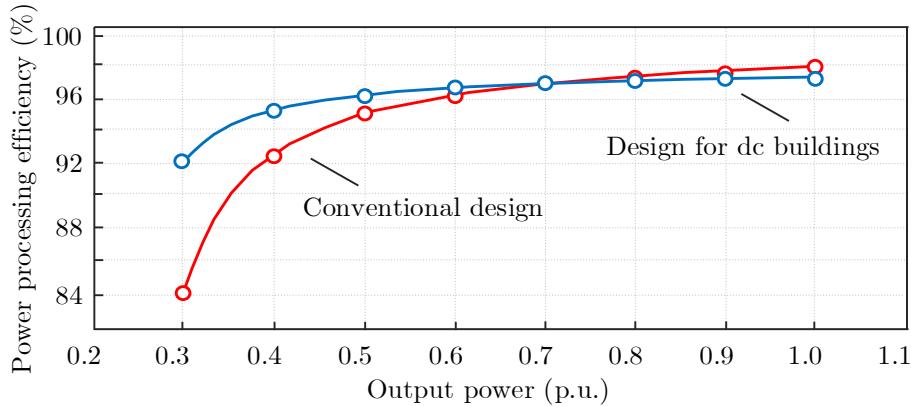
TWO-STAGE AC-DC CONVERTERS



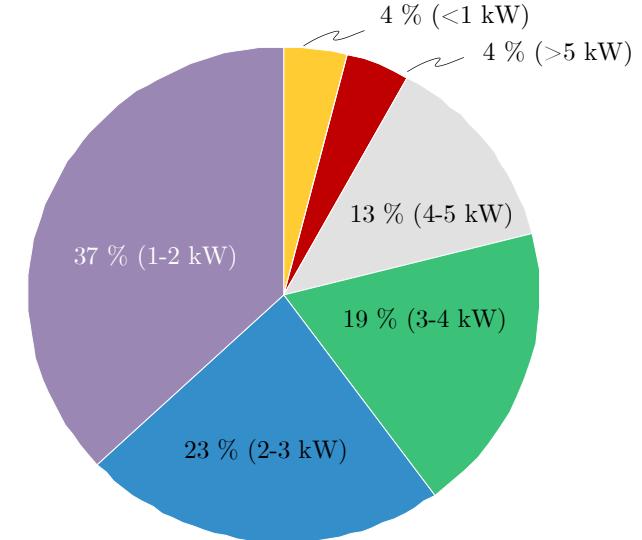
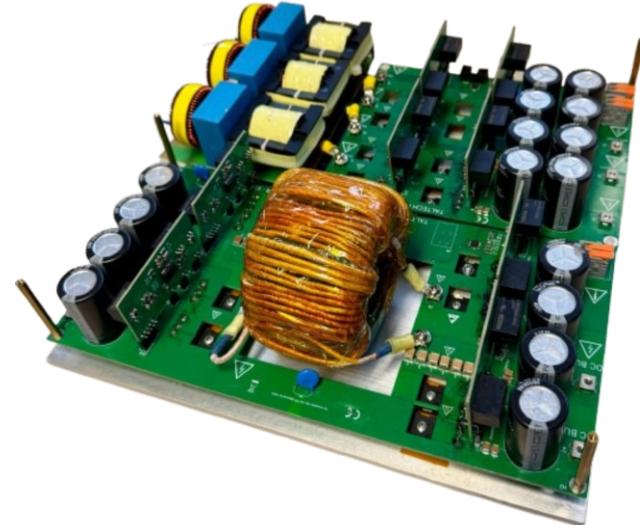
- Bidirectional power router for prosumer DC buildings
- High-frequency galvanic isolation
- Input 230/400 V_{ac} , output 350 V_{dc} , 5...10 kW
- Droop control according to Current/OS protocol
- Efficiency curve optimized for part-load operation based on statistical data (> 97 %)
- Possible multi-port configuration with USB-PD output



DESIGN TARGETS AND PRIORITIES

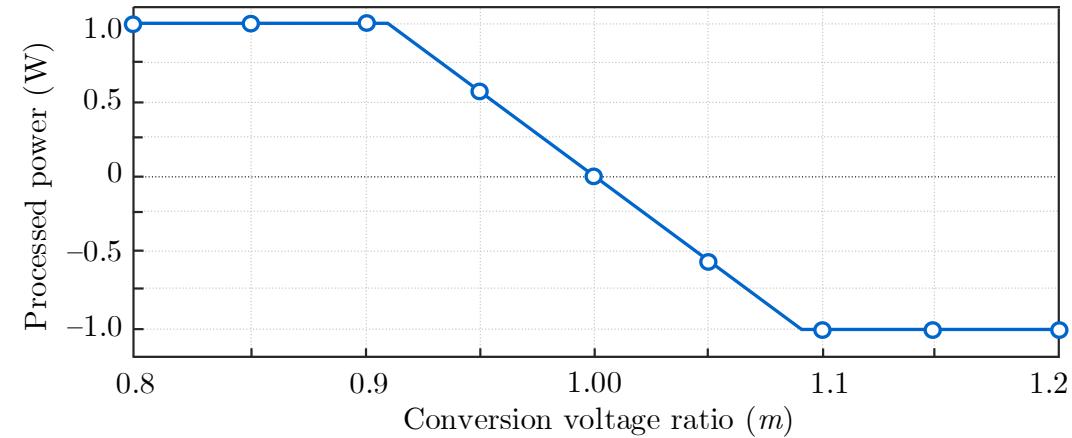
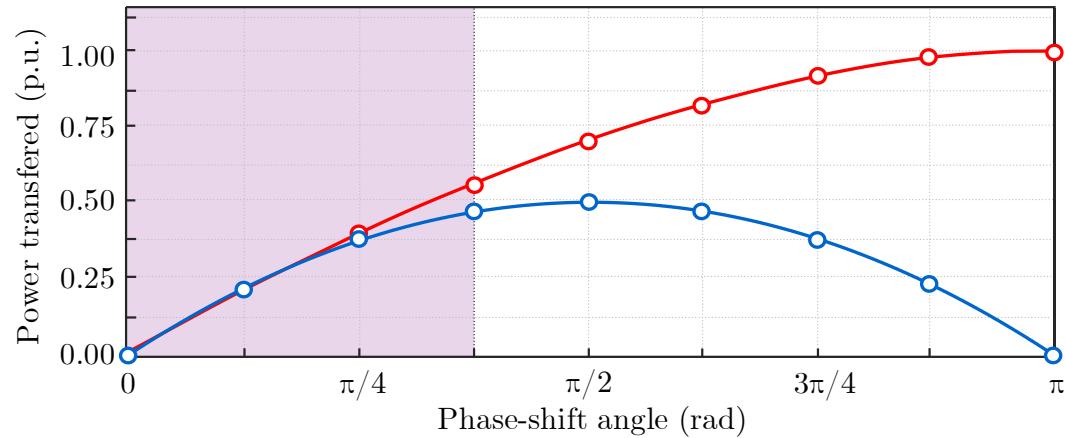


- Application oriented design
- Investigate actual operational profile
- Indicate most probable working conditions
- Optimized design considering the droop curve



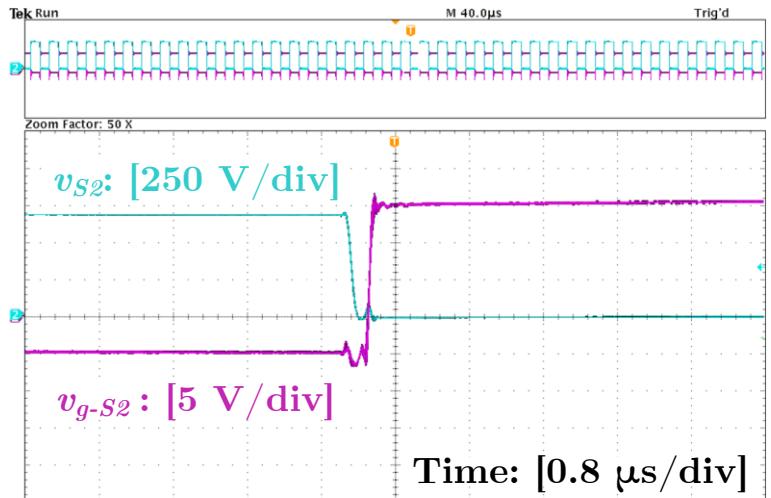
DROOP CONTROL IMPACT ON CONVERTER EFFICIENCY

- **Conventional design:** designed to operate within a **predefined region**
- **Operation under droop control:** the processed power is constrained to follow a **specific line**, which is determined by the droop control
- **Effective operation area should be considered**

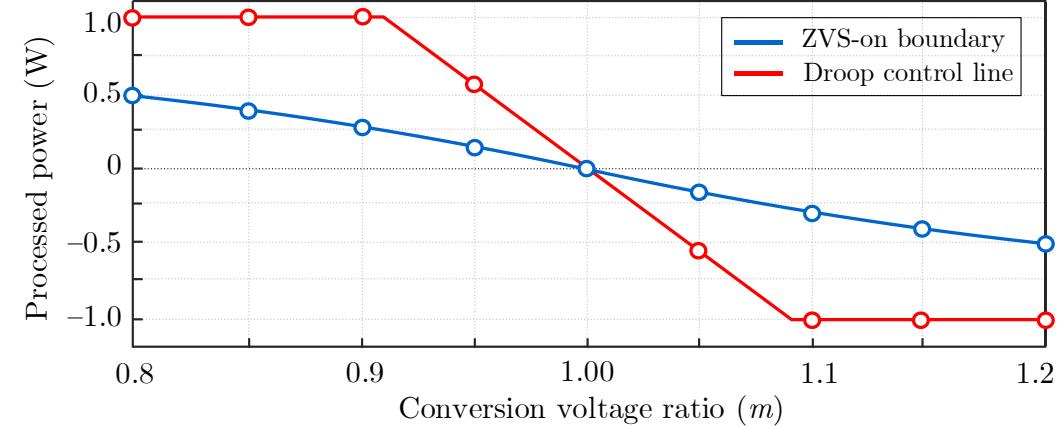


DROOP CONTROL IMPACT ON CONVERTER EFFICIENCY

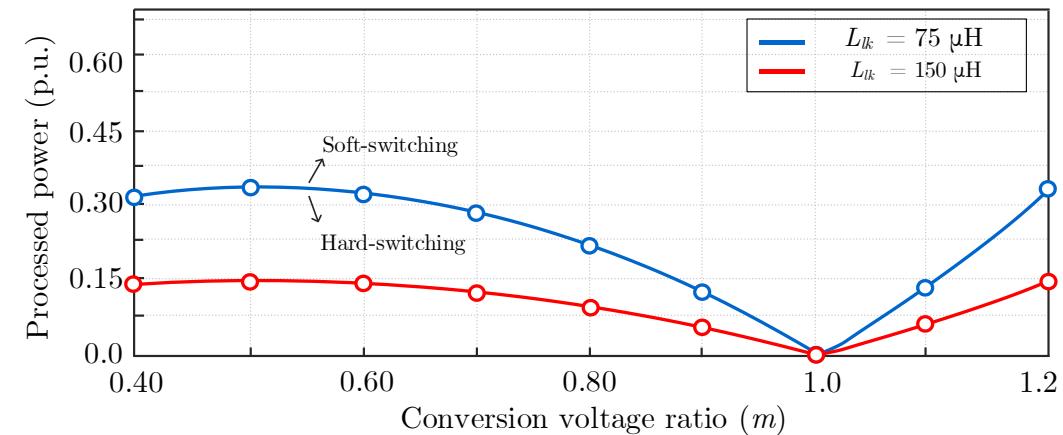
- Dual Active bridge operation
- How does droop control affect the soft-switching operation?
- Under droop control is possible to ensure **wide soft-switching range**



ZVS-on boundary / droop control line

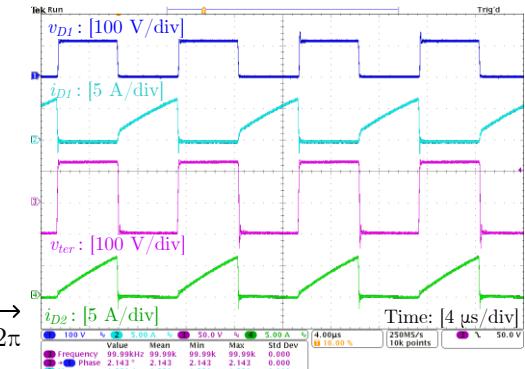
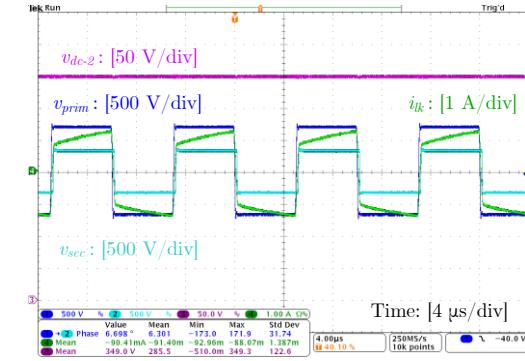
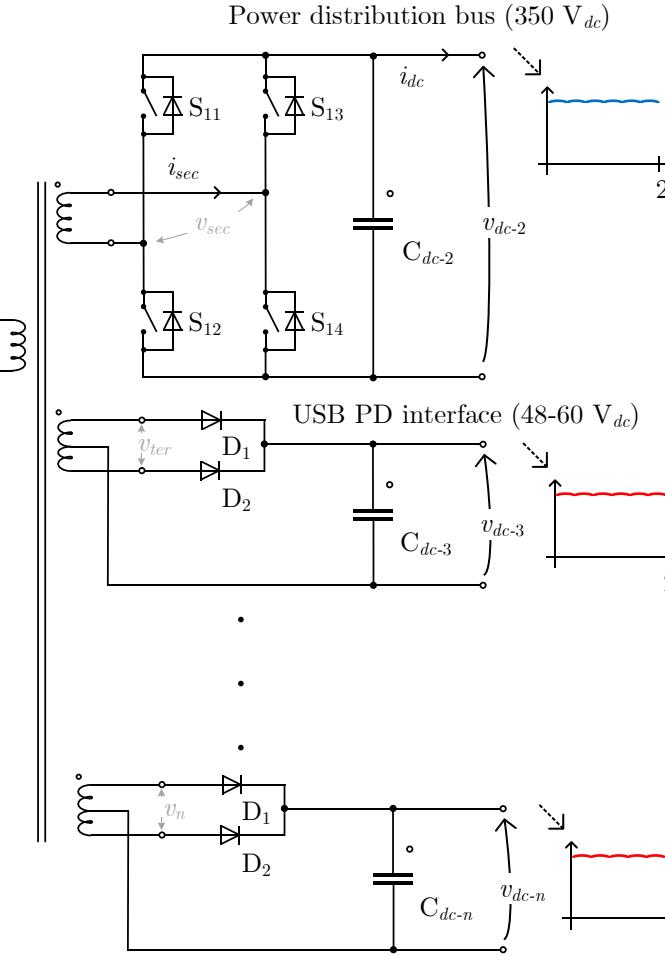
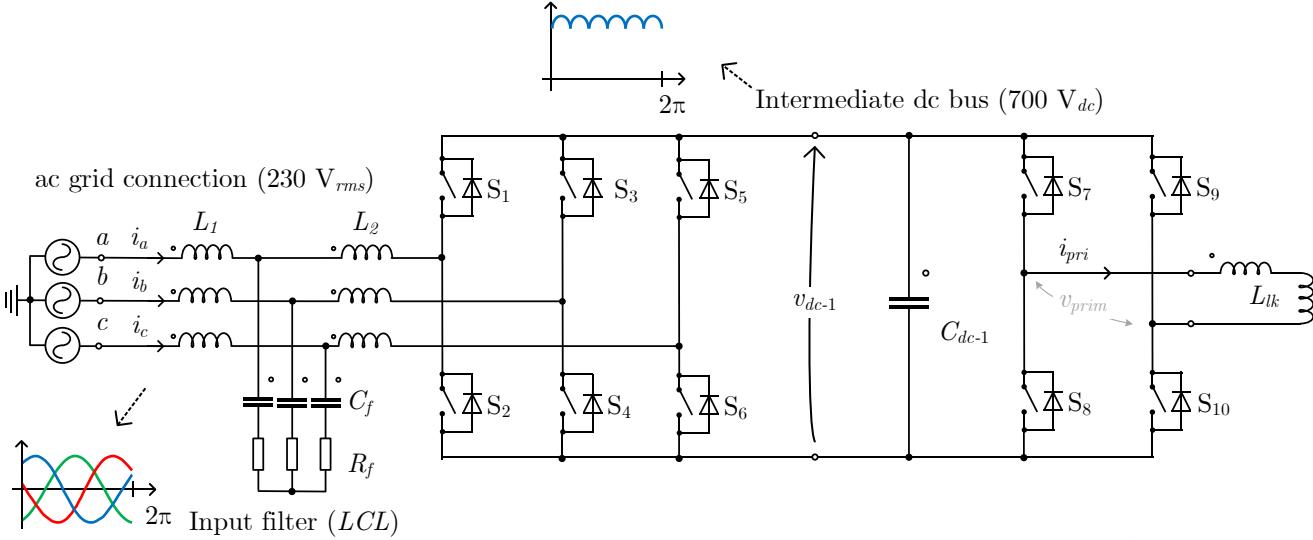


Soft-switching boundaries



EMERGING TOPOLOGIES FOR GIC

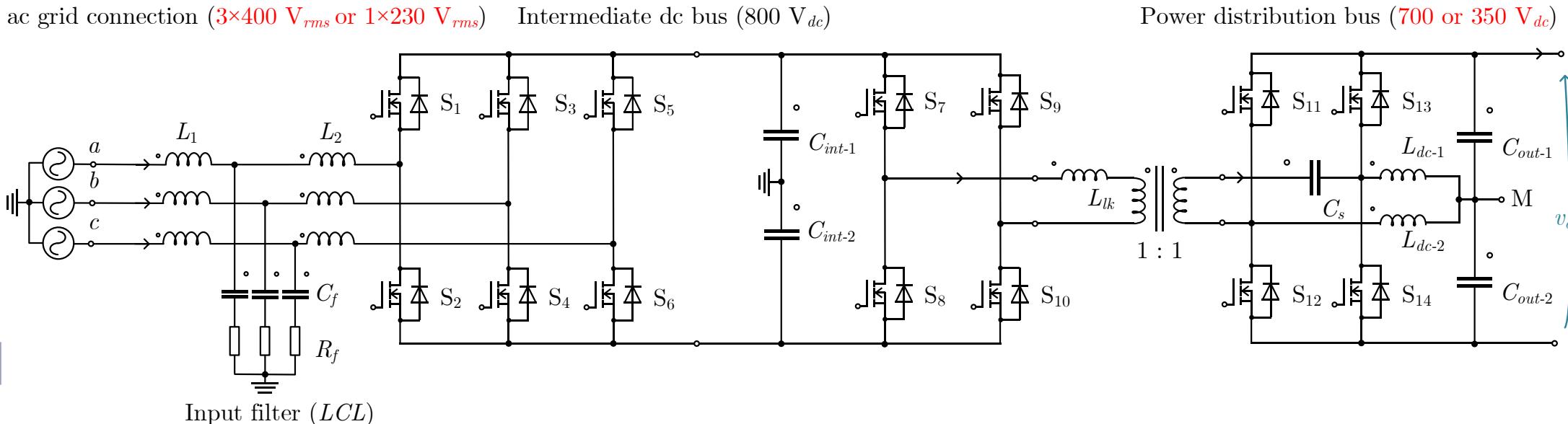
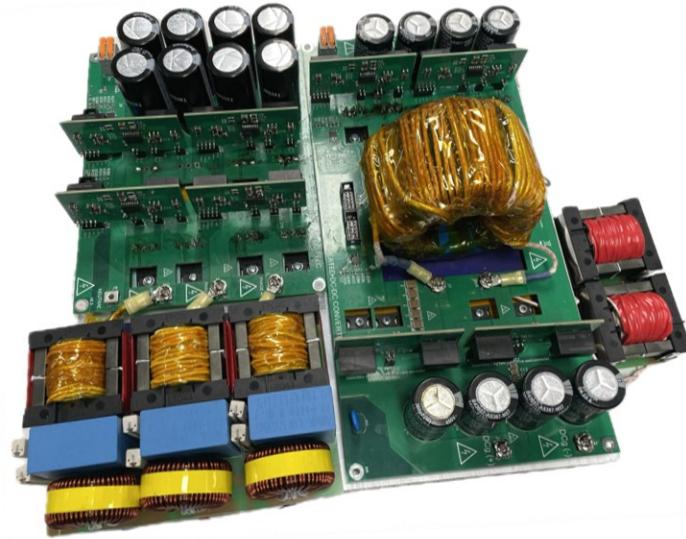
- Multiport converter with USB PD interface, according to Current/OS protocols



EMERGING TOPOLOGIES FOR GIC

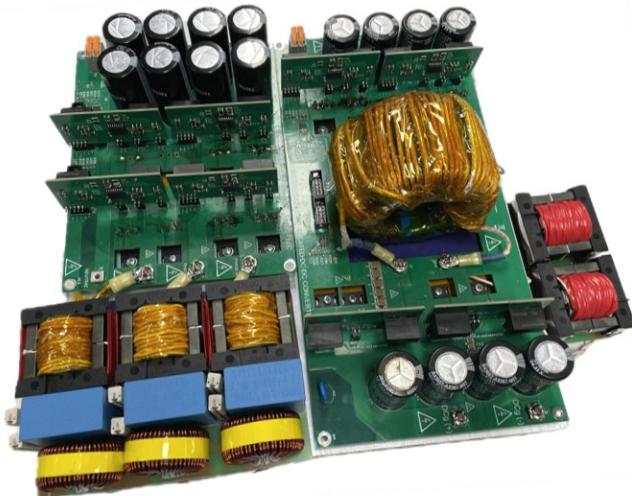
- Universal interlinking converter:

- Proposed to cover different types of DC grids (**bipolar and unipolar**)
- Self-balanced** configuration (additional service for the dc grid)
- Reduced number of semiconductors
- Either **single- or three-phase** connection with AC grid
- Better resilience and flexibility



EMERGING TOPOLOGIES FOR GIC

- **High flexibility for the AC grid connection:**
 - Individual phase control enables connection to both single-phase and three-phase systems
 - Under fault conditions, the converter can continue operating with derated power



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TABLE I
VOLTAGE, CURRENT, AND POWER RATINGS ACCORDING TO THE CONVERTER
OPERATION MODES

	Mode	ac voltage	ac current	Power rate
3-ph	Normal	* $3 \times 400 \text{ V}_{rms}$	7.25 A_{rms}	5.00 kW
1-ph	Normal	230 V_{rms}	7.25 A_{rms}	1.67 kW
2-ph	Abnormal	230 V_{rms}	7.25 A_{rms}	3.34 kW
1-ph	Abnormal	* $1 \times 400 \text{ V}_{rms}$	7.25 A_{rms}	2.90 kW

* Line-to-line voltage

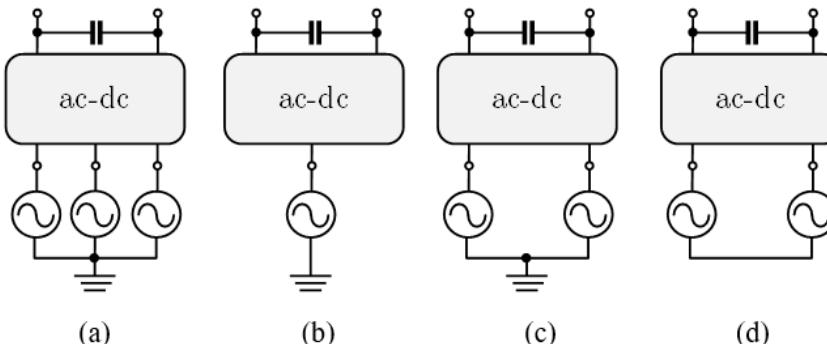
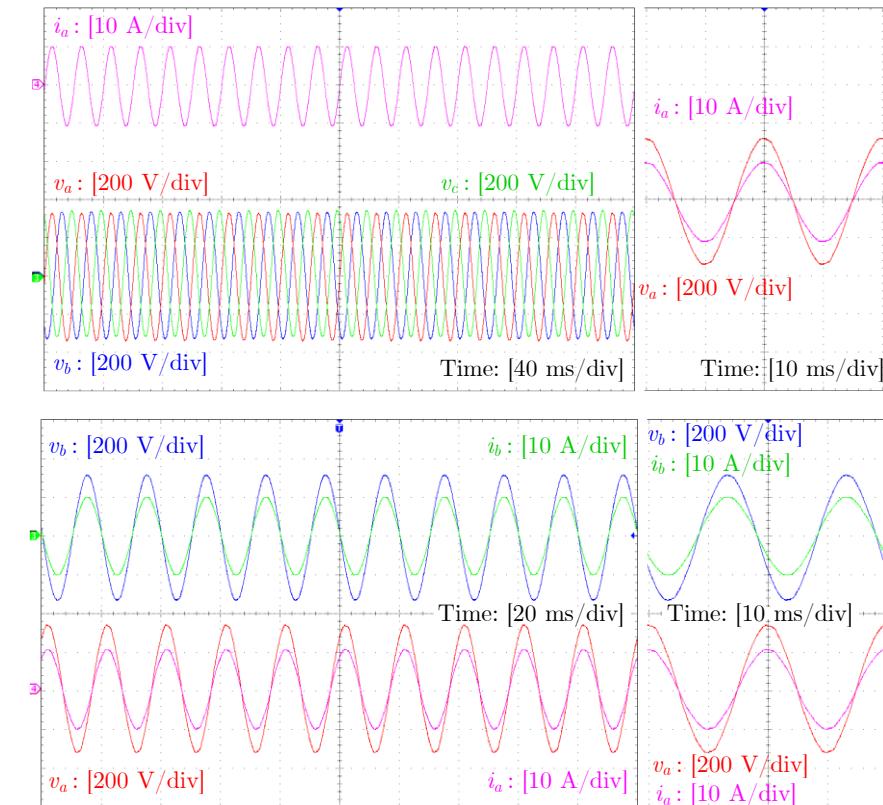


Fig. 2. Possible converter operation modes, according to the ac grid connection, and fault occurrence; (a) Mode I; (b) Mode II; (c) Mode III; and (d) Mode IV.



TALTECH RESIDENTIAL DC INNOVATION HUB



The first DC EXPERIENCE CENTER in Northern Europe



- An **international open platform** for research and demonstration of residential DC power distribution technology
- **Validation of net-zero-energy solutions** (workplace, space heating and cooling, ventilation, etc.)
- The **living lab** blends the everyday real-life experiences of pilot users with academic research to develop future-proof, energy-saving technologies
- **Data collection** for the future design of the energy-neutral TalTech campus

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taltech.ee/en/i3dc-initiative



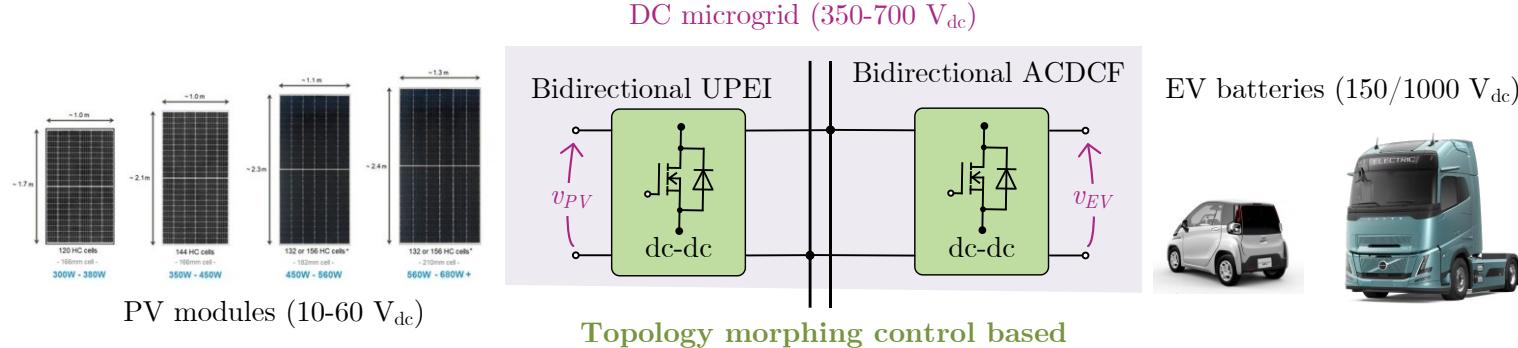
OVERVIEW OF FULL-POWER CONVERTERS FOR WIDE VOLTAGE RANGE APPLICATIONS

Dr. Sachin Chauhan



WHY WIDE VOLTAGE RANGE OPERATIONS?

- In Electric Vehicles
 - Battery voltage variation (150 V – 1000 V)
 - Regenerative braking and dynamic load conditions
 - Compatibility with multiple battery chemistries
- In Photo-Voltaic Systems
 - Solar panel voltage variation (e.g., 10-60 V) Per Module :
 - Irradiance/ Temperature/ MPPT
- Supporting Multiple Applications and Standards (350/700 Vdc according to Current/OS)
- Handling input/output voltage variations



Voltage Range	Architecture Type	Chemistry	Examples of Use
200V – 400V	Standard High Voltage	NMC, LFP, NCA	Nissan Leaf, Chevy Bolt, Tesla Model 3/Y (LFP or NCA), BMW i3
400V – 500V	Enhanced High Voltage	NMC, NCA	Tesla Model S/X, Audi e-tron, Hyundai Kona EV
800V – 900V+	Ultra-High Voltage	NMC	Porsche Taycan, Hyundai Ioniq 5, Kia EV6 GT, Lucid Air, Rimac Nevera

- Maximizing Energy Harvest and Efficiency
- Bidirectional capability for batteries

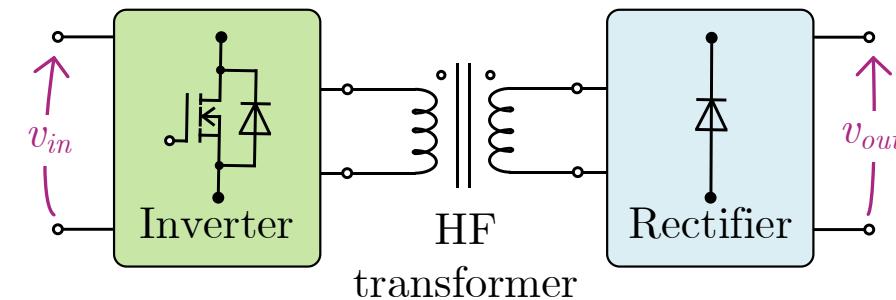
HOW TO ACHIEVE WIDE VOLTAGE RANGE IN DC/DC CONVERTERS?

Topology Morphing Control (TMC)

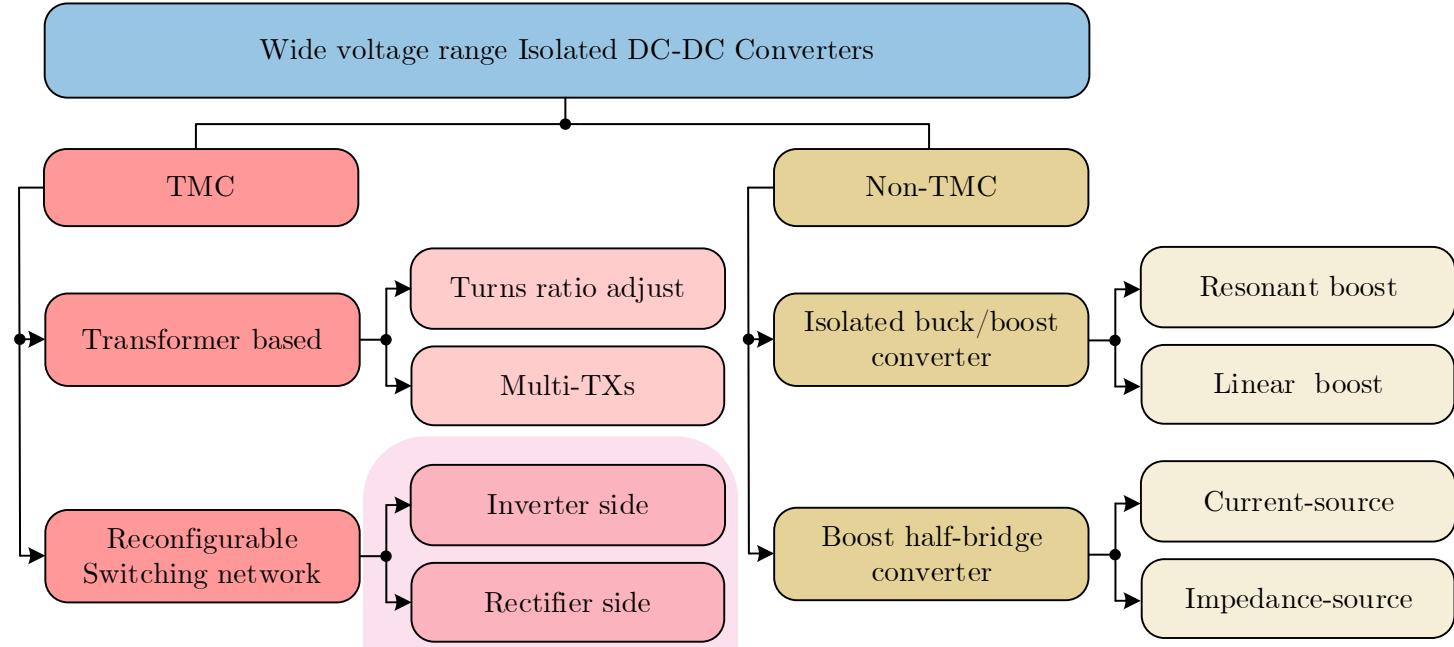
- Dynamic switch control to **morph between** the different topologies
- **Wide Input / Output voltage gain**
- Adaptable Gain Relation based on TMC.

Non-TMC

- Gain relation with control is **fixed** based on the chosen topology.
- **Limited gain range.**

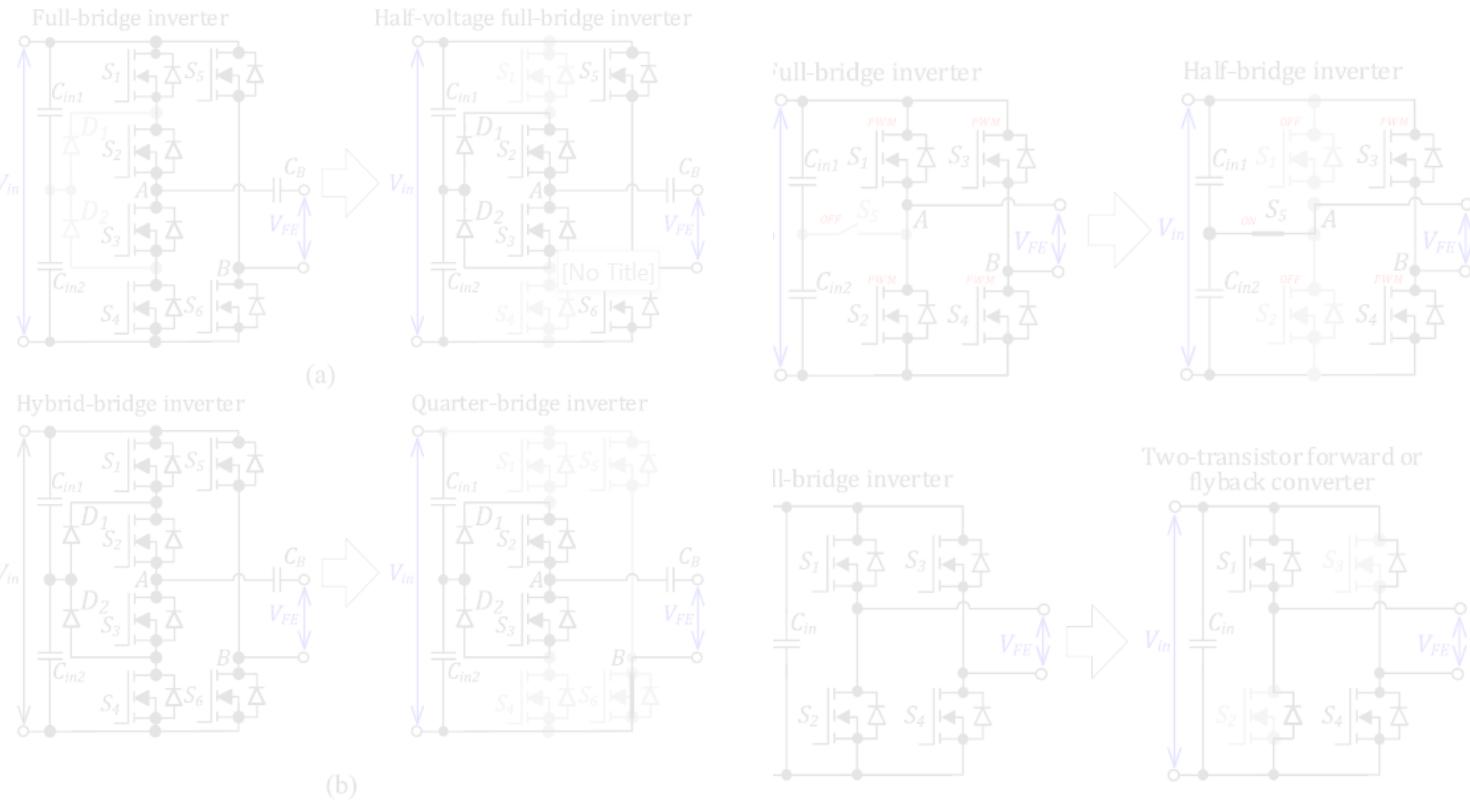
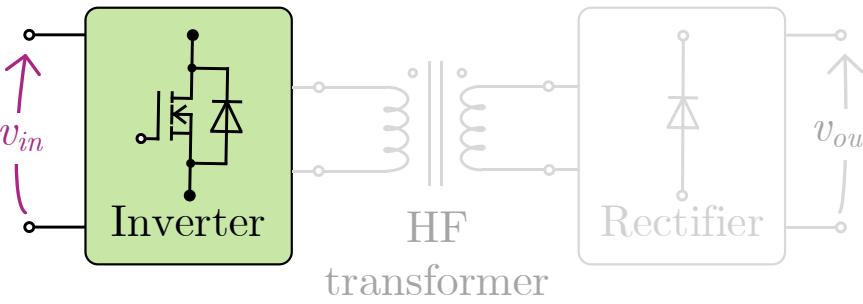
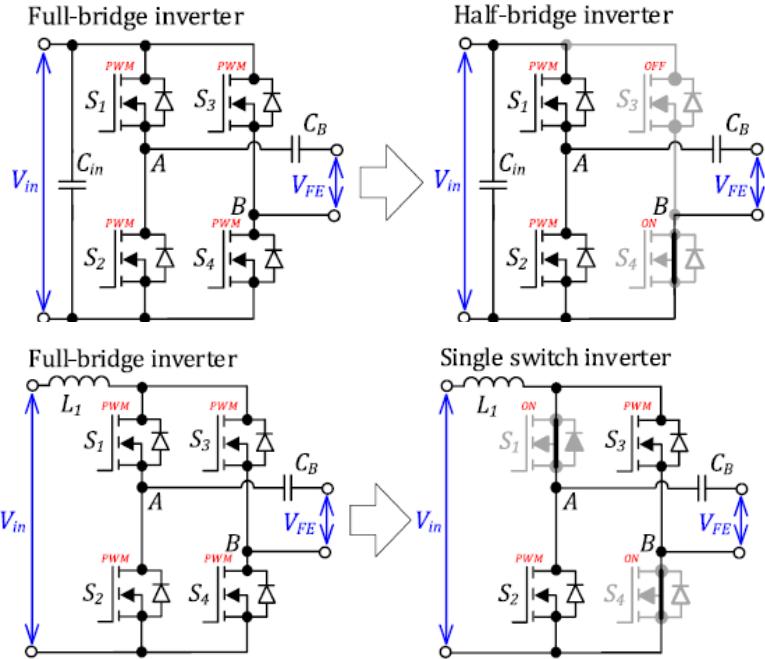


Overall voltage gain:
Inverter x transformer x rectifier



INVERTER SIDE TMC

- Normalized Voltage Gain Range Achieved (1;0.75;0.5;0.25)



INVERTER SIDE TOPOLOGY MORPHING CONTROL



TMC	Gain	S	D	C	Advantage	Disadvantage	Applications Examples		
							Vin, V	Vout, V	Power, W
FBI-HBI	1;0.5	4	0	2	Two-fold gain range extension	Higher Current stress on single switch	150-400	1650	2500[1]
FBI-2T-flyback or forward	1	4	0	1	Light load efficiency improvement (5%)	Higher conduction and reverse losses in body diodes	20-30	200-270	10-100[2]
FBI-SSI	1	4	0	L=1	Light load efficiency improvement (3%)	Higher current stress in diagonal switches	10-60	400	25-250[3]
H-TL FBI to HV FBI, to QBI	1;0.5;0.25	6	2	2	Four times gain range extension	Unequal voltage and current stress in switches	200-400	60	1200[4]
TL FBI to TQBI, to HVFBI, to QBI	1;0.75,0.5;0.25	8	4	4	Six times gain range extension	High number of switches, unequal current stress in switches	200	200-700	3500[5]

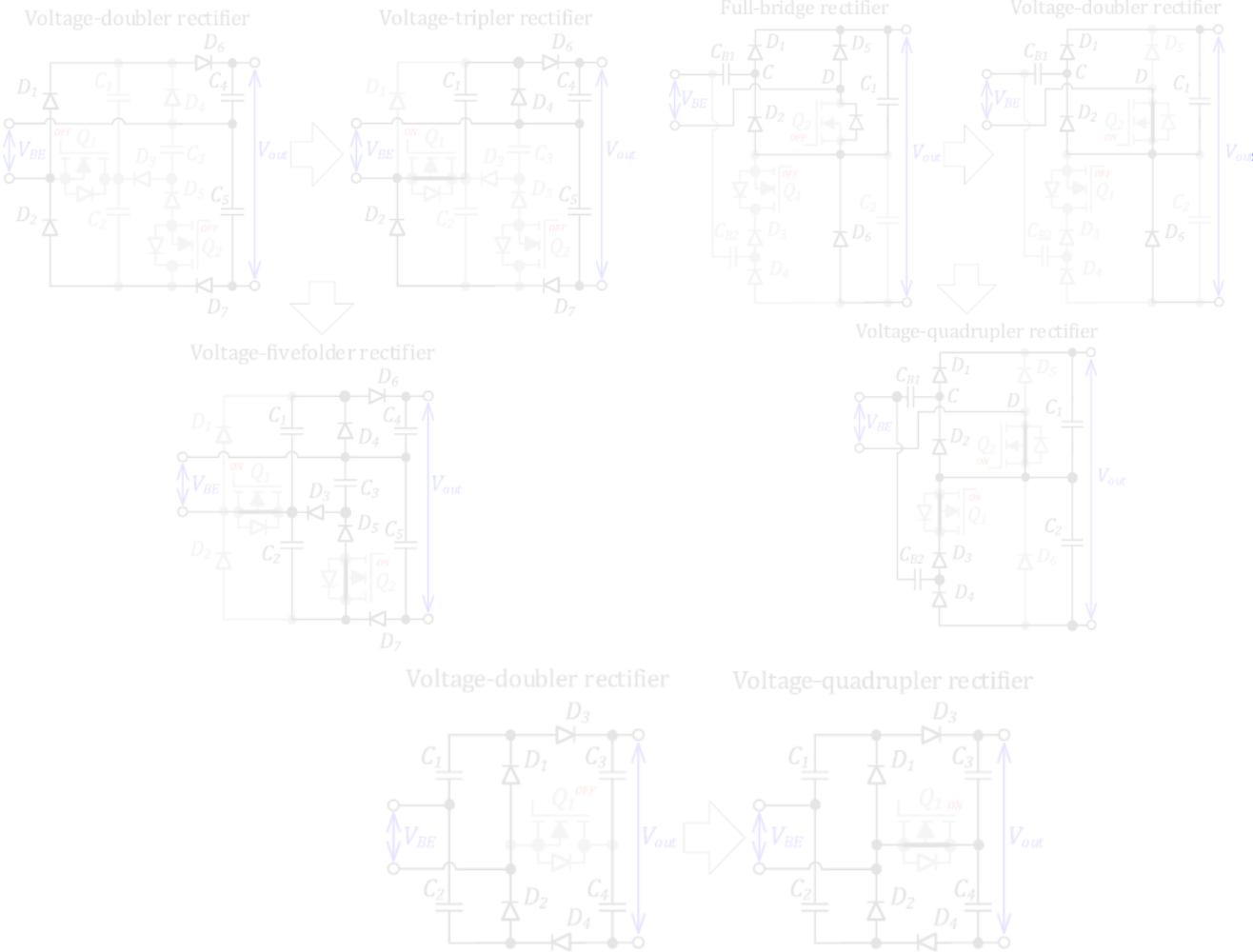
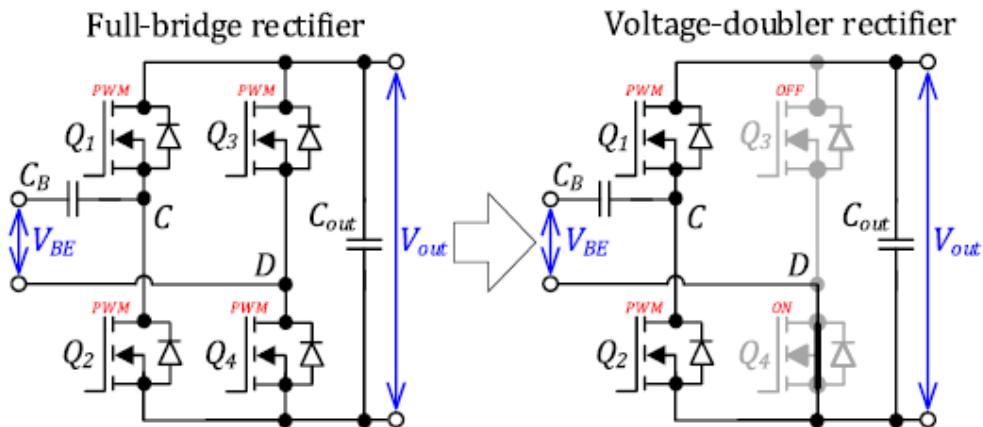
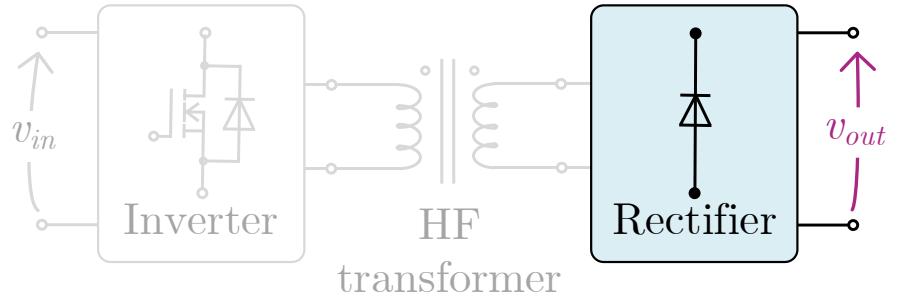
Note: S=Switch, D= Diode, C= capacitor, L= inductor



A. Chub, D. Vinnikov, R. Kosenko, and E. Liivik, "Wide input voltage range photovoltaic microconverter with reconfigurable buck-boost switching stage," IEEE Trans. Ind. Electron., vol. 64, no. 7, pp. 5974–5983, Jul. 2017.

RECTIFIER SIDE TOPOLOGY MORPHING CONTROL

- Normalized Voltage Gain Range Achieved (G:1-6)



RECTIFIER SIDE TOPOLOGY MORPHING CONTROL

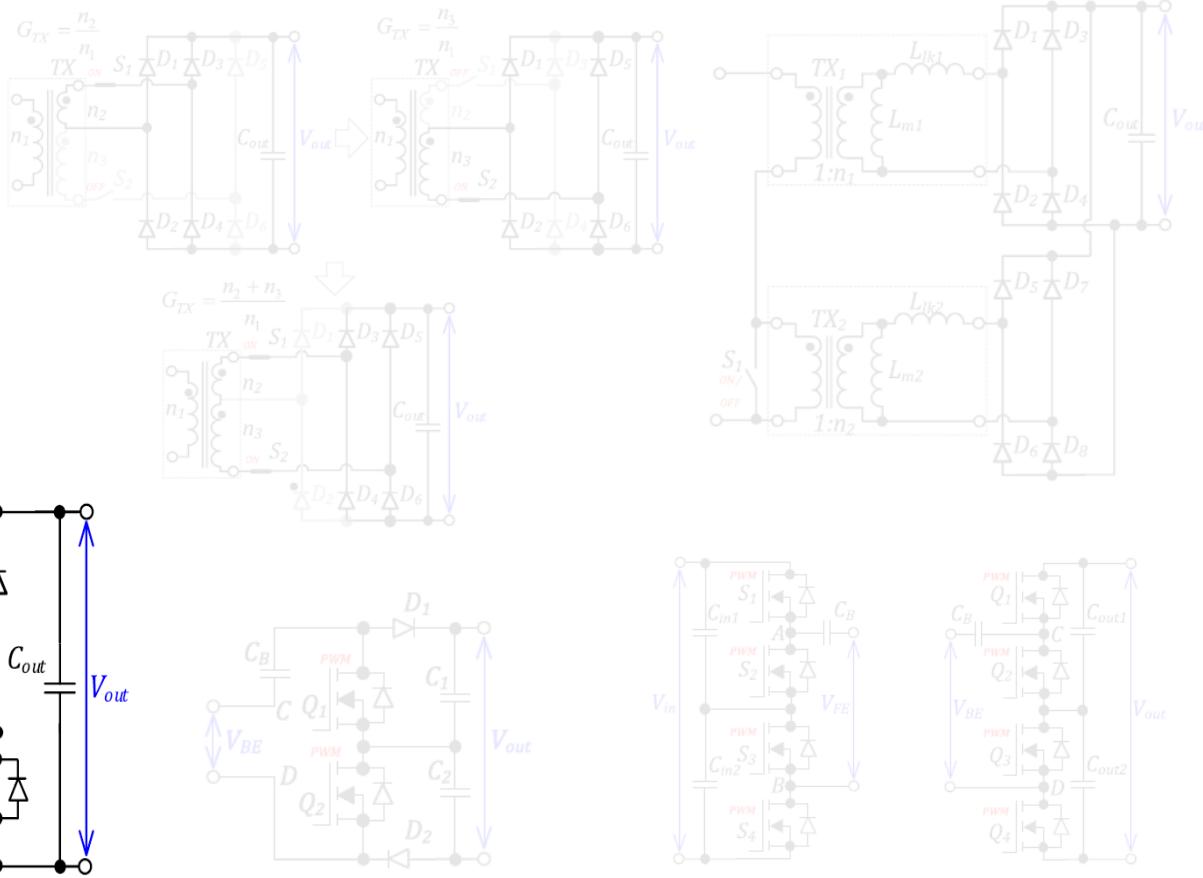
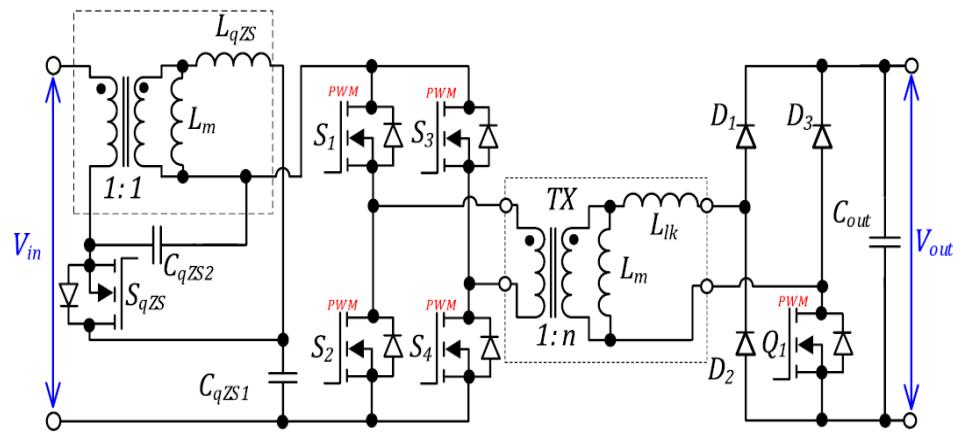


TMC	Gain	S	D	C	Advantage	Disadvantage	Applications Examples		
							Vin, V	Vout, V	Power, W
FBR-VDR	1;2	4	0	2	Two fold gain range extension	Higher Current stress on single switch and blocking capacitor	200-950	1650	3300[1]
FBR to SSR	1	4	0	1	Light load efficiency improvement (8%)	Higher conduction and reverse recovery losses in body diodes	20-30	200-270	10-100[2]
VDR-VQR	2;4	1	3	4	Two fold gain range extension	Higher Current stress on single switch and blocking capacitor	150-400	1650	2500[3]
FBR to VDR, to VQR	1;2;4	2	6	4	Four times gain range extension	Higher semiconductors, unequal and high currents stress on diodes and switches	5-110	400	360[4]
VDR to VTR, to VFR	2;3;5	2	7	5	2.5 fold gain range extension	High number of utilized components, unequal current stress in diodes	25-100	500	250[5]
VQR to VFR, to VSR	4;5;6	2	8	6	1.5 fold gain range extension	Higher number of switches, unequal current stress in switches.	25-50	760	300[6]
TL FBR to 1.5xVM, to VDR, to VQR	1;1.5;2;4	8	4	4	Four times gain range extension		200	200-700	3500[7]

Note: S=Switch, D= Diode, C= capacitor, L= inductor

ADVANCES IN TOPOLOGY MORPHING CONTROL

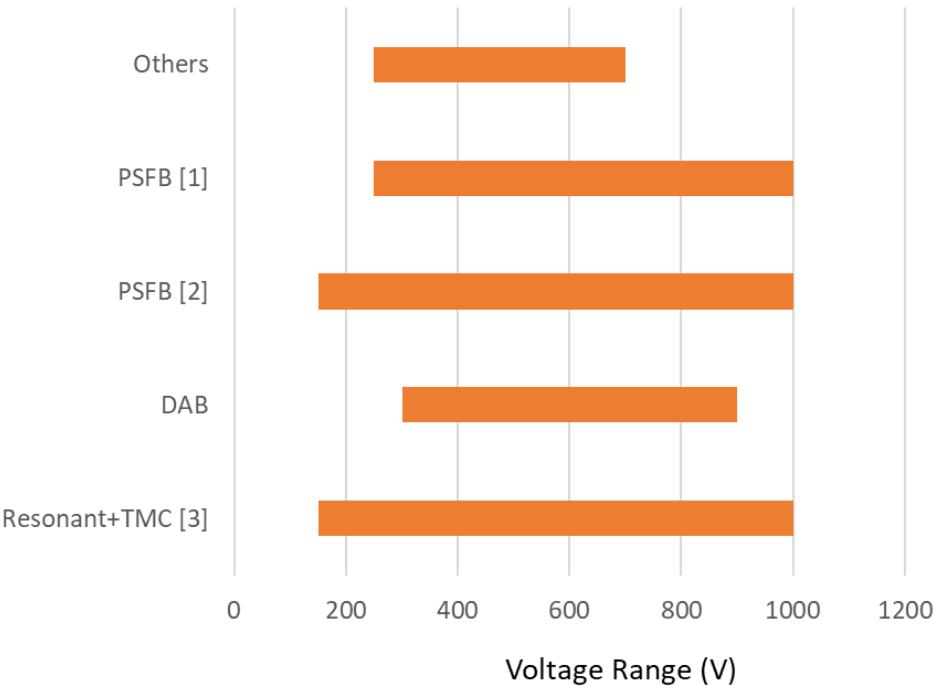
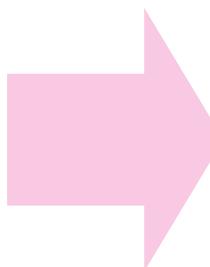
- Active rectifier with variable structure
- ACTIVE Three-level Half-bridge Inverter and Rectifier With Variable Structure
- Adjusting Transformer Turns Ratio
- Bypassing Series Transformer
- Double Full-Bridge LLC Converter
- Five-switch reconfigurable inverter
- LLC with auxiliary coupled inductor
- Transformer with fractional turn ratios
- Multitrack Converter Architecture
- Quasi-Z-source



CONVERTER TOPOLOGIES FOR WIDE-VOLTAGE RANGE

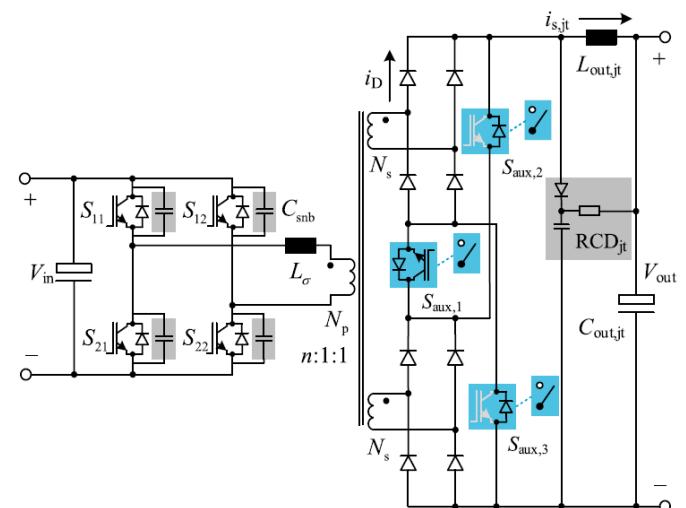
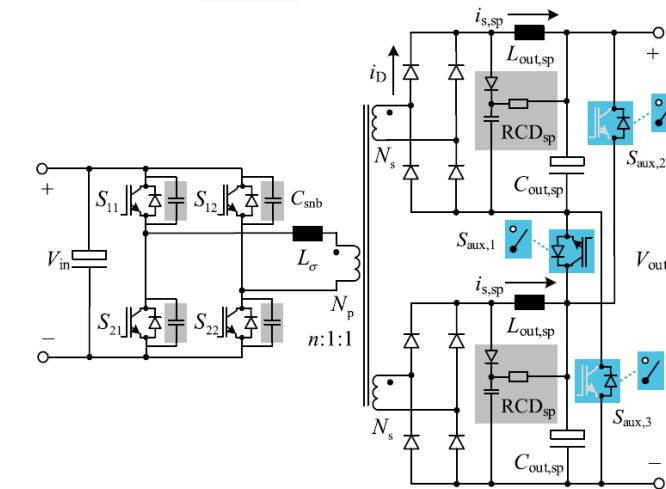
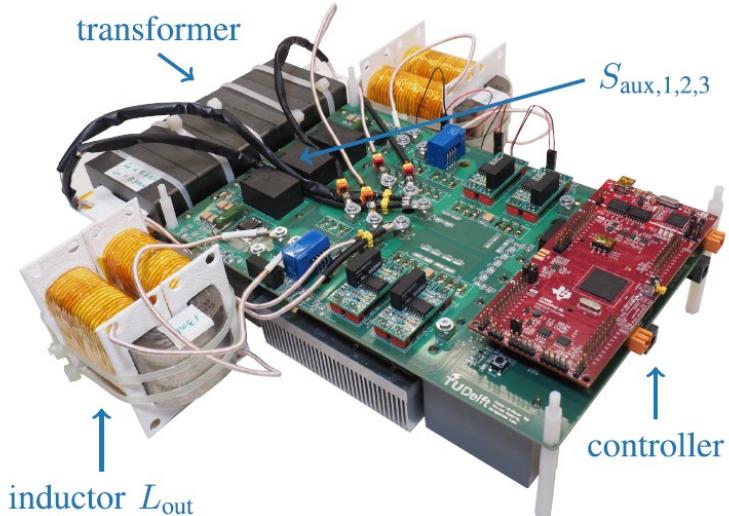
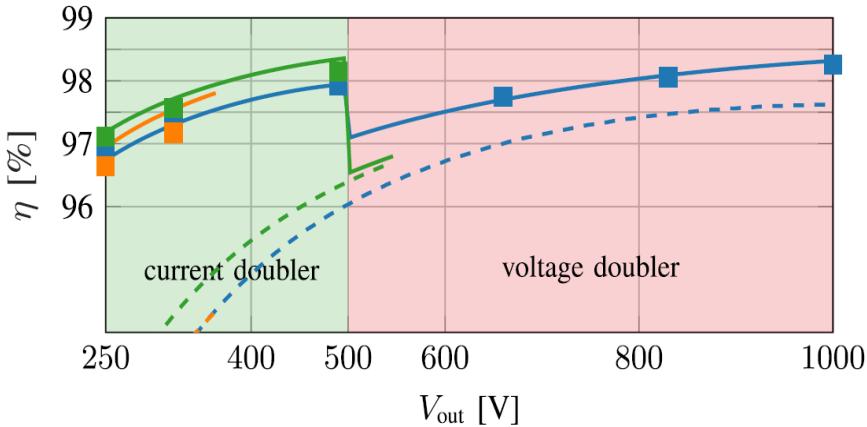
- Non-Isolated Topologies
 - Buck-Boost (incl. SEPIC, CUK, Zeta)
 - Interleaved design for higher power levels
- Isolated Topologies
 - Full-bridge, Push-Pull, Flyback (up to medium power level)
 - Dual Active Bridge (DAB)
 - Phase-Shift Full Bridge (PSFB)[1,2 (T. U. Delft)]
 - Resonant + Reconfigurable Topologies

Topologies with relatively wider voltage range



WIDE-VOLTAGE RANGE ISOLATED TOPOLOGIES FOR EVS

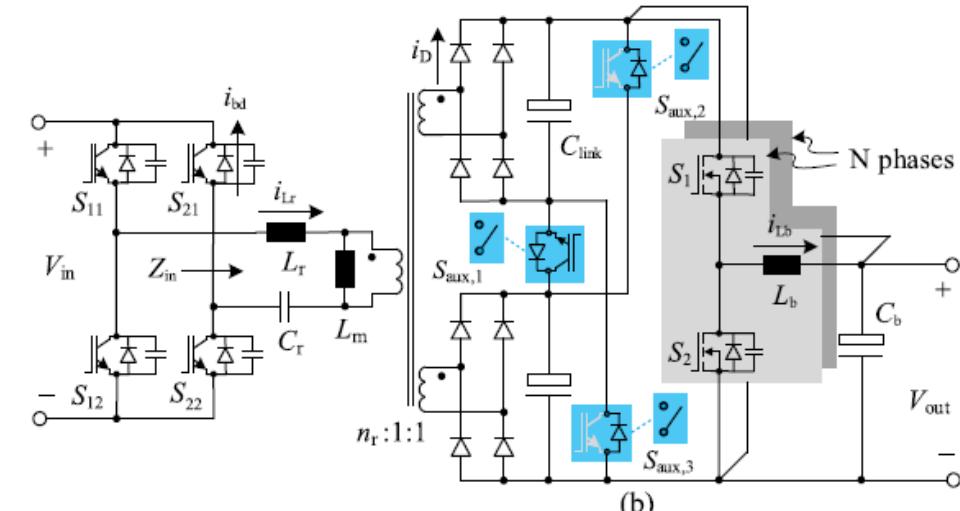
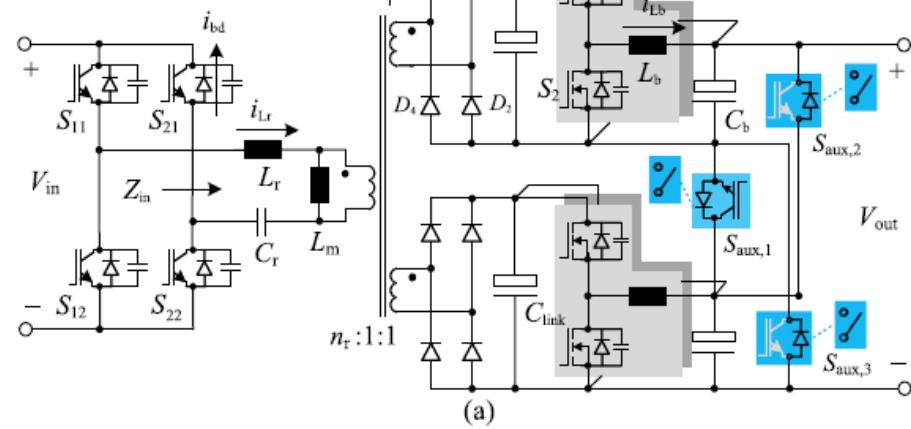
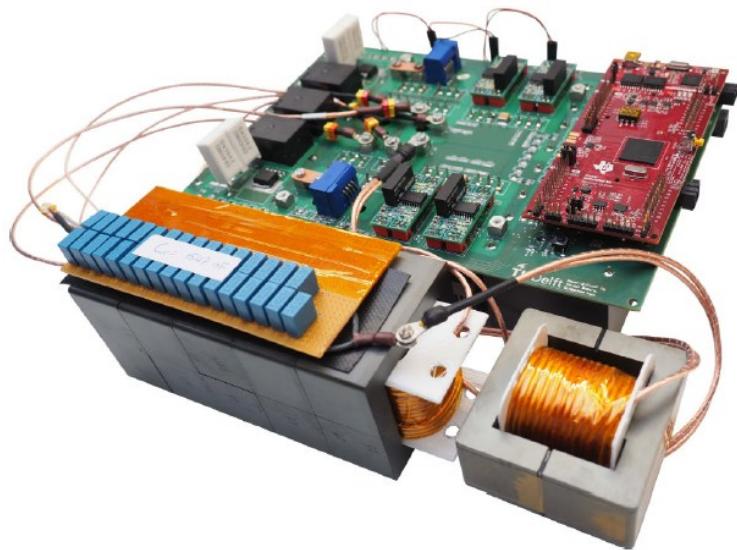
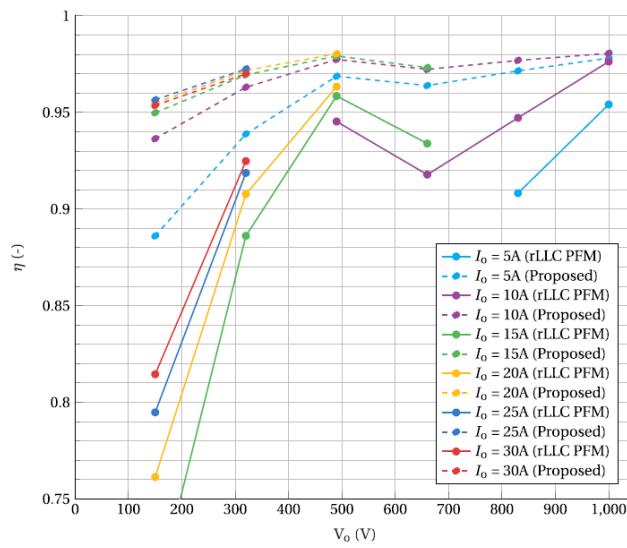
- Reconfigurable Phase Shift Full-Bridge Converter
 - V_{out} (250-1000V)
 - P_{out} 11 kW
 - Full Range Efficiency ($>96.5\%$)
 - Peak. Efficiency (98.3%)



WIDE-OUTPUT VOLTAGE RANGE CONVERTER FOR EVS

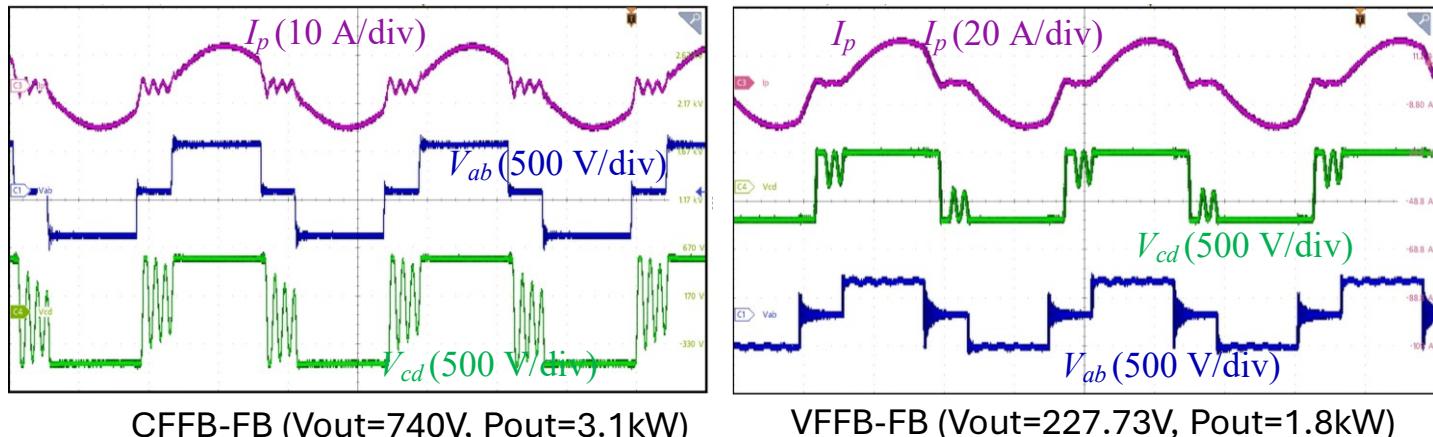
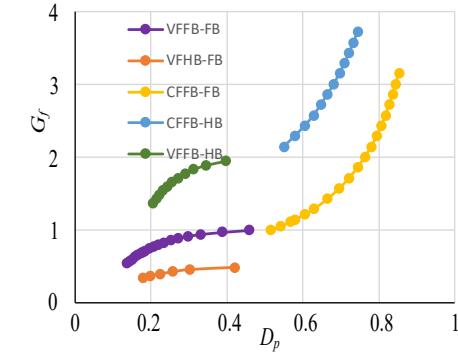
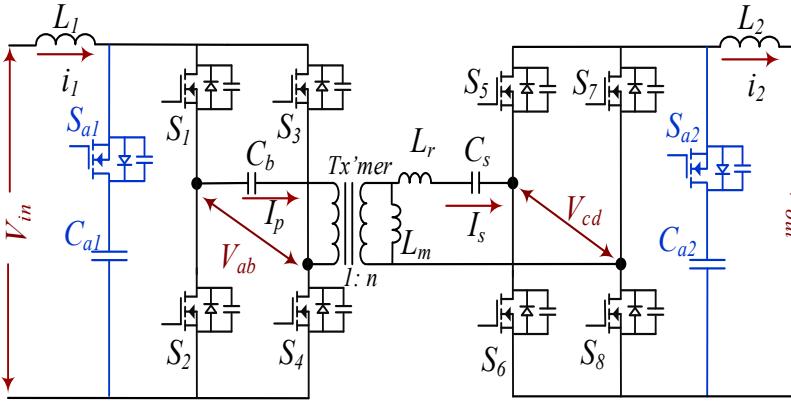
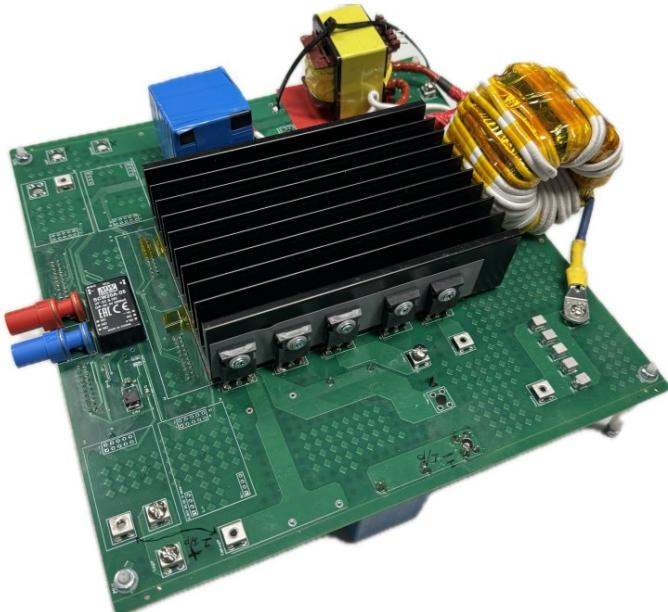
- A Reconfigurable Two-Stage 11kW DC-DC Resonant Converter

- Vout (150-1000V)
- Pout 11 kW
- Full Range Efficiency (>95%)
- Max. Efficiency (97.66%)



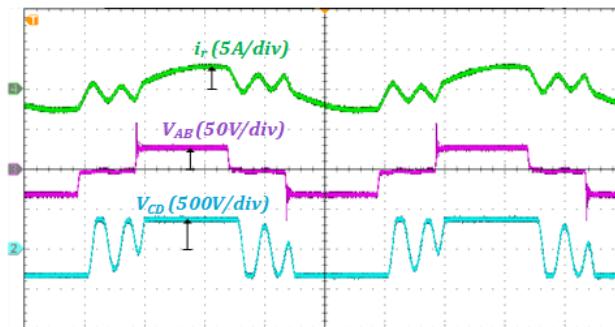
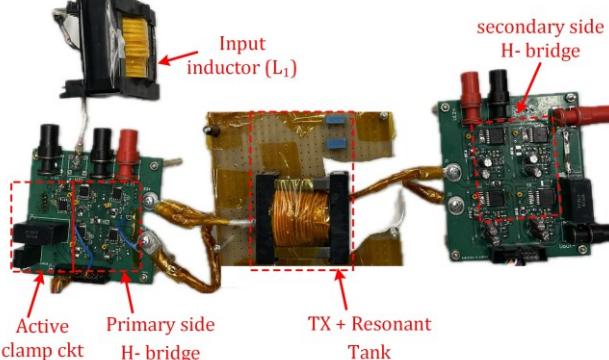
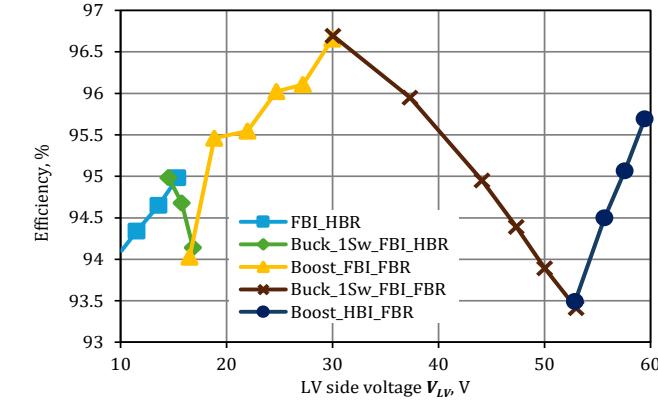
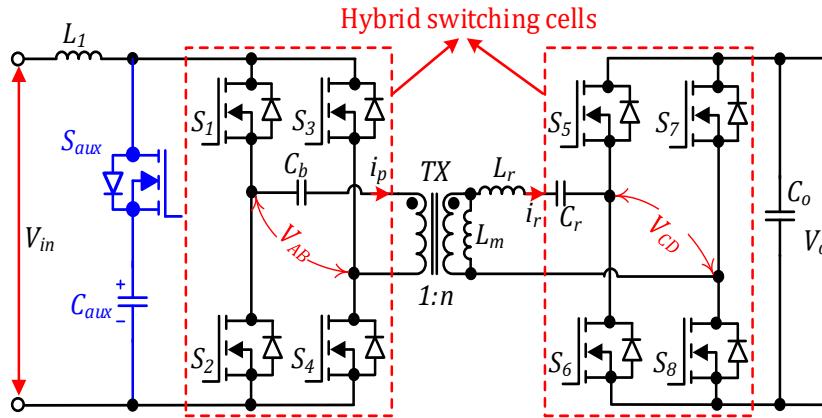
WIDE OUTPUT VOLTAGE RANGE CONVERTER FOR EVS

- Active Clamped Dual Current-Fed Bidirectional Converter
 - V_{in} (350V) and V_{out} (150-1000V)
 - 3.1 kW prototype with Max efficiency (97.66%).
 - Full Range Efficiency (>93%)

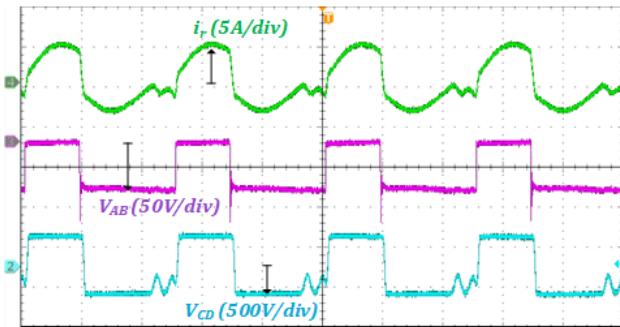


WIDE INPUT VOLTAGE RANGE CONVERTER FOR PV AND DC BUILDING APPLICATIONS

- Current-Fed Isolated Buck-Boost Series-Resonant DC-DC Converter
 - V_{in} (10-60 V) and V_{out} 350V.
 - 350W prototype with Max efficiency ($>96.6\%$).
 - Can support both PV and Battery charging
- CF 1sw-FBR mode introduced for better efficiency in buck mode



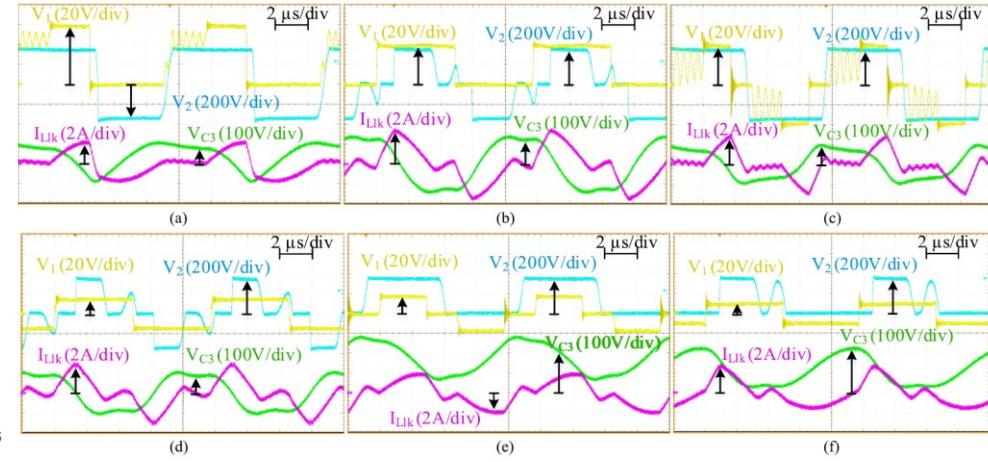
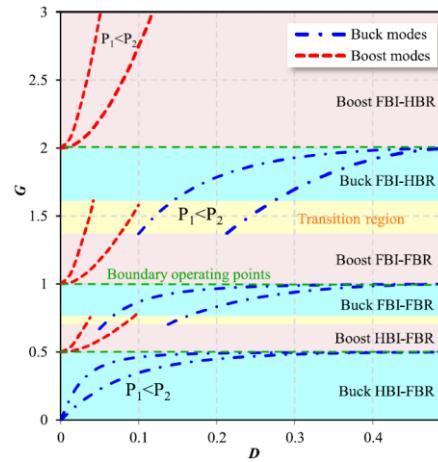
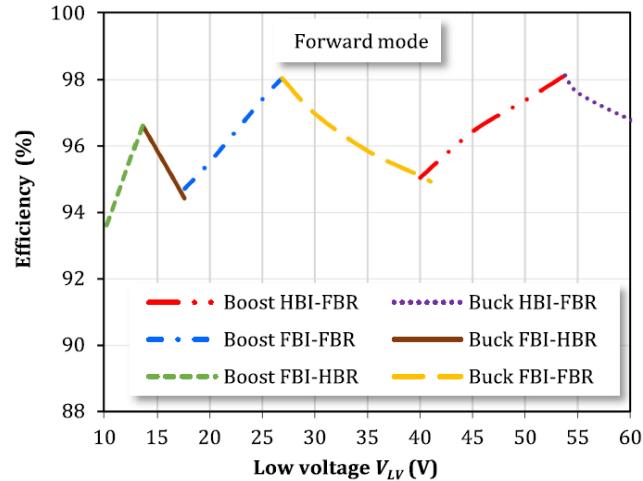
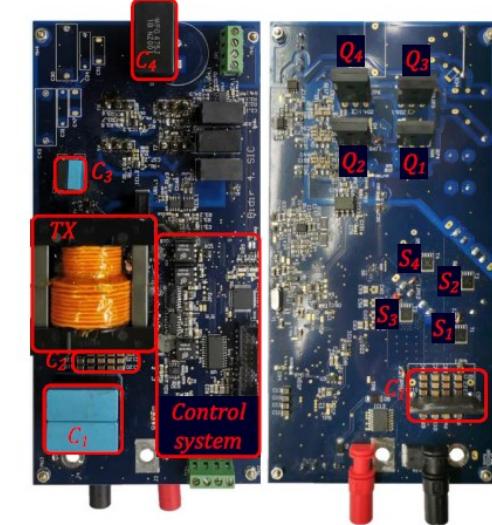
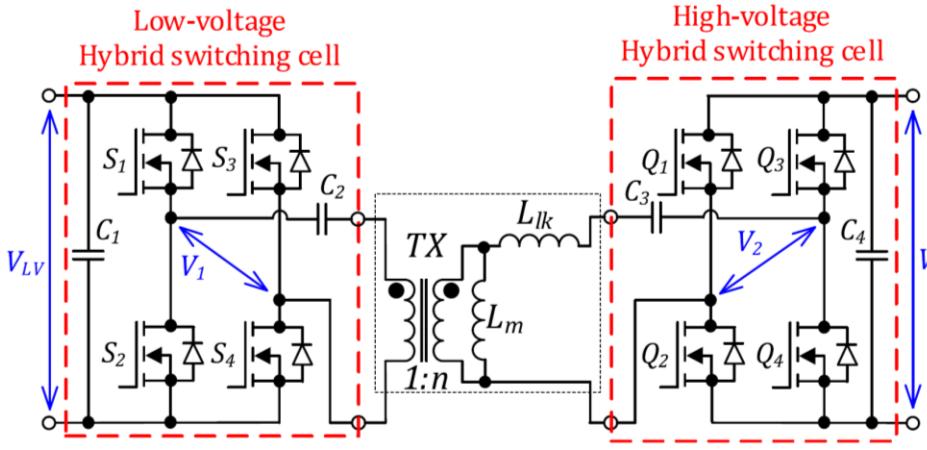
CF FBI-FBR boost mode
($V_{out}=20V$, $P_{out}=200W$)



CF 1Sw-FBR buck mode
($V_{out}=740V$,
 $P_{out}=3.1kW$)

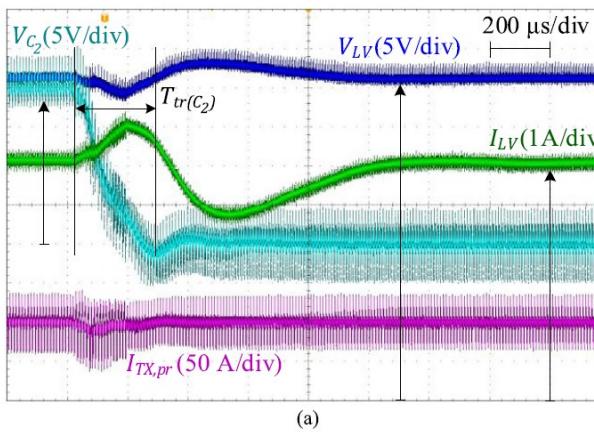
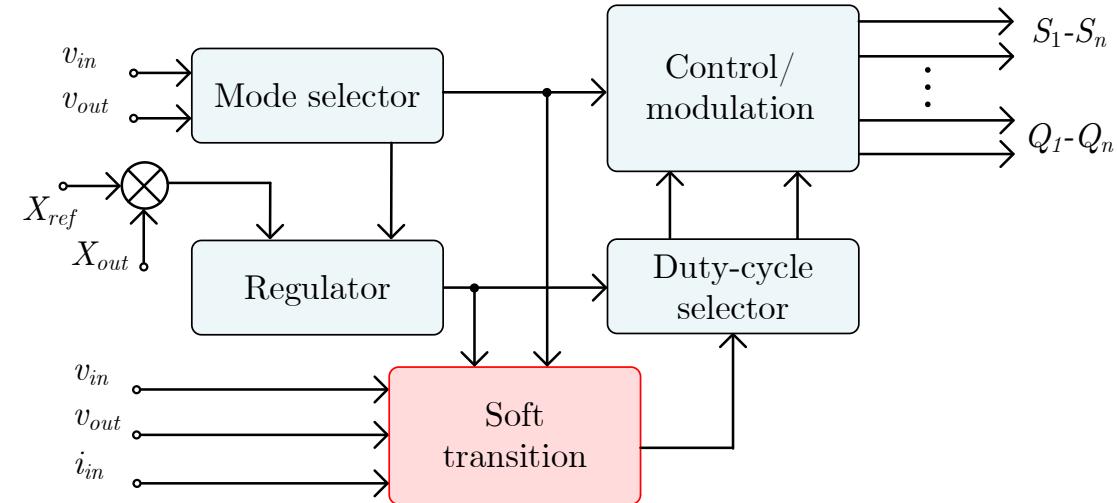
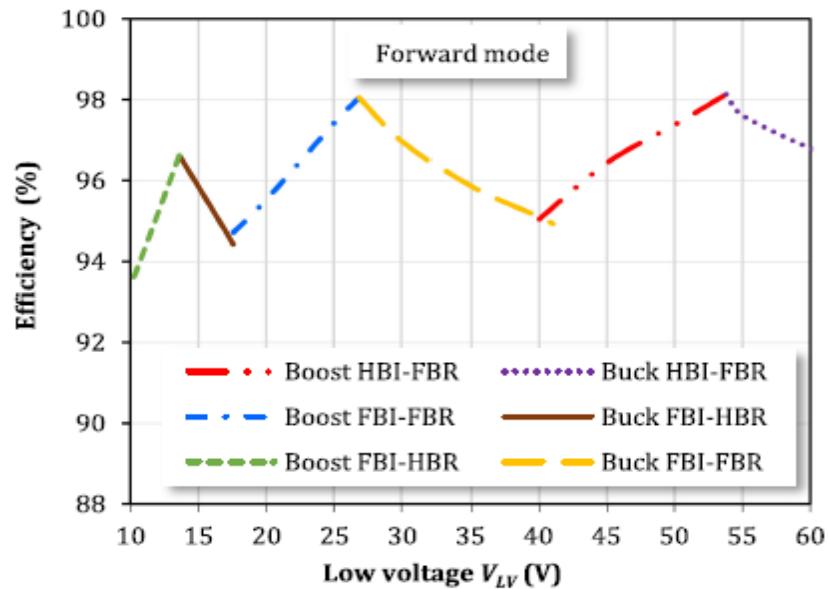
WIDE INPUT VOLTAGE RANGE CONVERTER FOR PV AND DC BUILDING APPLICATIONS

- A Bidirectional Isolated Hexamode DC-DC Converter
 - V_{in} (10-60 V) and V_{out} (350/700V).
 - 350W prototype with Max efficiency (>98%).
 - Can support both PV and Battery charging.

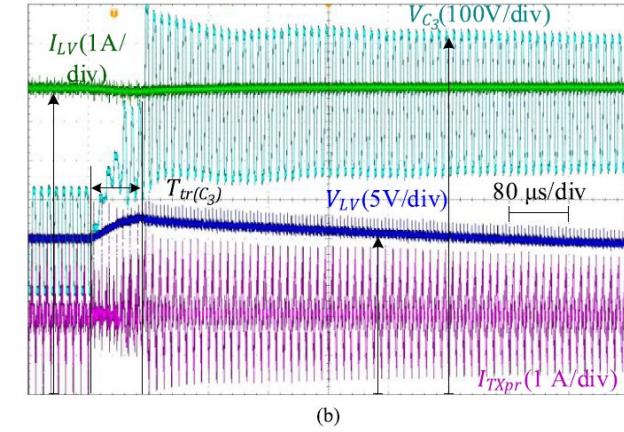


CHALLENGES IN TMC-BASED WIDE-VOLTAGE RANGE TOPOLOGIES

- Integration of TMC for the control system
- Implementation of transition between topologies
- Step change in efficiency after



(a)



(b)



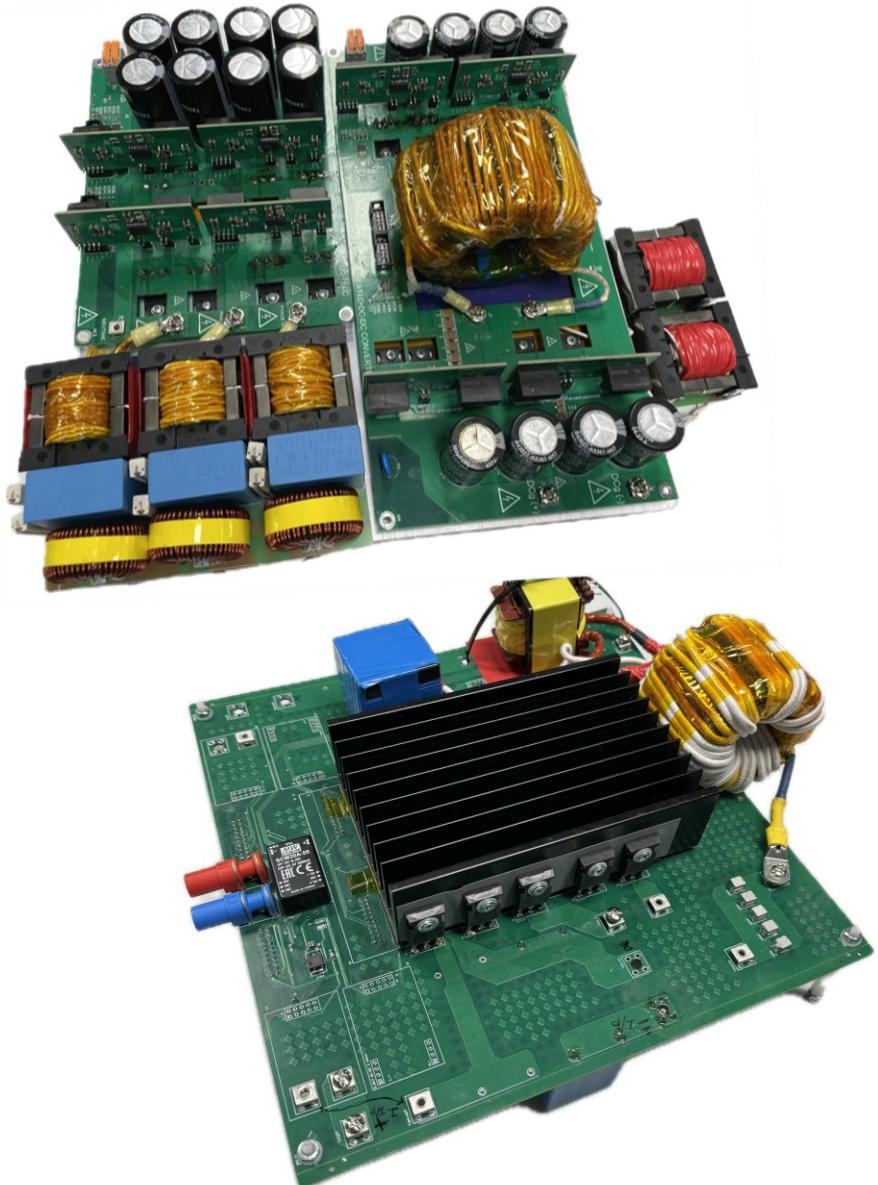
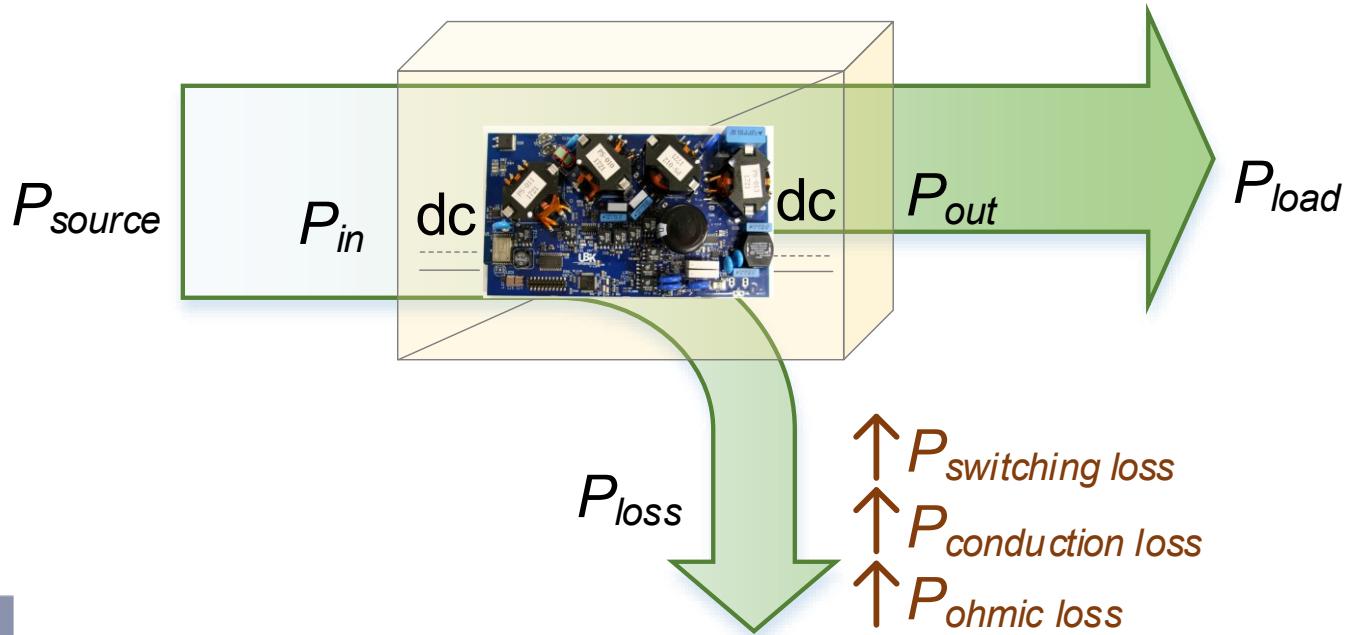
BREAKING LIMITS WITH PARTIAL POWER PROCESSING (PPP)

Dr. Neelesh Yadav



FULL POWER CONVERTERS

- **Full Power Converter (FPC):**
all power is processed by a dc-dc converter
components. **Losses are a fraction of total power.**

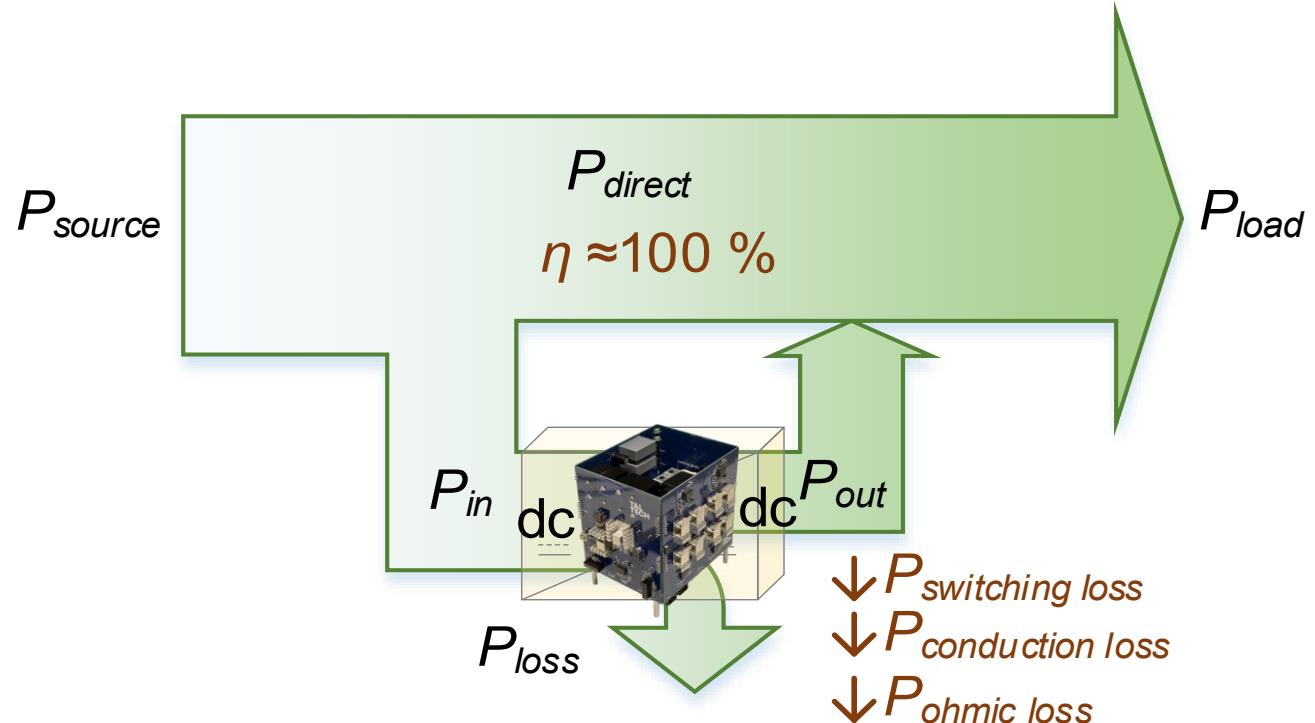


PARTIAL POWER CONVERTER (PPC)

- **Partial Power Converter (PPC):**

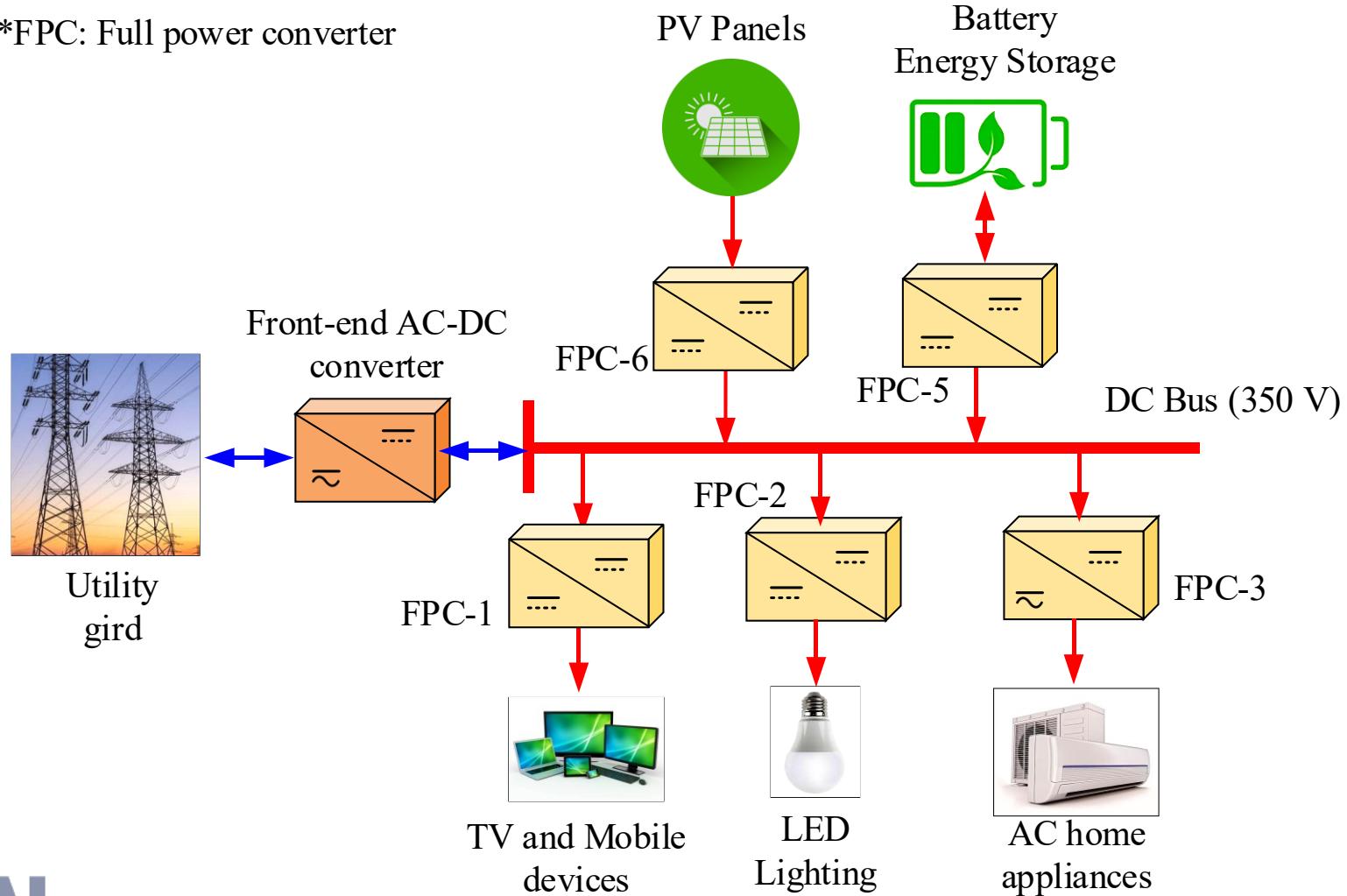
only a fraction of the power is processed by an isolated dc-dc cell. **Losses are a fraction of processed power**

- Reduced losses
- Lower component ratings
- Smaller weight and size
- Potentially faster dynamics



PPC APPLIED TO DC BUILDINGS

*FPC: Full power converter



A Typical DC microgrid for a building

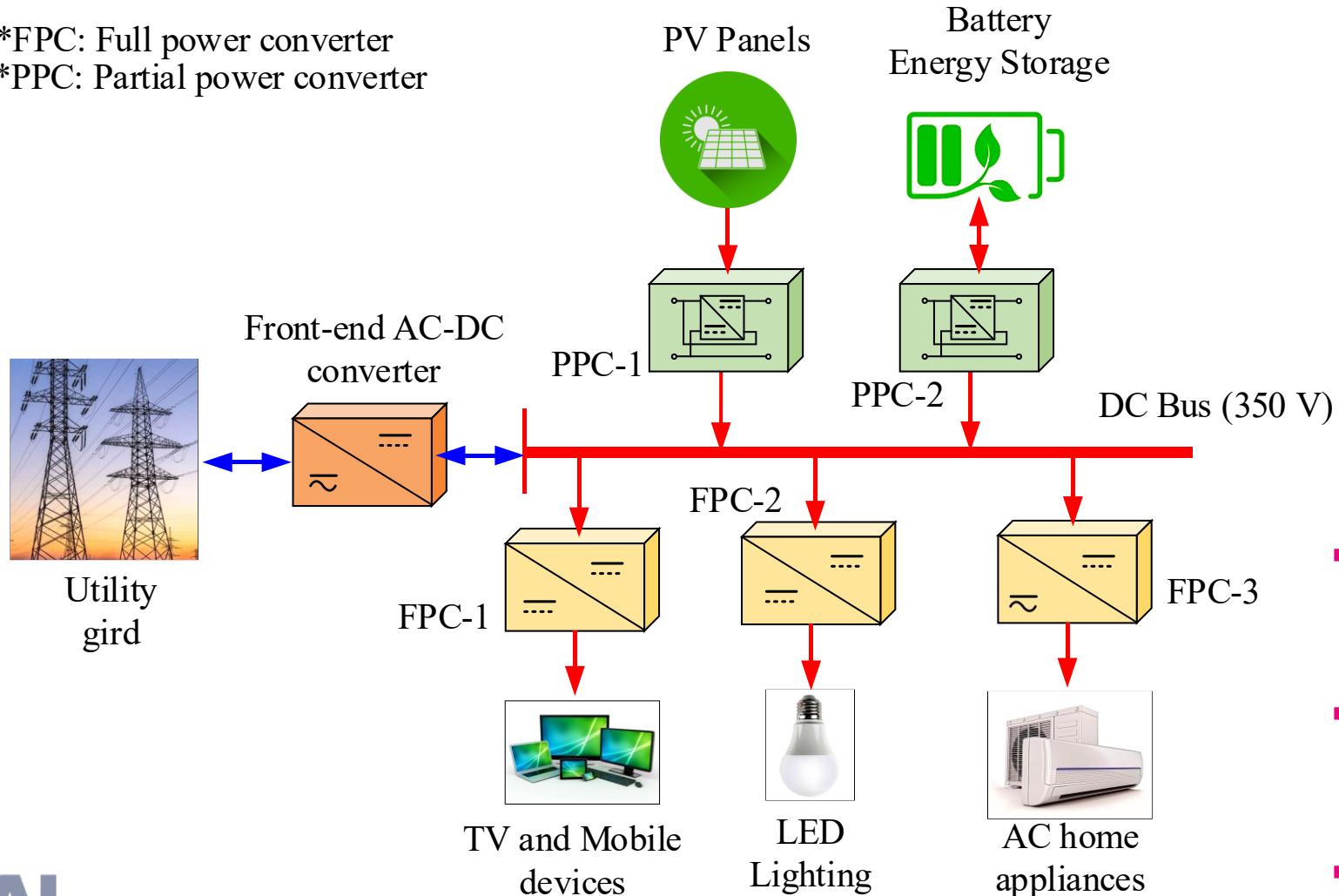


- **More losses:** Process all power in a wide voltage range, **efficiency** (97..98%)
- **Higher semiconductors cost:** Higher current and voltage rating on the converter port
- **Cooling required:** results in higher cost and volume

PPC APPLIED TO DC BUILDINGS

*FPC: Full power converter

*PPC: Partial power converter



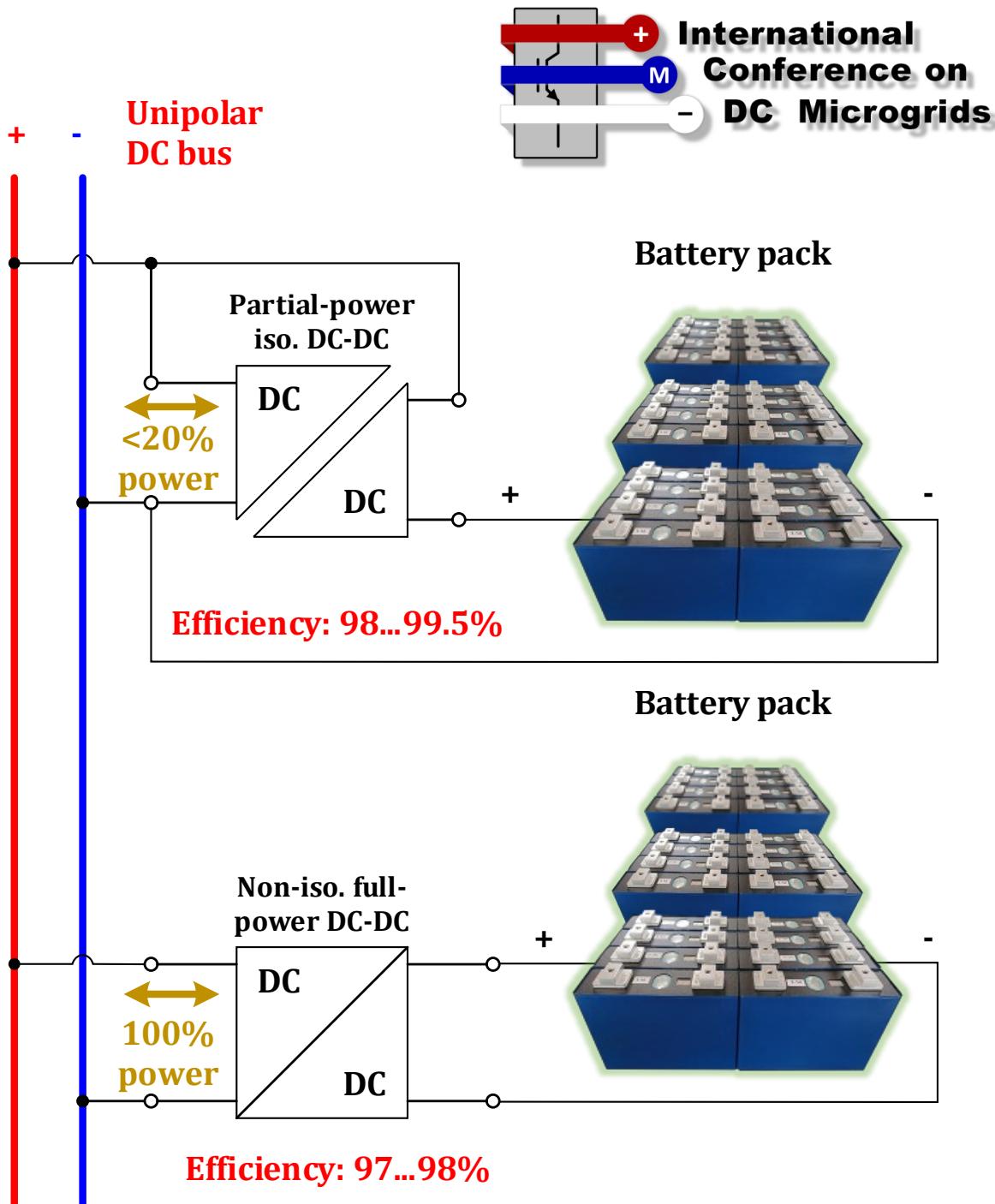
Partial power converter based DC microgrid for a building



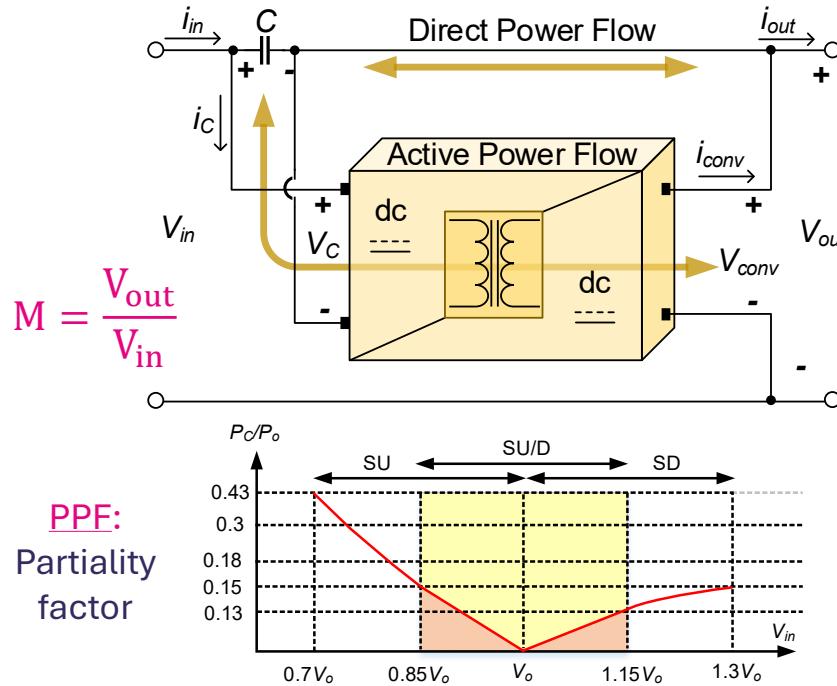
- **Reduced losses:** Process only a fraction of the power, **highly efficient (98...99.5%)**
- **Low semiconductors cost:** Reduced current rating on one converter port, reduced voltage rating on the other
- **Reduced cooling requirement:** results in higher cost and volume

PPC vs FPC

- Full power converter needs to process all power in a wide voltage range – **more losses**
- Partial power converter deals with only a **fraction** of power and thus could be more **efficient** and **low-cost**
- Reduced current rating on one converter port, reduced voltage rating on other – **reduced semiconductors' cost**
- Reduced cooling requirements, resulting in reduced cost and volume
- Higher power **density**
- Potentially faster **dynamics**



PPC CLASSIFICATION



Type II S-PPC:

Series-input-parallel-output (SIPO)

S-PPC

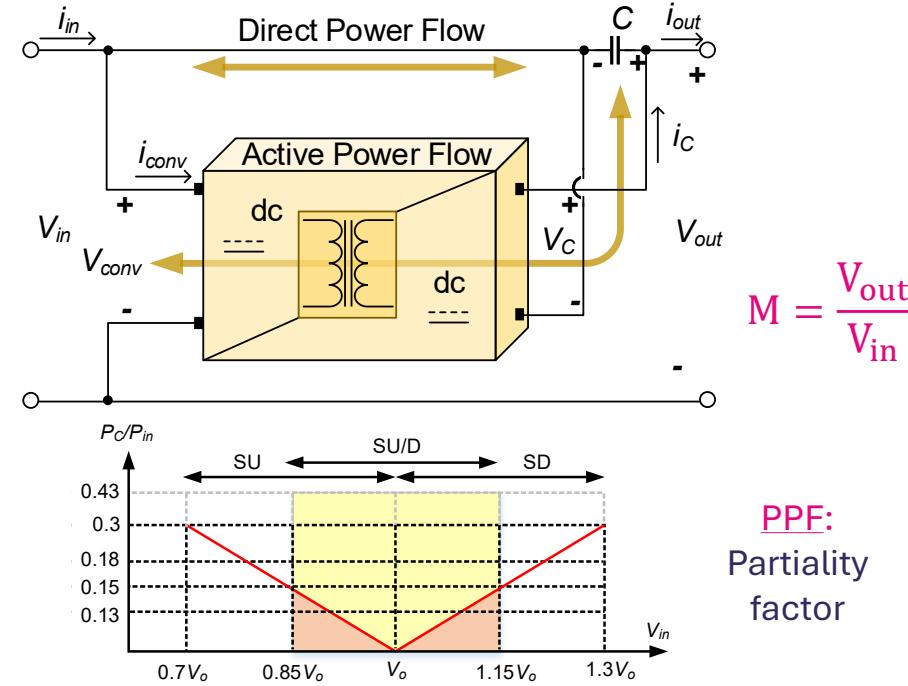
1. DC-DC Stage (M)

- Step-up
- Step-down
- Step-up/down

2. Configuration

- Type I
- Type II
- *Derived*

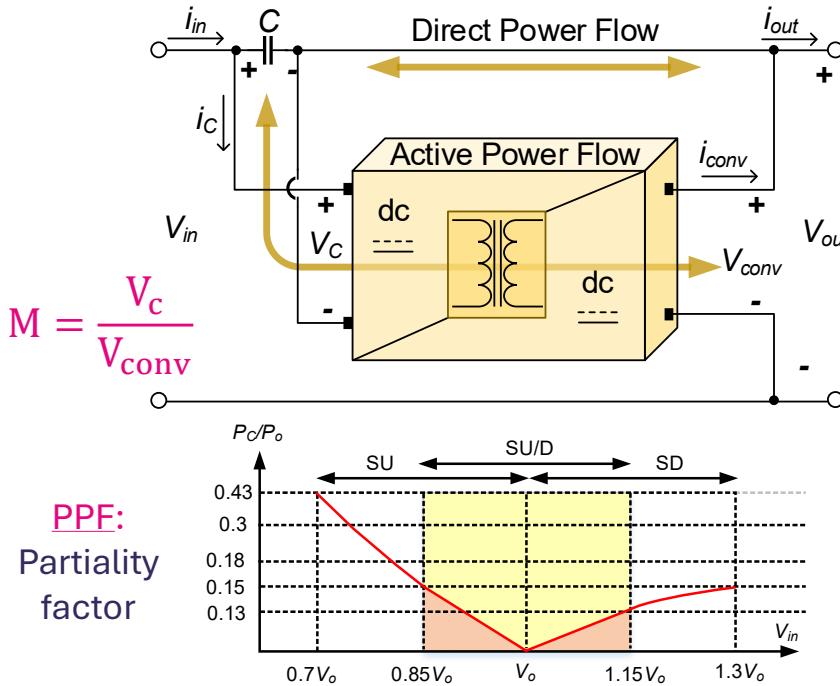
All derived configurations exhibit equivalent characteristics as the original configurations



Type I S-PPC:

Parallel-input-series-output (PISO)

PPC CLASSIFICATION

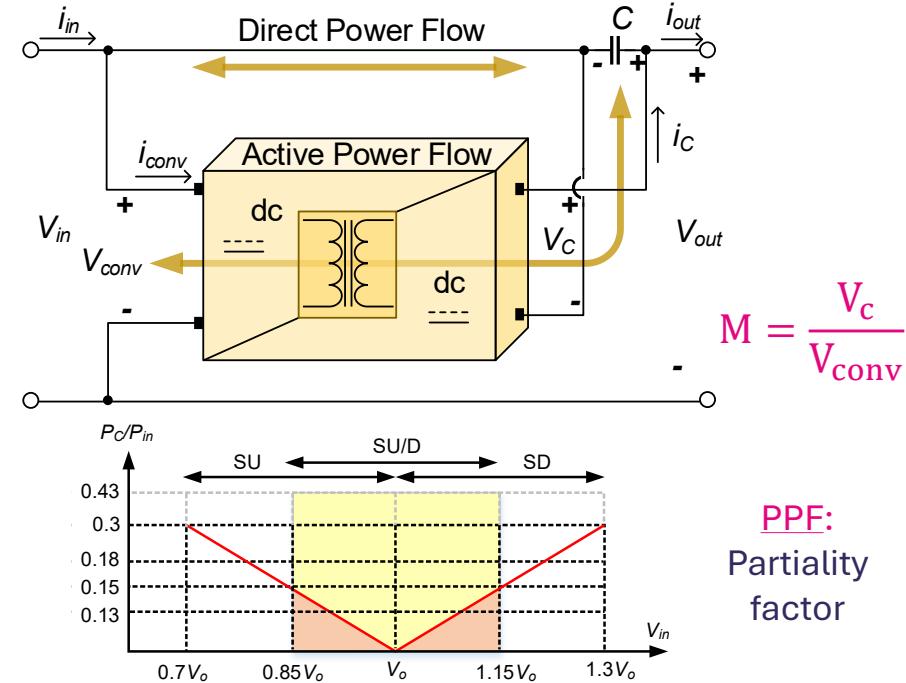


Type II S-PPC:

Series-input-parallel-output (SIPO)

DC-DC Converter

1. Topology Ports
 - Current-Fed (CF)
 - Voltage-Fed (VF)
2. Voltage Gain (M_C)
 - Buck
 - Boost
 - Buck-Boost
3. Isolation
 - Non-Isolated
 - Isolated

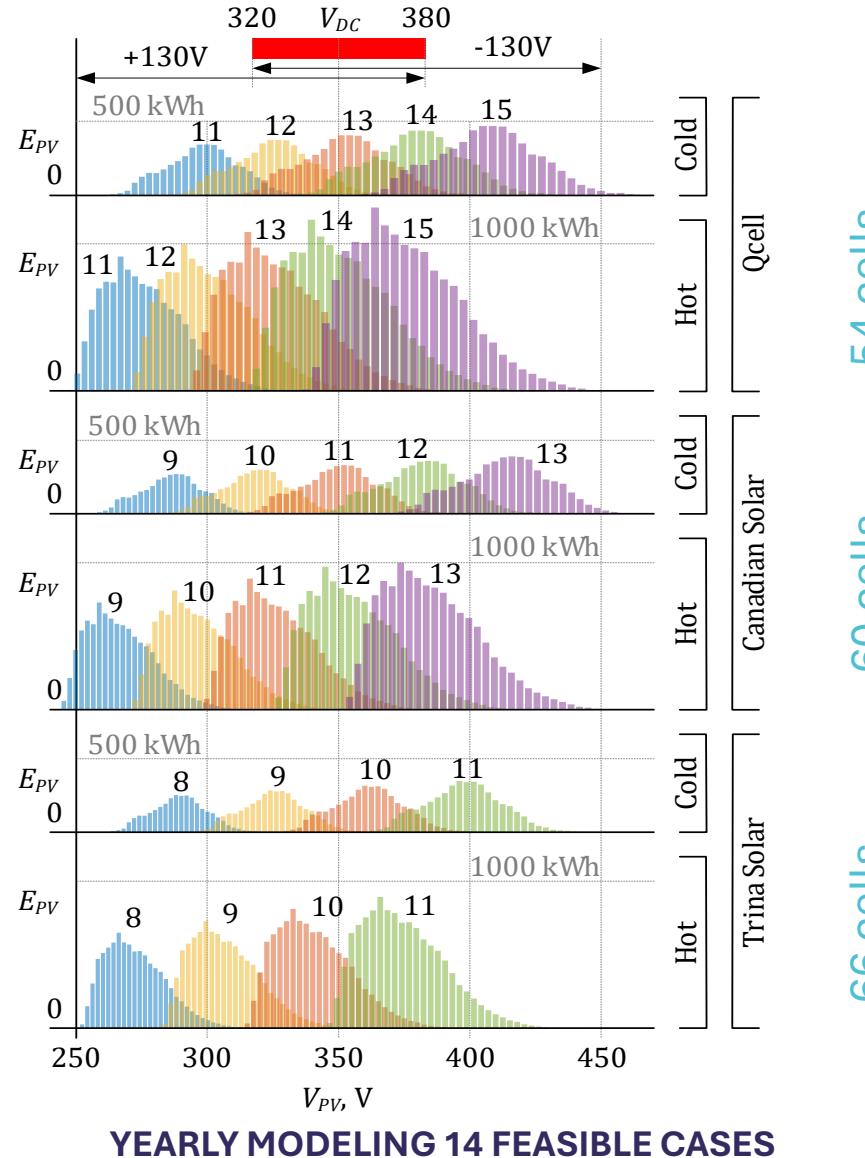
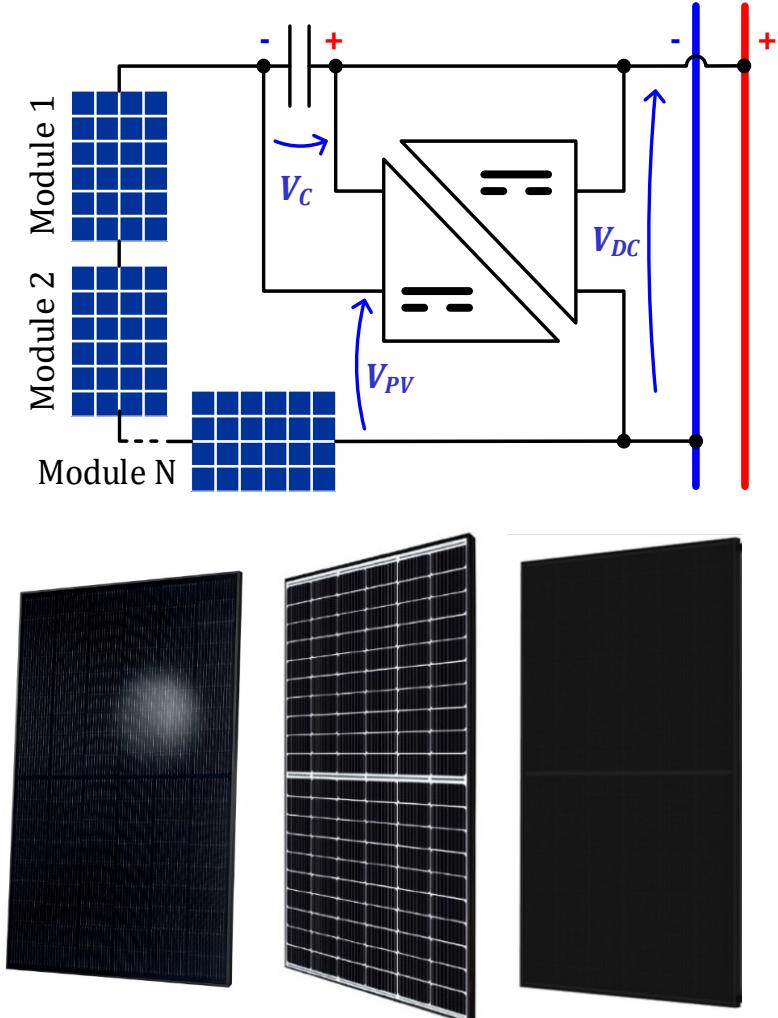


Type I S-PPC:

Parallel-input-series-output (PISO)

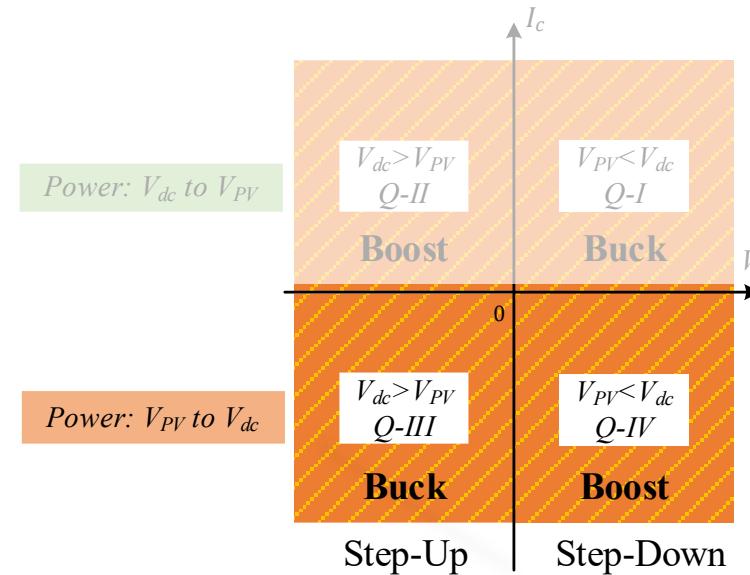
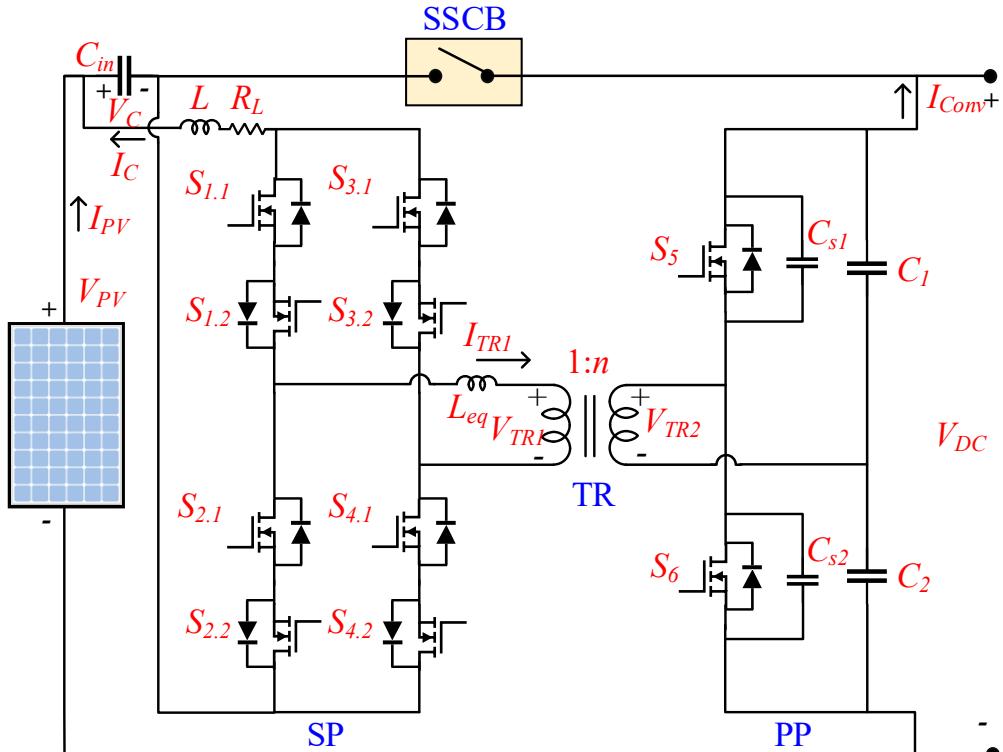
PARTIAL POWER CONVERTERS IN PV APPLICATIONS

- Residential droop-controlled DC microgrid based on Current/OS system can normally vary in the range of $350V \pm 30V$

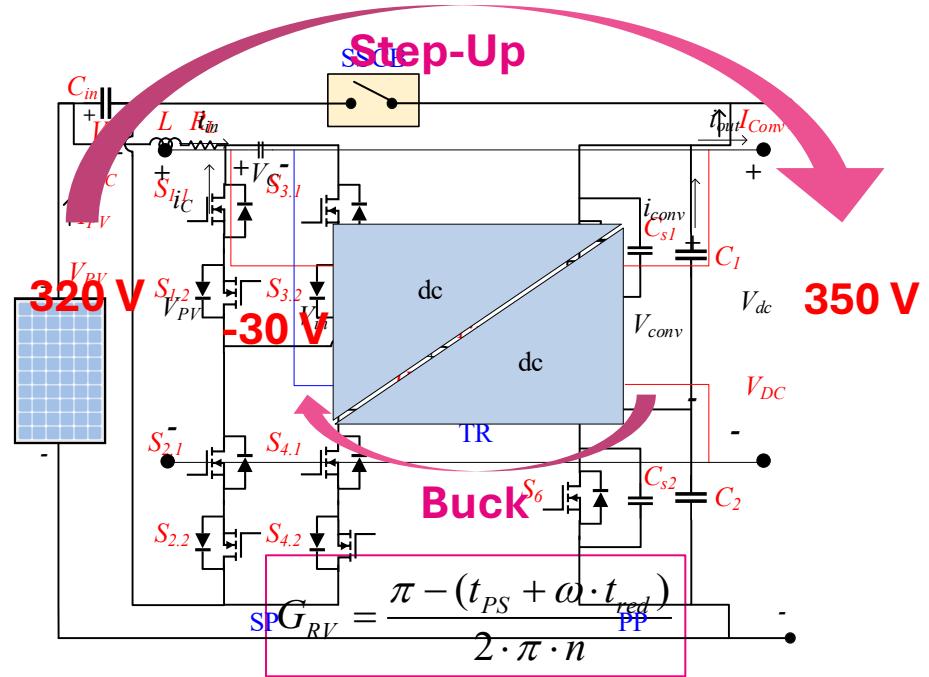


TOPOLOGY SIMPLIFICATION

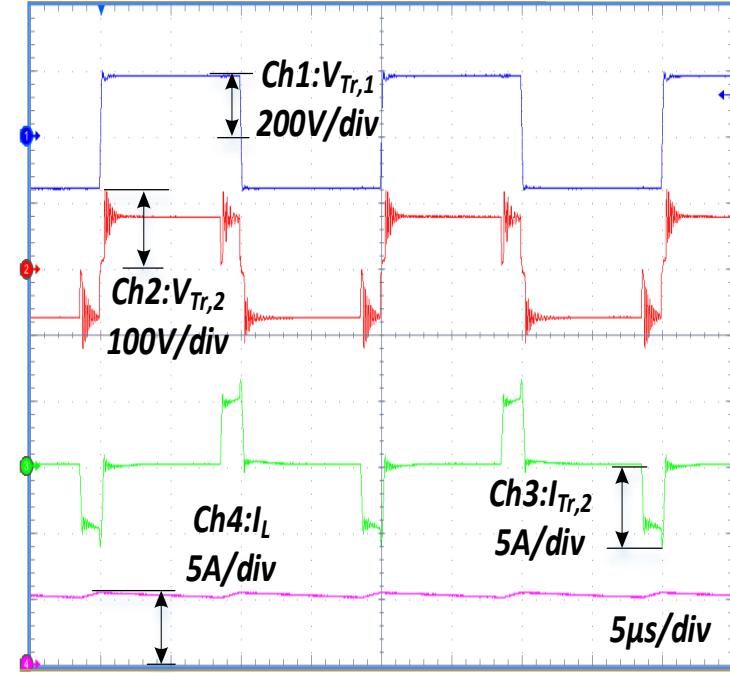
- Current-fed full-bridge converter



STEP-UP AND BUCK OPERATION MODE

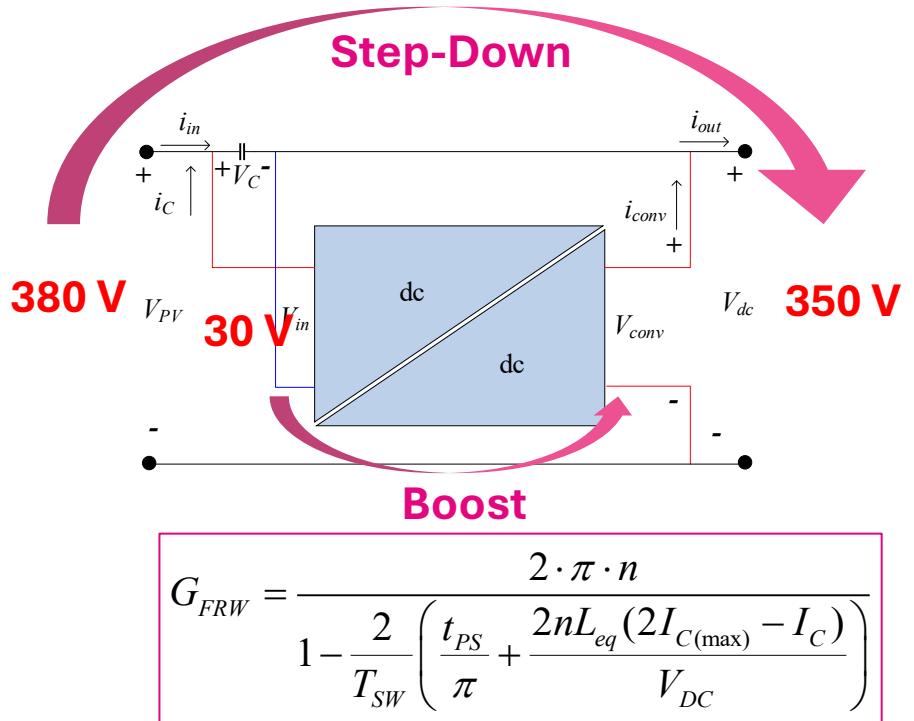


- Power flow from LV to HV
- dc-dc stage gain (G_{RV}) can be reduced to almost zero
- Can regulate near-zero LV port voltage

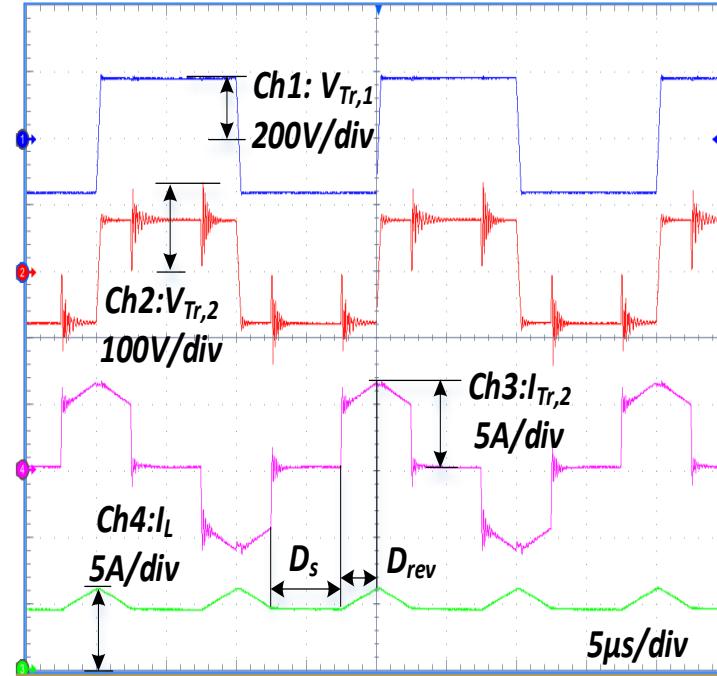


Current-voltage waveforms while working with $I_{out}=5\text{ A}$ $V_{in}=350\text{ V}$ and $V_{out}=350.5\text{ V}$

STEP-DOWN AND BOOST OPERATION MODE



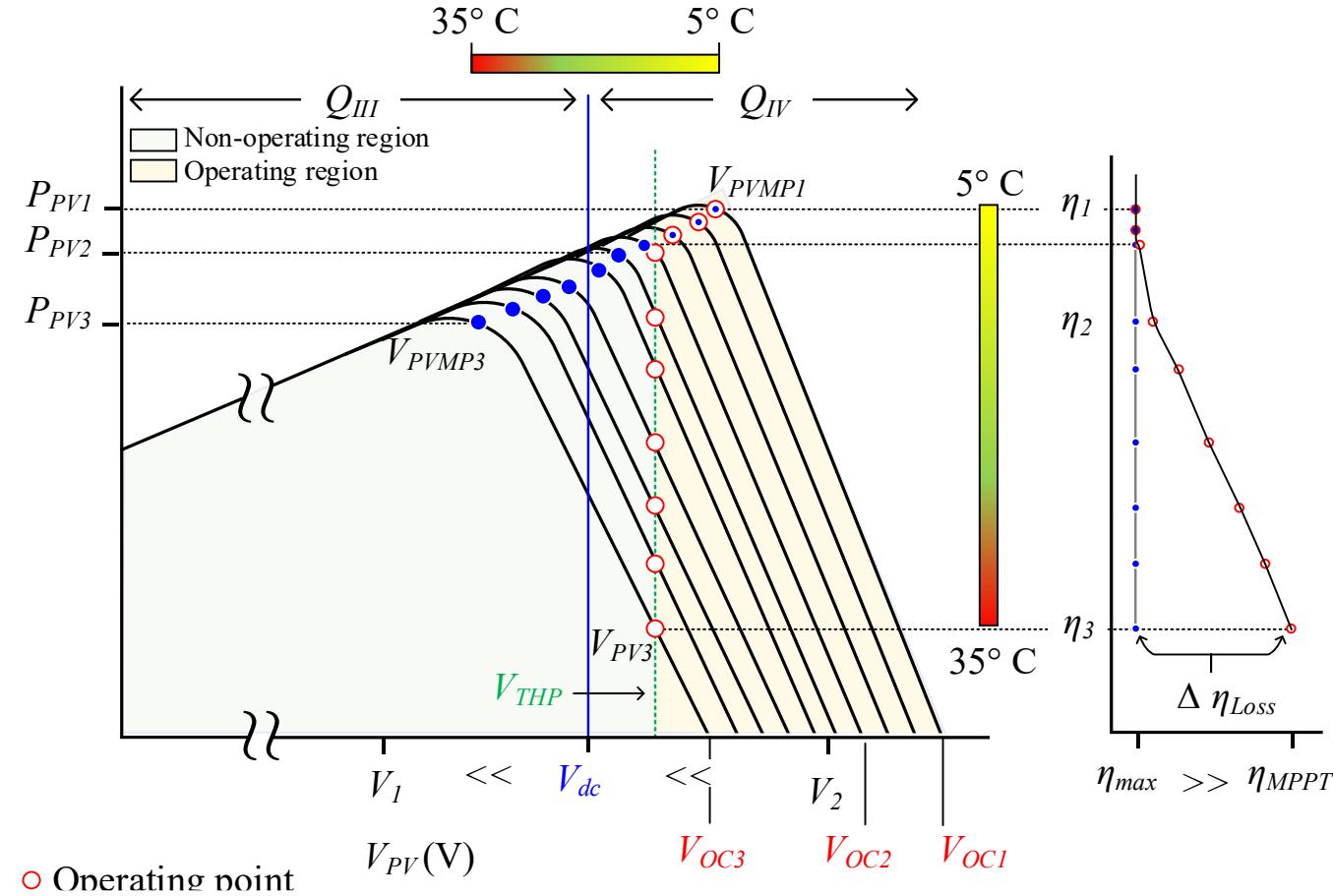
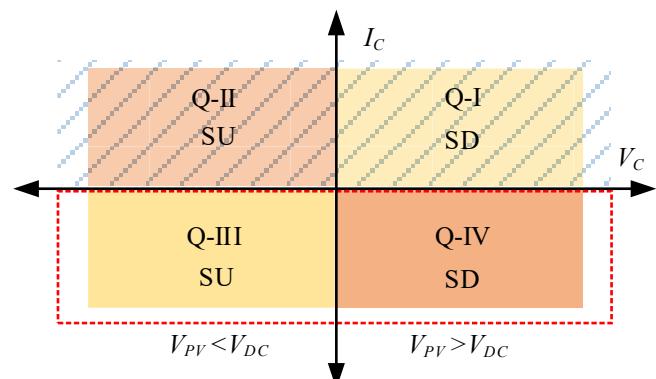
- Power flow from LV to HV
- dc-dc stage gain (G_{RV}) voltage gain depends on the power
- limitations in boosting a very low voltage at the LV port
- This means that the converter can easily handle the zero series port voltage



Current-voltage waveforms while working with
 $I_{out} = 5 \text{ A}$ $V_{in} = 348 \text{ V}$ and $V_{out} = 350 \text{ V}$

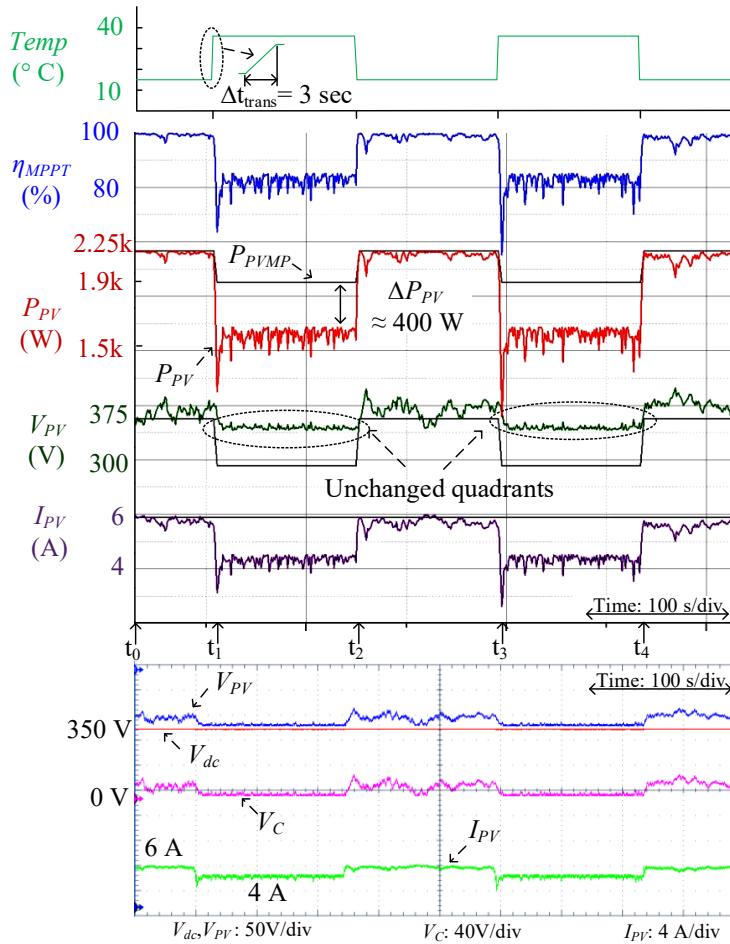
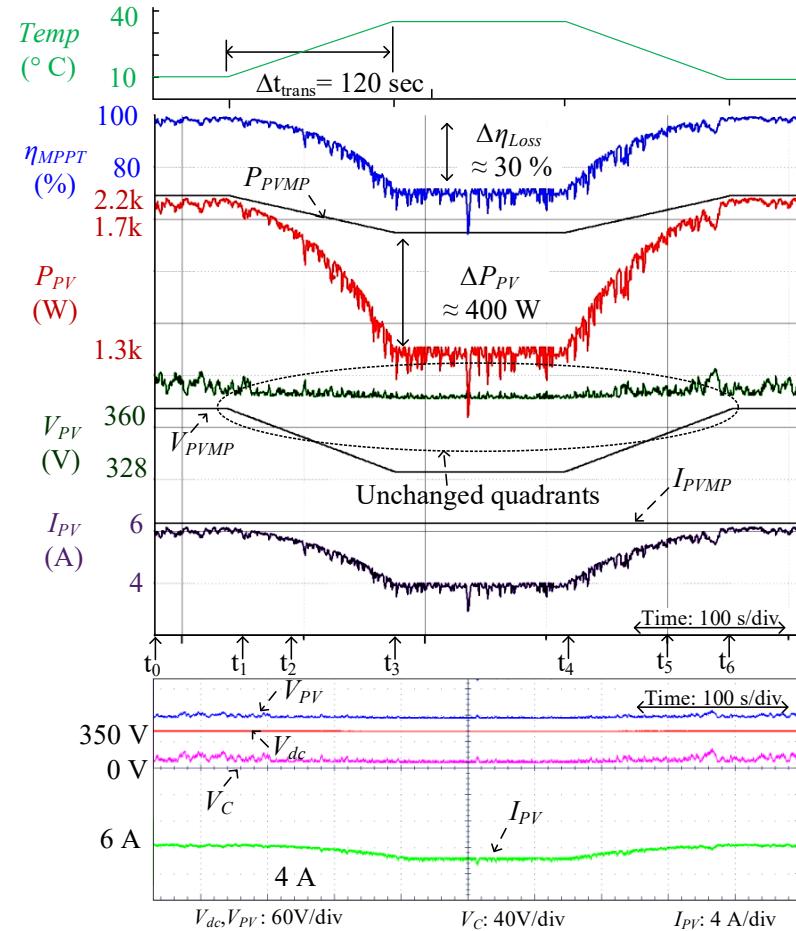
MPPT ISSUES IN STEP-UP/DOWN PPC – FORMULATION

- Q-III \leftrightarrow Q-IV with change of polarity of V_C
Causes MPPT efficiency drop.
- Typical modulations offers few challenges while operating mode at/or near zero partiality ($K_{pr}=0$) i.e. $V_{PV} \approx V_{dc}$
- PPC does not change its quadrants because capacitor **does not have enough charge to transfer energy to inductor at low K_{pr}** , which is needed for current control.



N. Yadav, at al. "Improved Maximum Power Point Tracking Algorithm for Step-Up/Down Partial Power Converters Operating Around Zero Partiality," in **IEEE J. Emerg. and Sel. Topics in Power Electron.**, vol. 12, no. 2, pp. 1984-1994, April 2024.

MPPT ISSUES IN STEP-UP/DOWN PPC – EXPERIMENTAL



- At/near zero voltage at the series port converter cannot regulate the current
- Converter gets stuck in one quadrant and MPPT efficiency deteriorate
- In the given experimental example, MPPT efficiency drops by 23.5%

IMPROVED MPPT OMITTING DEAD ZONE- CONCEPT

When V_{PV} decreases into the DZ

PPC controller saturation

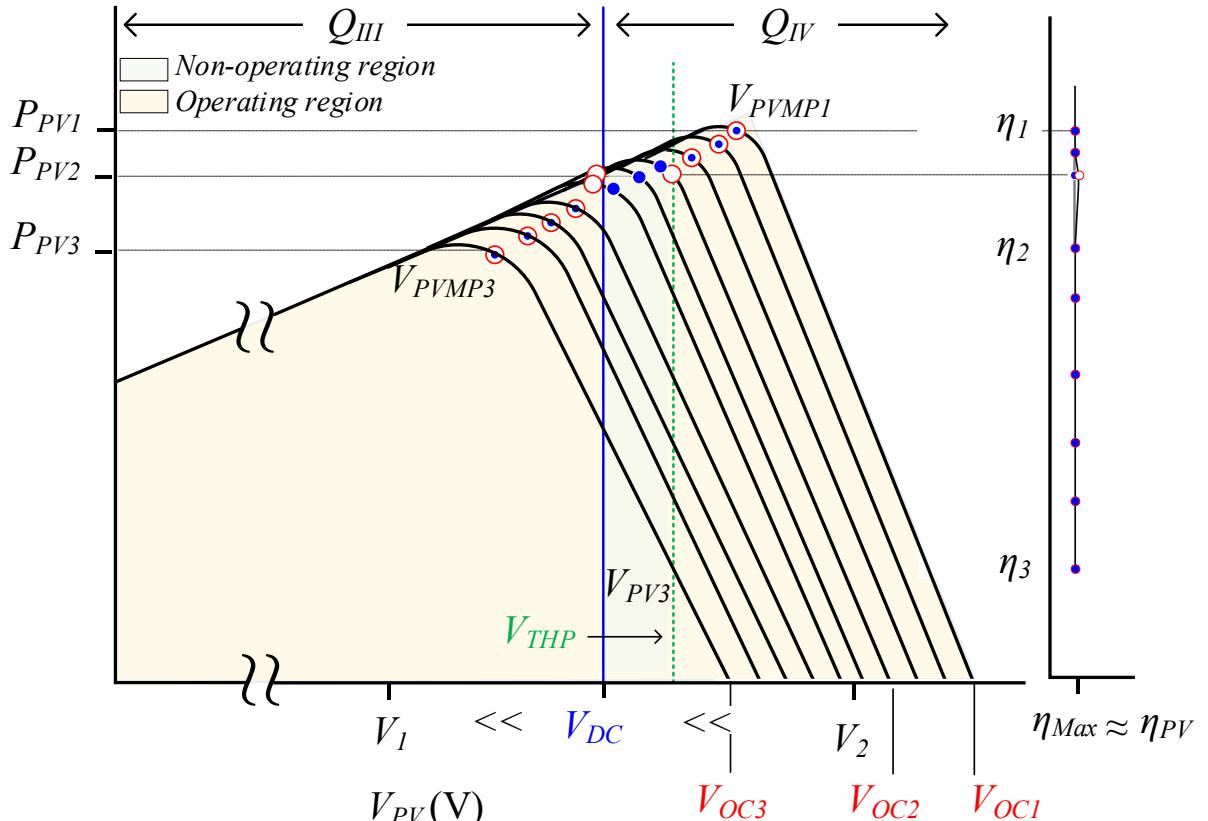
Critical Dead Zone (CDZ)

Change of quadrant forcefully

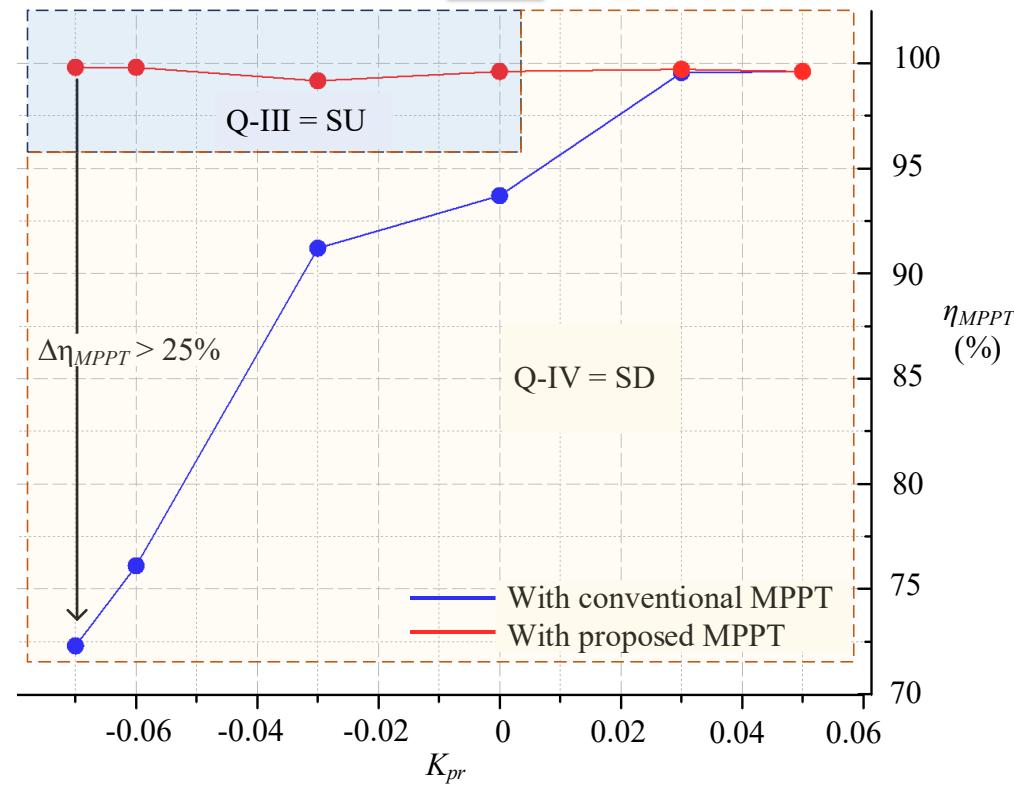
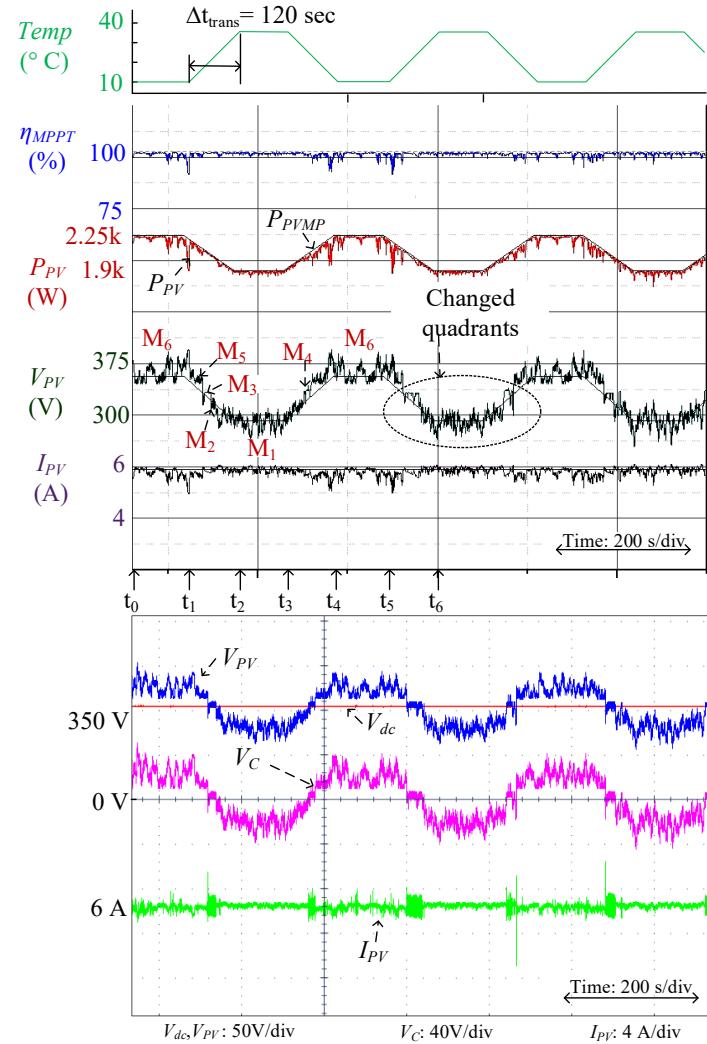
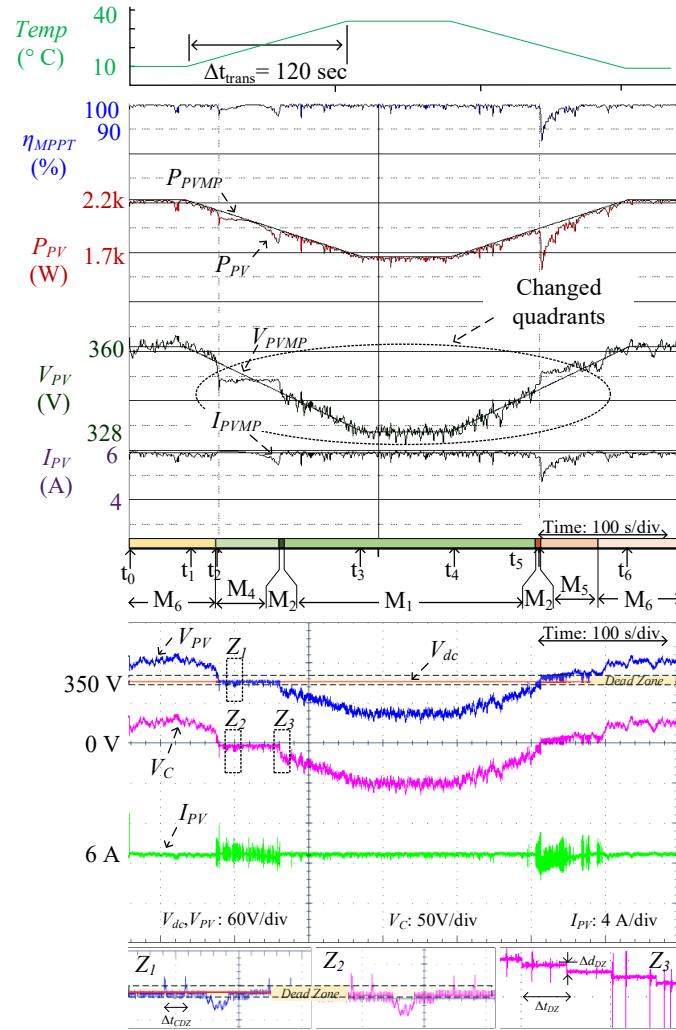
Proposed control algorithm pushes the operating point

PPC changes its operating quadrants
(Q-IV \rightarrow Q-III) and (SD \rightarrow SU)

- The proposed algorithm avoids the saturation of the controller
- Gets a new operation point to enhance the MPPT efficiency.



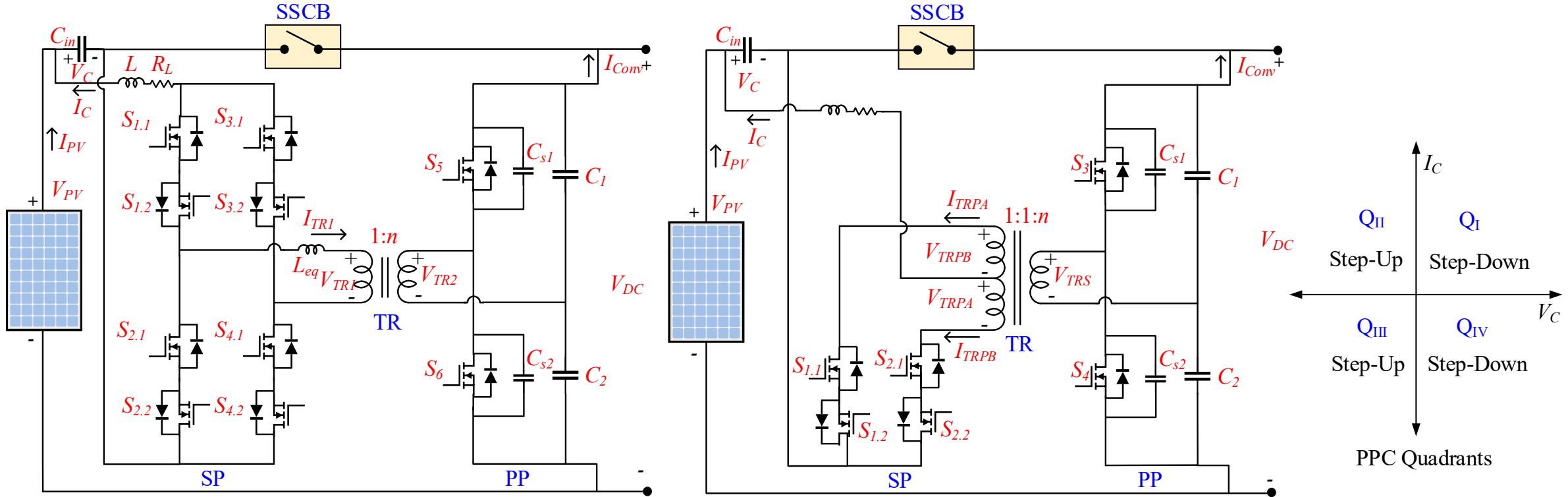
IMPROVED MPPT IMPLEMENTATION



- Quadrant switching results in significant transients, but allows to improve MPPT overall
- A better solution is needed if PV string is likely to operate near the dead zone

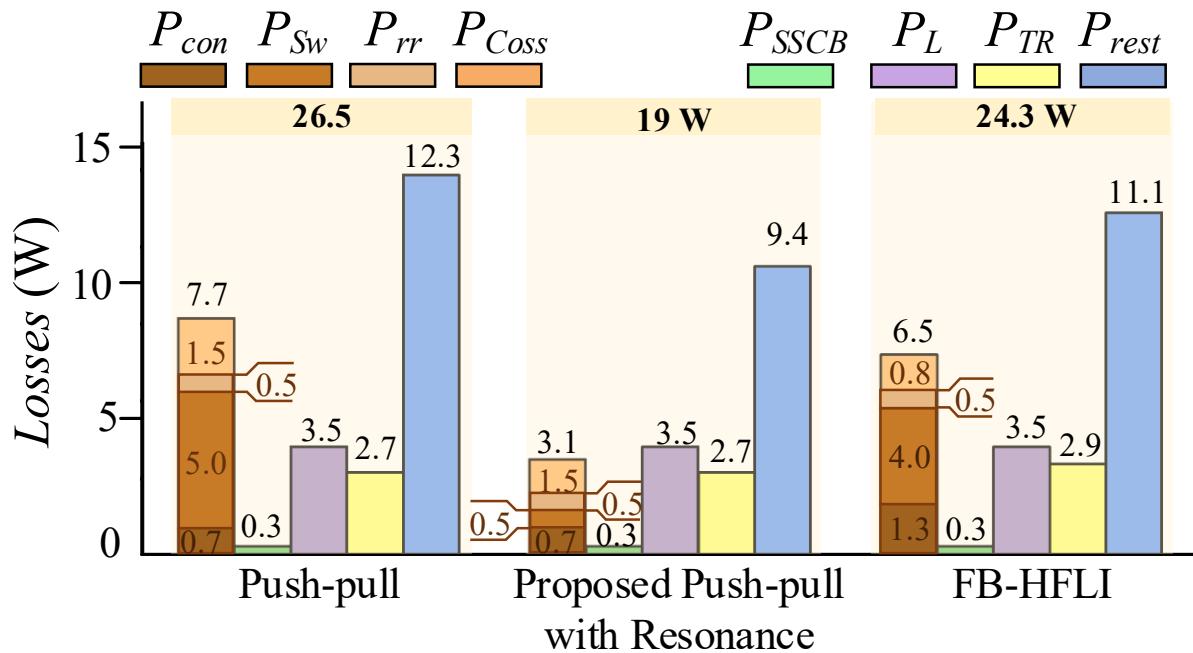
PUSH-PULL TOPOLOGIES REDUCING THE NUMBER OF 4-QUADRANT SWITCHES

- Current-fed full-bridge converter can be replaced with the current-fed push-pull topology



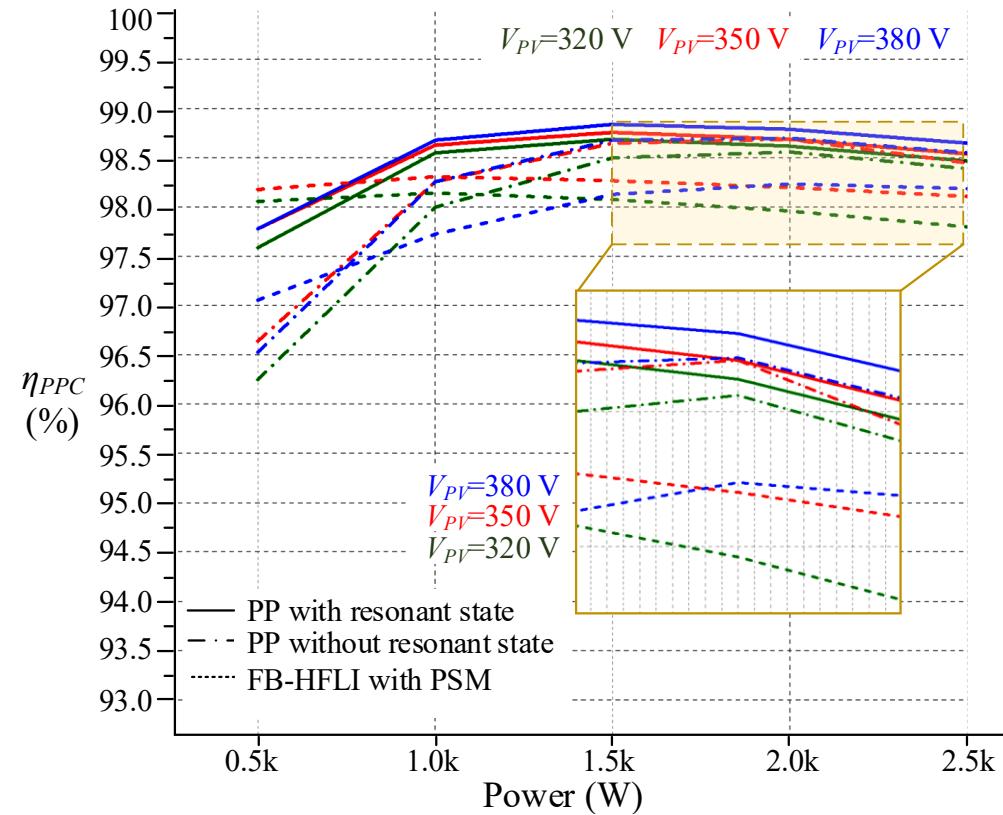
COMPARISON OF IMPLEMENTATIONS

- Power losses at 2.5kW/350V/30V considering best possible implementation
- The CF push-pull with resonant switching can outperform FB topology with resonant switching as well

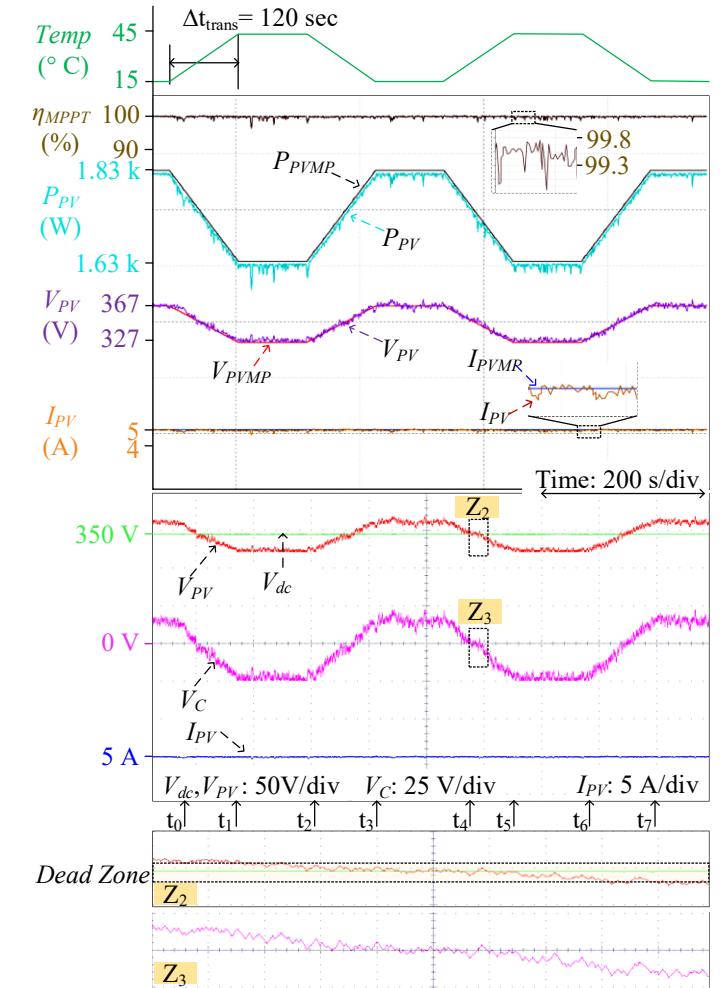


Topology	At 2kW, $V_{PV}=320$ V, $V_{DC}=350$ V		Price, p.u.
	Low Voltage side Switch stress	Voltage (V)	
FB-HFLI	75	85	1.4
Push-pull	220	339	1.0
Proposed push-pull	192	328	1.0

OPERATION WITH PV STRING



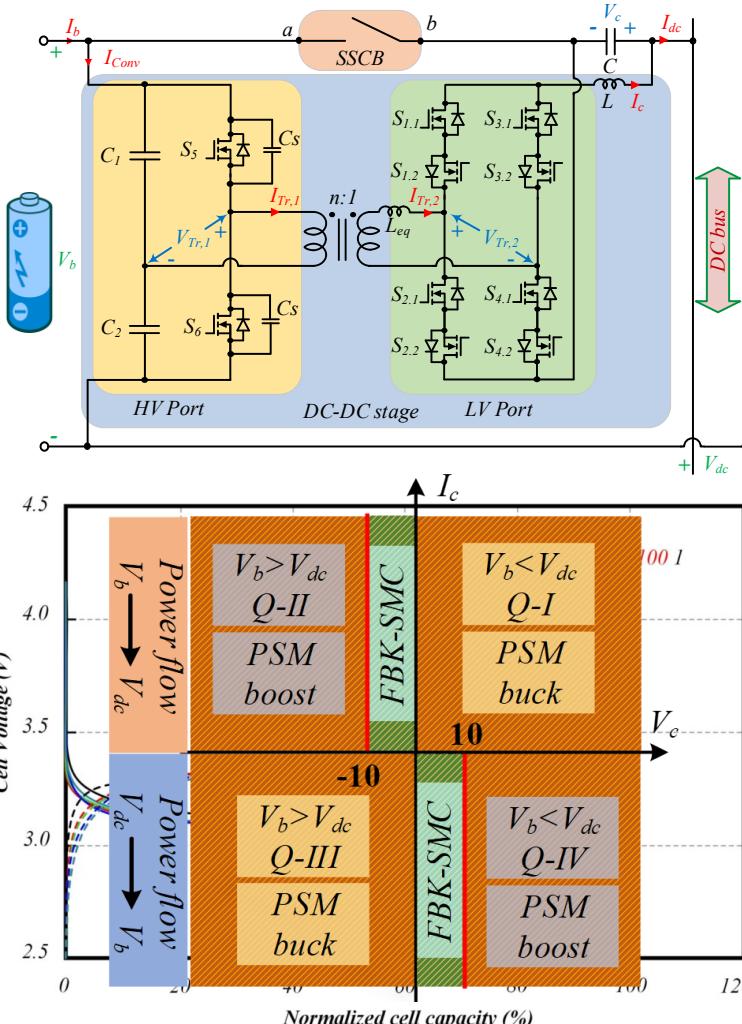
- This topology can be recommended for application with narrow voltage regulation range, i.e., low partiality



DC BUILDING APPLICATIONS SECOND LIFE BATTERY ENERGY STORAGE INTEGRATION



- Current-fed implementation limits current stress on components
- Can manage current control at zero ser. voltage
- RMS current of capacitor is constrained
- Series port utilizes bidirectional switches for 4-quadrant operation and full soft switching
- Half-bridge implementation of the parallel port improves efficiency of the isolation transformer
- Low-cost power semiconductors
- Embedded solid-state circuit breaker



Bat. voltage	V_b	350 V($\pm 30V$)
DC μ G voltage	V_{dc}	350 V($\pm 30V$)
Rated power	P_{reated}	4 kW
Rated power of dc-dc cell	P_{Conv}	750 W
Switching frequency	f_{SW}	75 kHz

- $V_{battery_nominal}$: 350 V [LiFePo₄: 109 cell]
- At SoC = 90 % $109 \times 3.2 V \approx 380 V$
- At SoC = 10 % $109 \times 2.9 V \approx 320 V$
- $V_{dc} = 320 V$ to $380 V$
- $I_{dc} = 10 A$ to $-10 A$

KEY FEATURES

- **Highest Efficiency:**

Achieves up to 99.45% efficiency, cutting energy losses and operational costs.

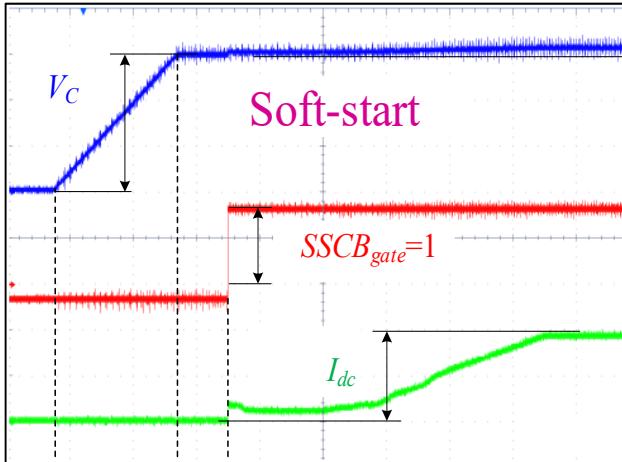
- **Embedded Protection:**

Built-in short- and open-circuit protection ensures long-term system reliability.

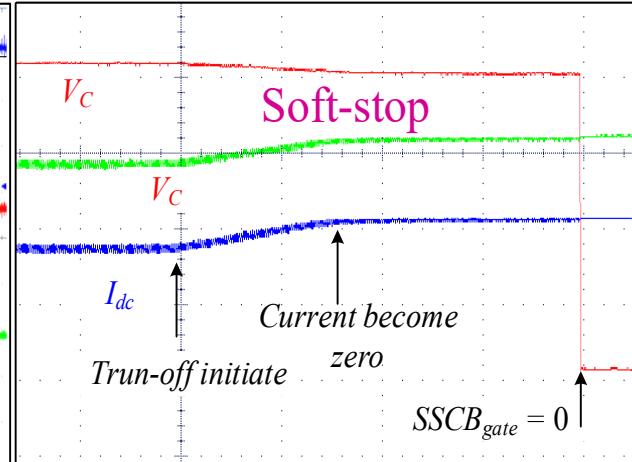
- **Soft-Start and Soft-Stop:**

Meets soft turn-on/off requirements to prevent false triggers of solid-state protection and reduce component wear-out.

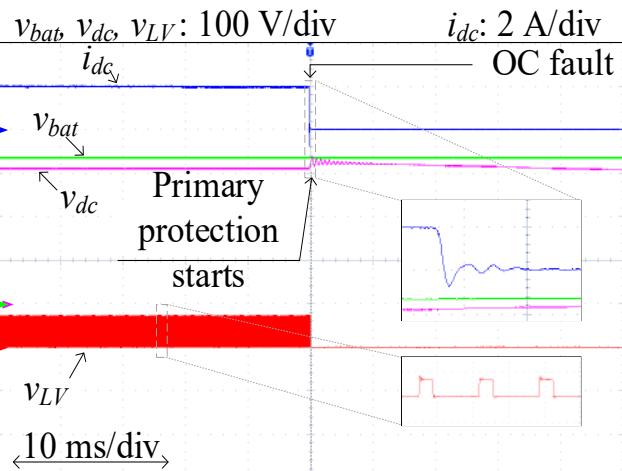
- **Soft-start**



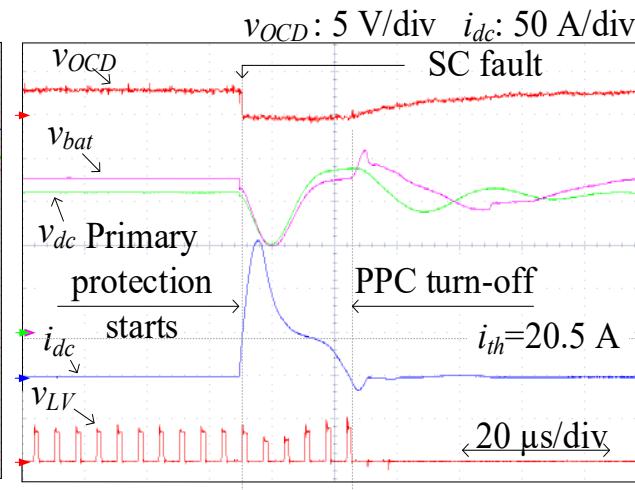
- **Short-stop**



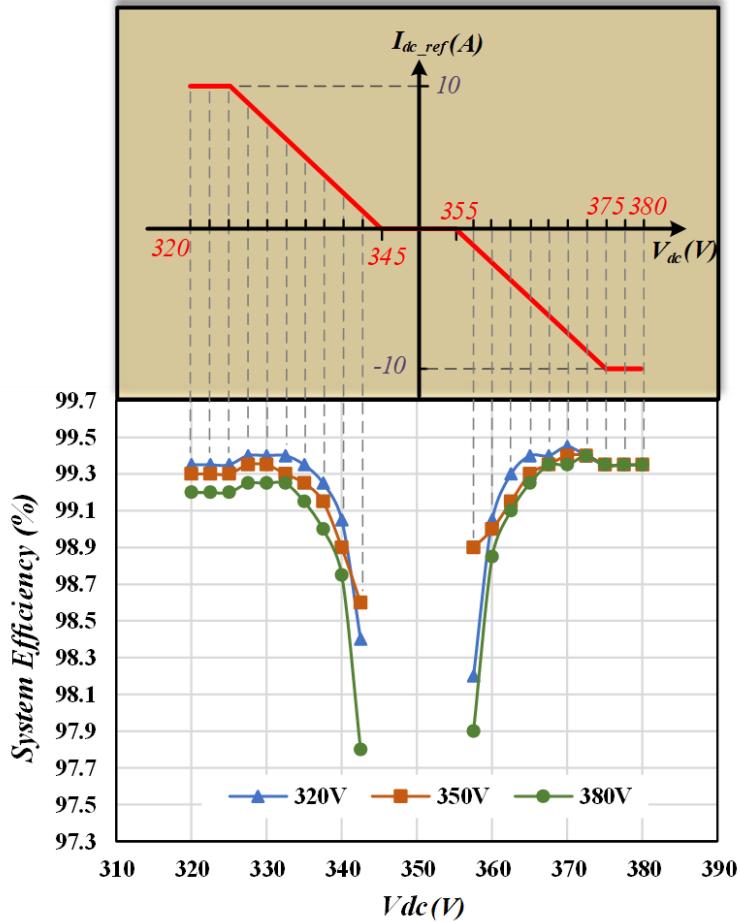
- **Open-circuit protection**



- **Short-circuit protection**



EXPERIMENTAL PROTOTYPE

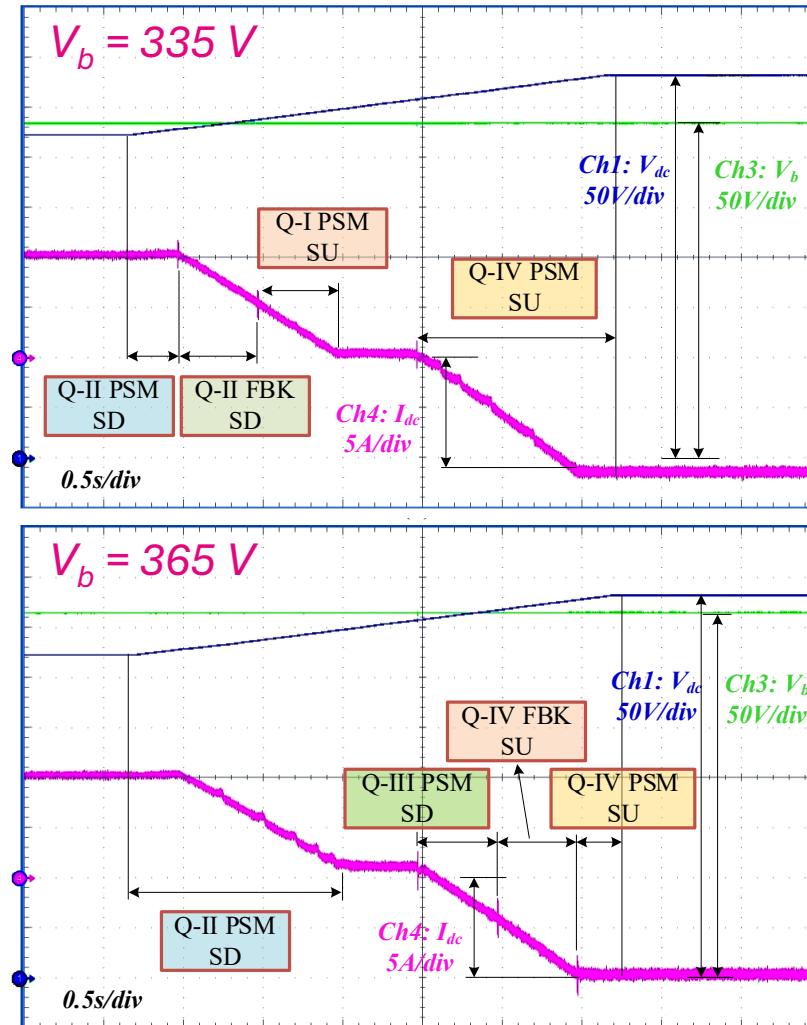
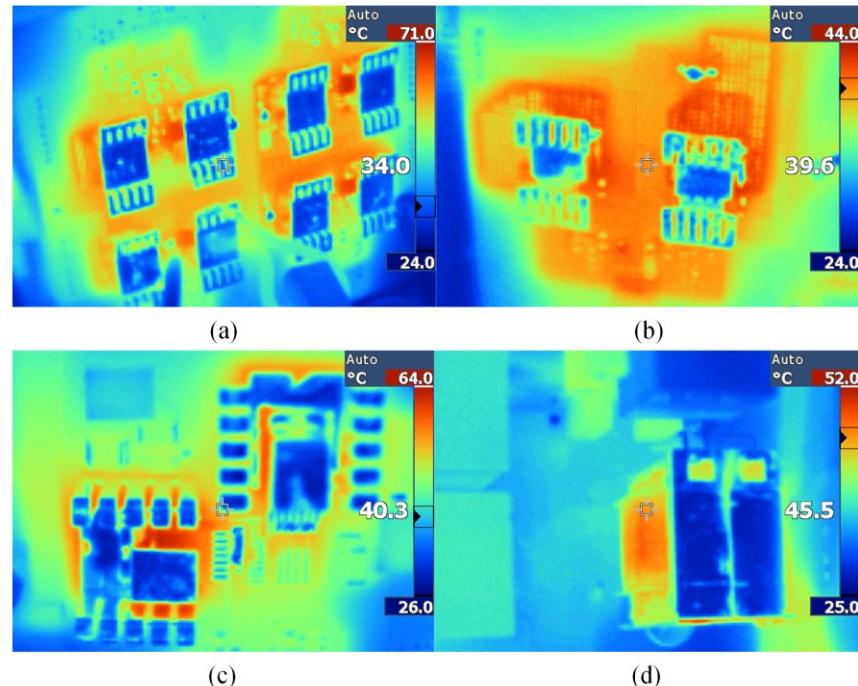


Function	Element	Order	Data	Units	Max	Min
U_{dc}	1	---	339.62	V	348.48	-0.74
I_{dc}	1	---	4.456	A	5.545	-0.002
P	1	---	1.5132k	W	1.8735k	-0.0007k
U_{dc}	2	---	334.31	V	334.96	-0.03
I_{dc}	2	---	-4.551	A	1.770	-5.647
P	2	---	-1.5213k	W	0.0054k	-1.8871k
η_{ta1}	---	---	99.469	%	216.145	-994.956

Parameters	Value/Type
LV port (Output) switches	BSC0403NSATMA1
HV port (Input) switches	G3R60MT07J
SSCB switches	UF3SC065030B7S
LV port inductor	164 μ H (CPER3231-820MC)
Transformer turns ratio	2.4:1 (EILP32 core)
HV port capacitors	20 μ F (R60IR51005040K)
Series capacitor	60 μ F (DCP4G056007GD4KSSD)
Switching frequency	75 kHz
Microcontroller	STM32G474

EXPERIMENTAL VALIDATION

- Topology morphing control enables smooth transition between modes
- PCB-soldered heatsinks are sufficient for thermal management (SSCB is the hottest part)
- Control considers **variations** in both DC and battery voltage

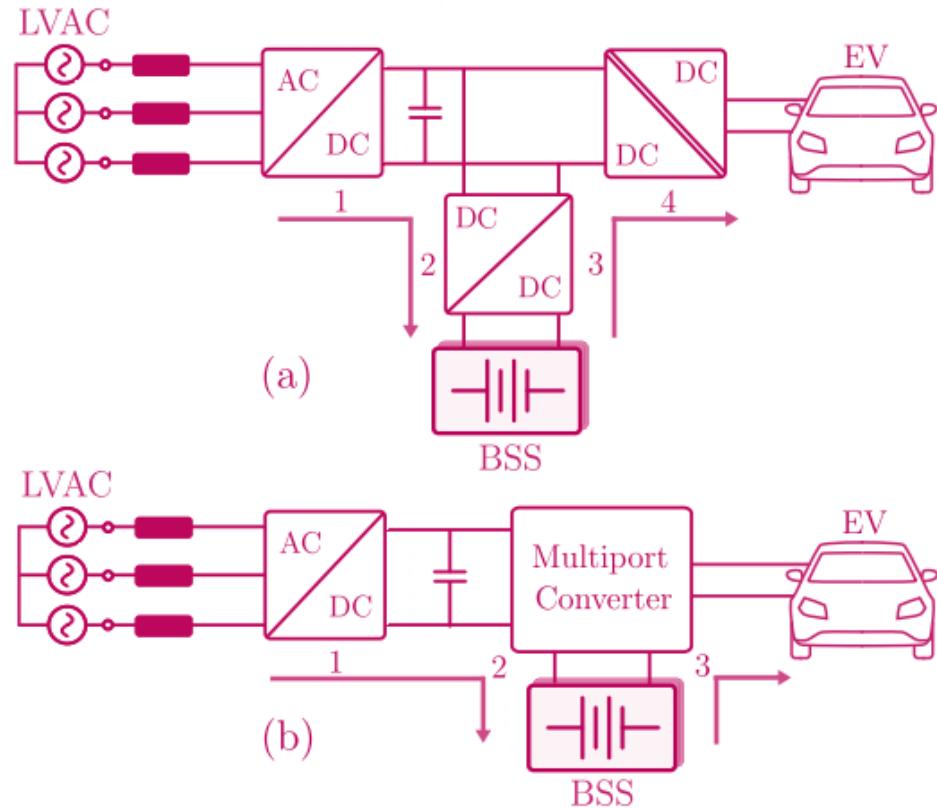


MULTIPORT CONVERTER

- Integration of battery storage systems (BSS) is becoming of particular interest because of the **peak power reduction** during the charging process.

MPC features:

- Reduces the number of conversions,
- High conversion efficiency and
- High power density.
- State-of-the-art PPC architectures that **two-port applications are the primary** emphasis of present PPC technology.
- Work to be done on the PPC approach's application to multiport networks.

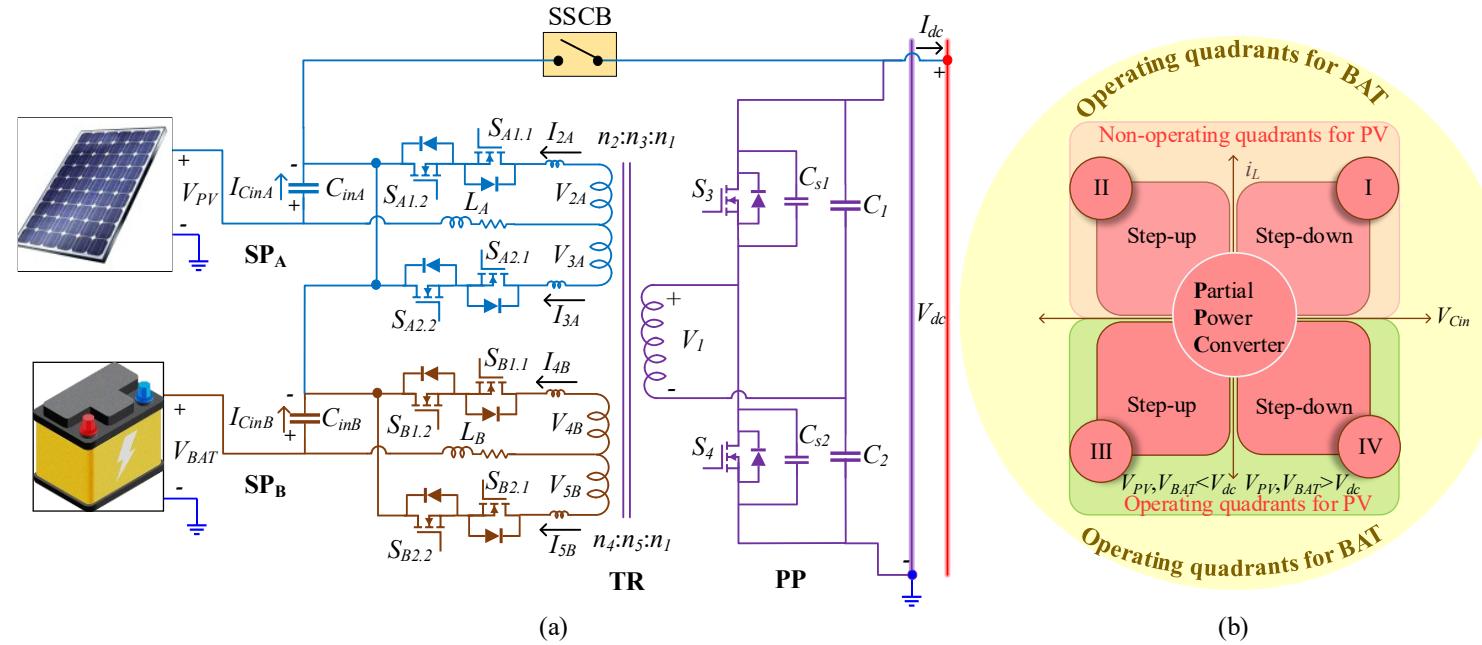


(a) BSS integration in DC link, (b) BSS integration with multiport converter

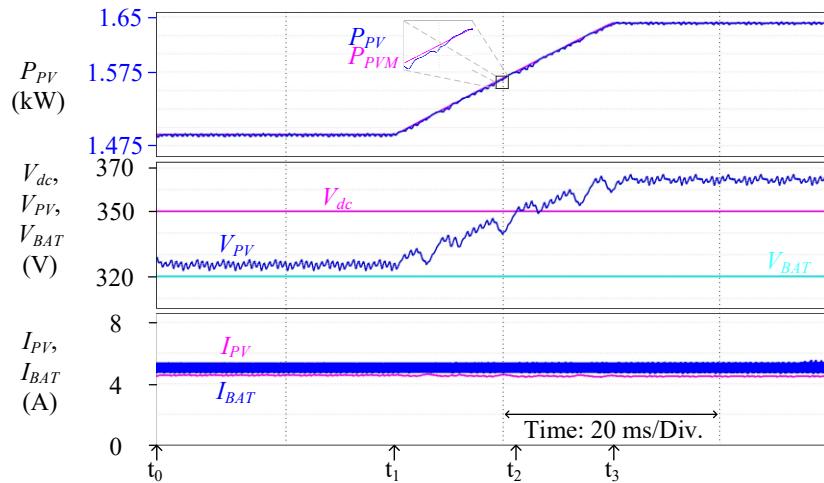
DUAL-INPUT SINGLE OUTPUT MULTIPORT CONFIGURATION

Main features

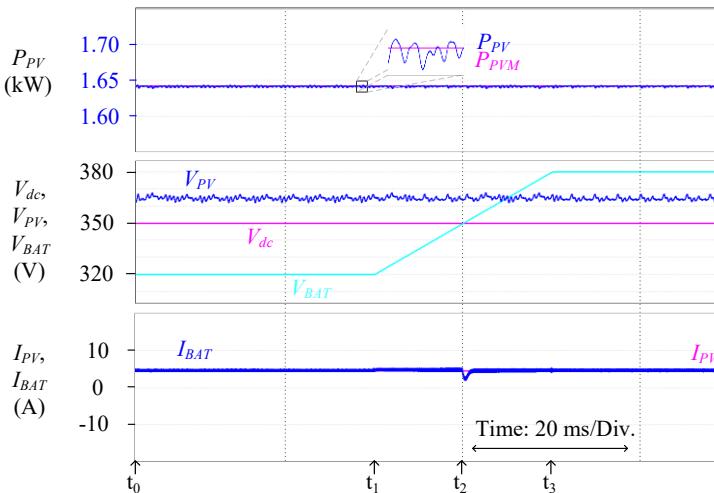
- Utilizes a soft-switching **current-fed push-pull** topology, which **reduces the number of switches** and the implementation cost.
- Fully decoupled control loops
- Wide voltage** regulation range with min. partiality
- A **short resonant state** is introduced into the modulation to enable complete soft switching and **reduce switching losses**.
- Embedded protection enables soft start-up and safe operation of the system



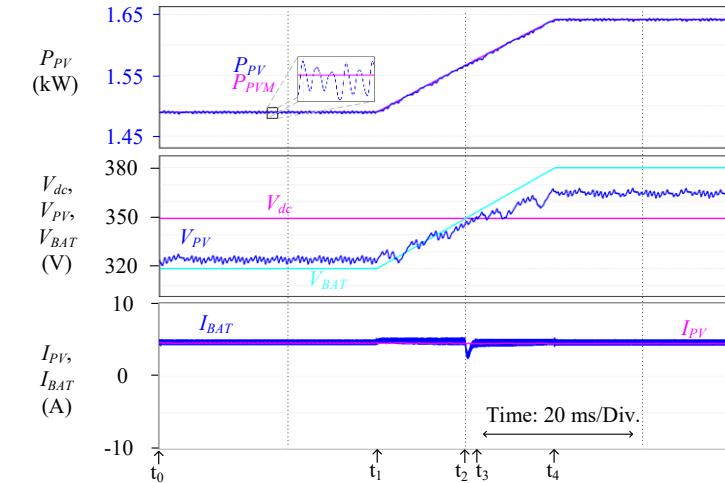
DUAL-INPUT SINGLE OUTPUT MULTIPORT: RESULTS



PPC performance for varying V_{PV} (325 to 365 V) while keeping constant $V_{BAT} = 320$ V and $V_{dc} = 350$ V.

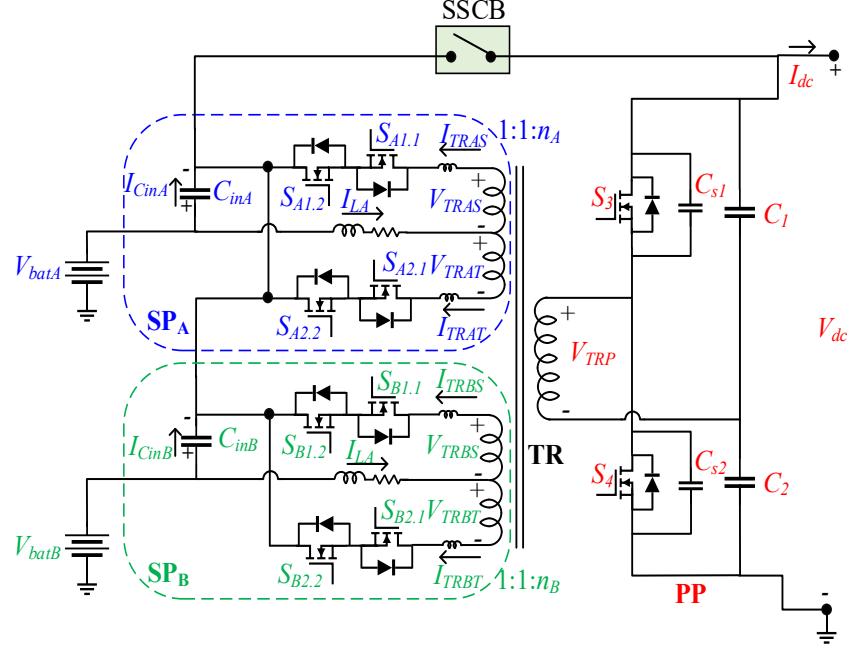


PPC performance for varying V_{BAT} (320 to 380 V) while keeping constant $V_{PV} = 365$ V and $V_{dc} = 350$ V.

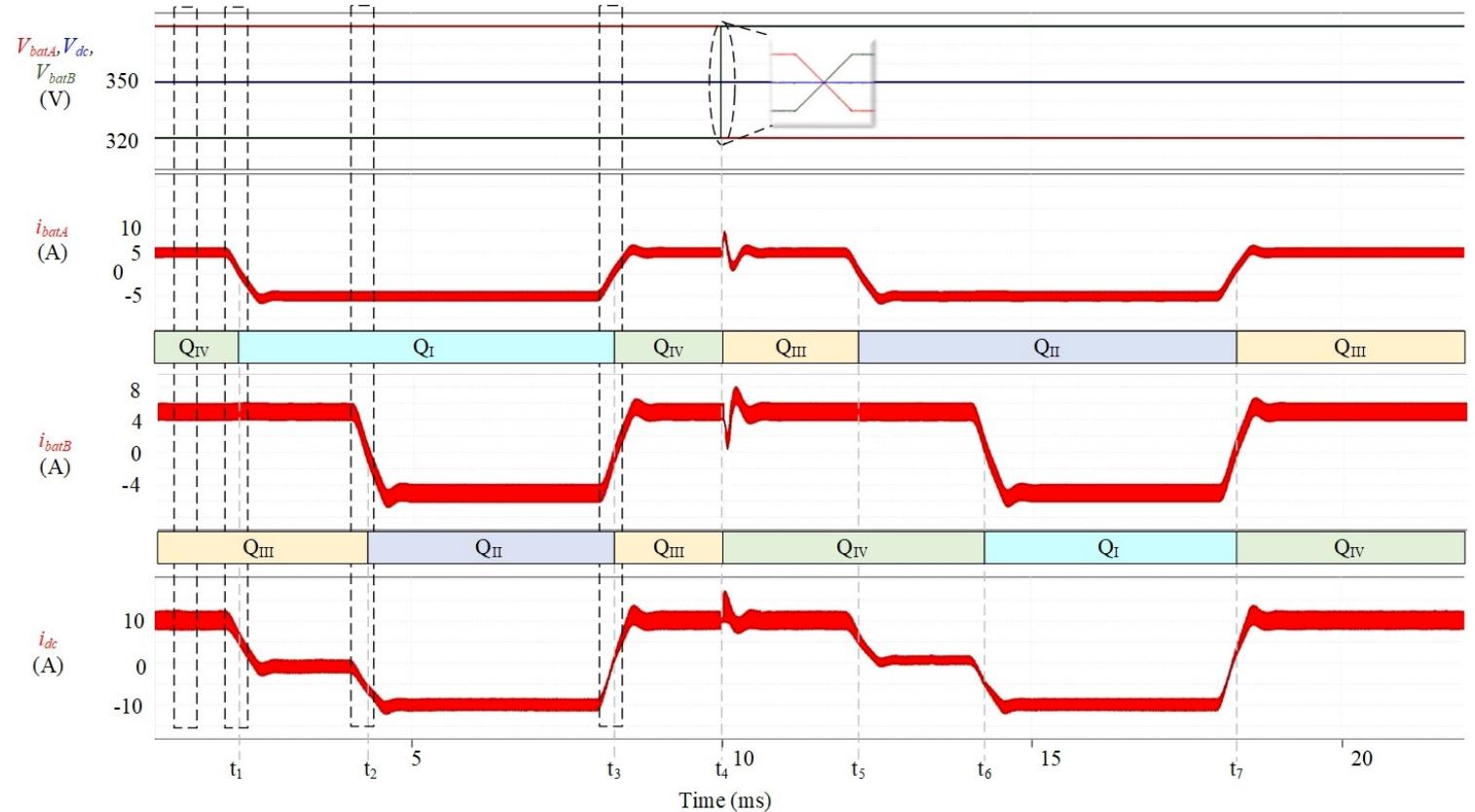


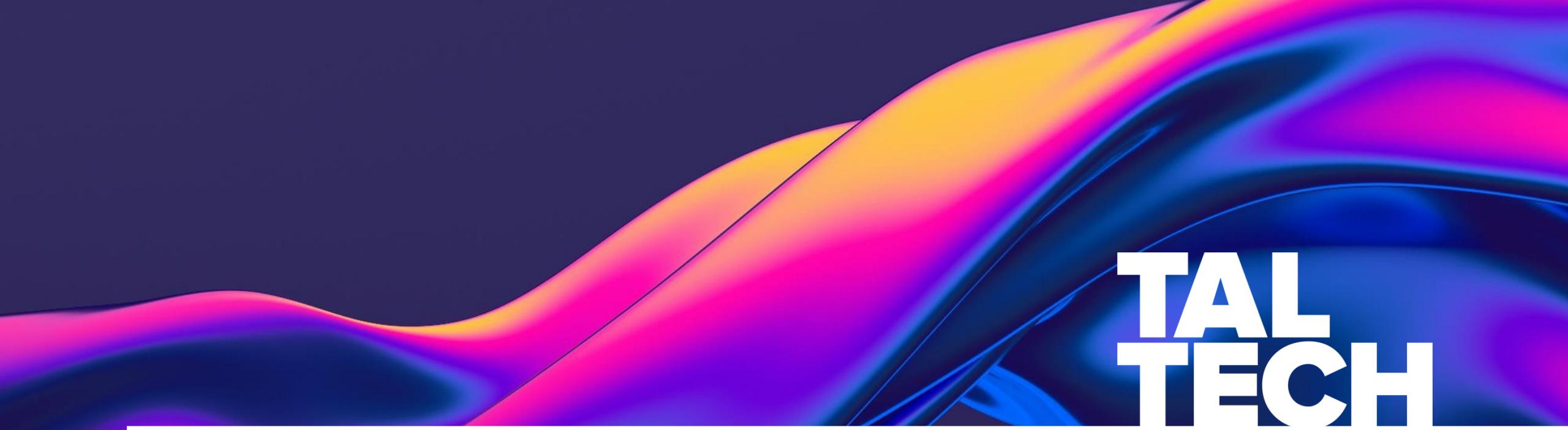
PPC performance for varying V_{PV} (325 to 365 V) and varying V_{BAT} (320 to 380 V) while keeping constant $V_{dc} = 350$ V.

FOUR QUADRANT OPERATION OF MULTIPORT PPC



Multiport partial power converter structure





TAL TECH

THE ROLE OF PPC IN INTEGRATING ELECTRIC VEHICLE AND DC BUILDING TECHNOLOGIES

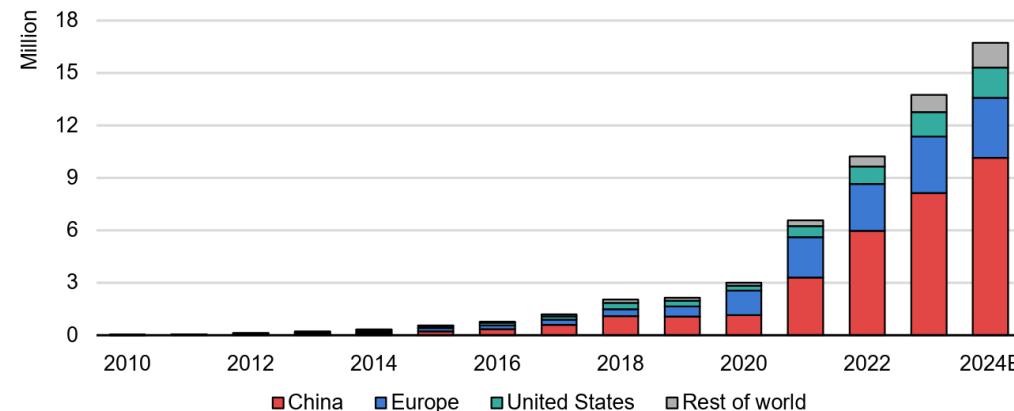
Dr. Niwton Gabriel Feliciani dos Santos



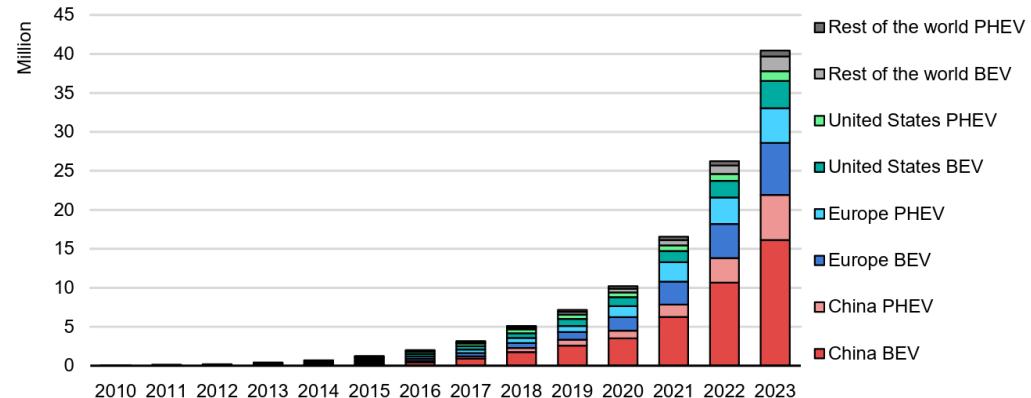
TRENDS IN ELECTRIC VEHICLES (EVs)

- EVs continue to make progress toward becoming a **mass-market product** in an increasing number of countries.
- In **2023**, most sales occurred in **China (60%)**, **Europe (25%)**, and the **United States (10%)**.
- In **India**, EVs hold a **2% market share**, supported by government incentives and domestic manufacturing efforts.
- In **Brazil (3% share)**, the adoption of EVs is being driven by the availability of cheaper models, primarily from **Chinese brands**.

Electric car sales, 2010-2024

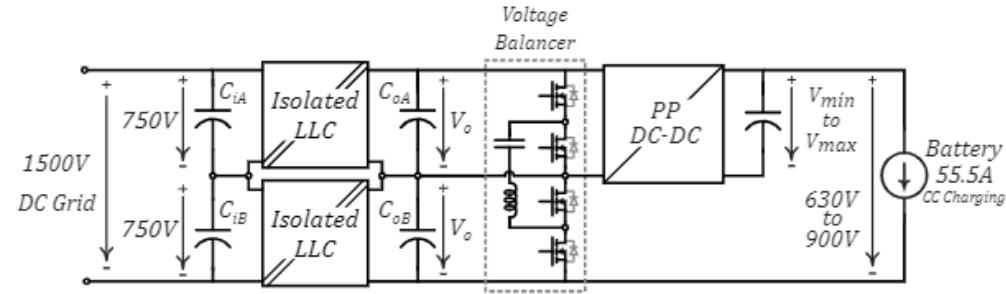


Global electric car stock trends, 2010-2023



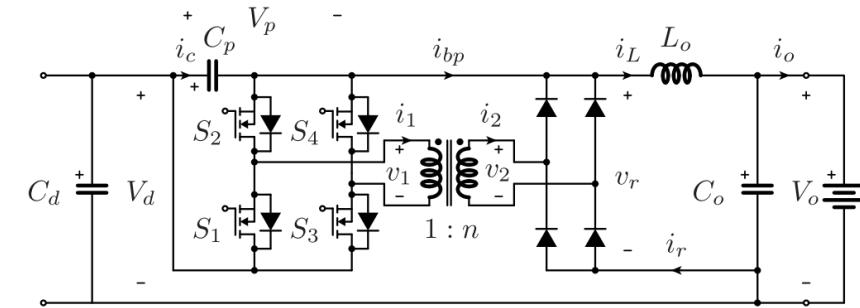
SOLUTIONS FOR EVS

Two-stage PPC for fast charging



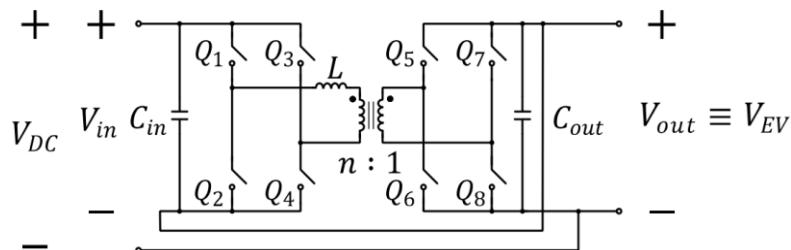
A. Stanojević, Y. E. Bouvier, and P. J. Grbović, "Comparison of 2-stage isolated converters for fast EV charger, using partial power," in *Proc. IECON 2022 – 48th Annu. Conf. IEEE Ind. Electron. Soc.*, Brussels, Belgium, 2022.

Type II S-PPC for fast charging



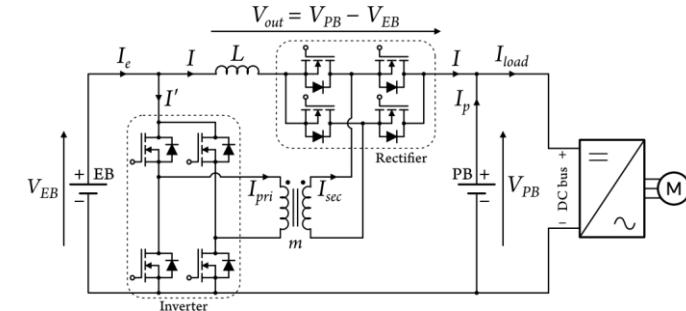
S. Rivera et al., "Partial-power converter topology of type II for efficient electric vehicle fast charging," *IEEE J. Emerg. Sel. Topics Power Electron.*, vol. 10, no. 6, pp. 7839–7848, Dec. 2022.

DAB-PPC for an on-board charger



J. Anzola, S. Sharma, I. Aizpuru, S. Bhattacharya, and J. S. Artal-Sevil, "Performance improvement of a silicon partial power converter over a silicon carbide full power converter," *IEEE Trans. Transp. Electricif.*, vol. 10, no. 1, pp. 1680–1691, Mar. 2024.

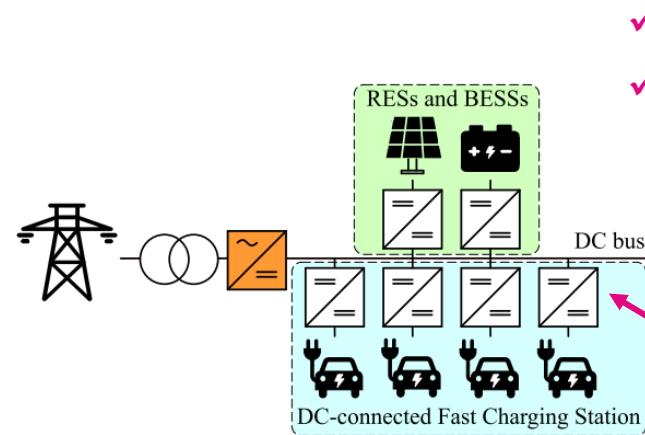
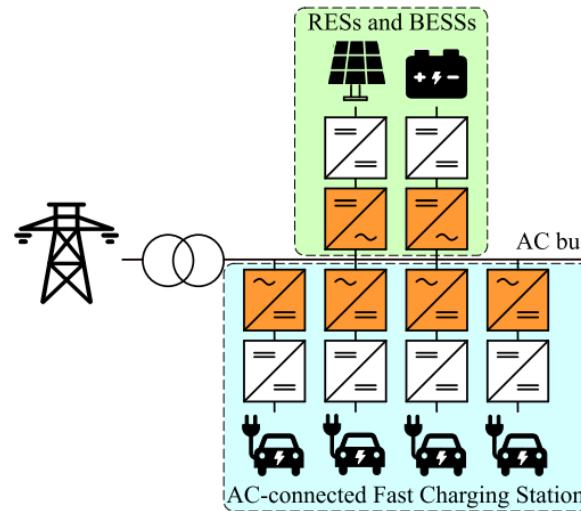
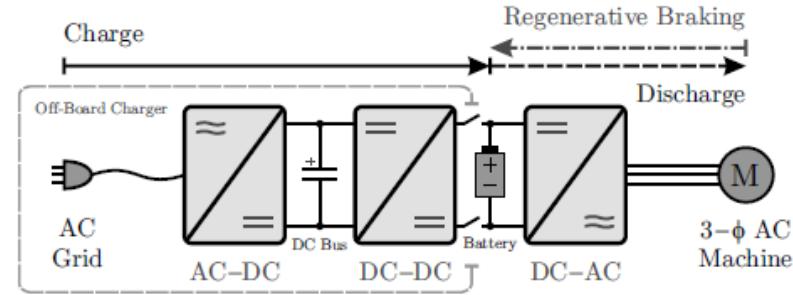
PISO S-PPC for HESS and EV traction



C. A. F. de Freitas, P. Bartholomeus, X. Margueron, and P. Le Moigne, "Partial power converter for electric vehicle hybrid energy storage system using a controlled current source cascade architecture," *IEEE Access*, vol. 12, pp. 150898–150913, 2024.

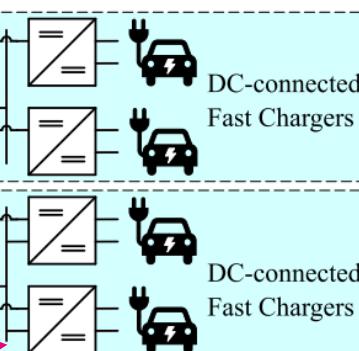
EVS AND DC BUILDINGS INTEGRATION

- Ideas for **Smarter Energy Use**:
 - AC-connected fast charging stations (FCSs)** are still more common.
 - DC-connected FCSs** are on track to become the main **fast-charging** solution in the growing world of **DC-powered buildings**.



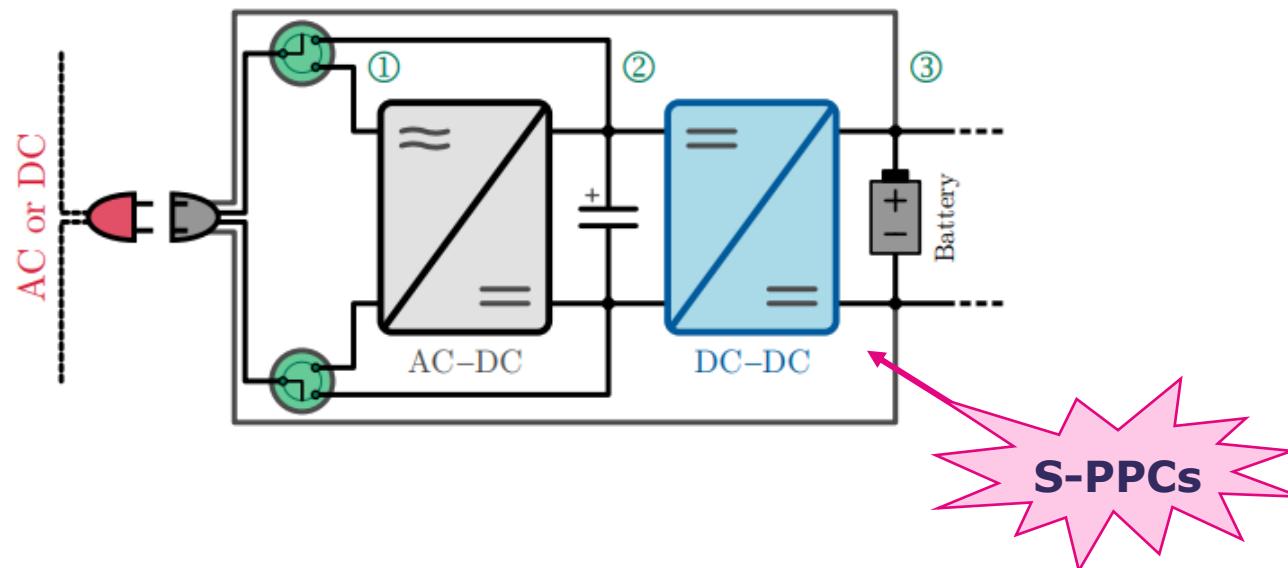
✓ Increased efficiency
✓ Lower number of converters

S-PPCs



EVS AND DC BUILDINGS INTEGRATION

- Ideas for **Smarter Energy Use**:
 - For the **on-board chargers (OBCs)**, one idea is to allow switching between **slow AC charging** and integration with **DC buildings**, without needing an external converter.



- ① Slow charging from the ac grid (OBC)
- ② Integration with dc buildings (OBC)
- ③ Fast or semi-fast charging (FCS)

RECONFIGURABLE S-PPCs (OBC)

- Advanced Topologies for PPCs:

- Reconfigurable PPCs

- Achieve an optimal balance between power processing, performance, and voltage regulation range

- Step-up/down SIPO S-PPC

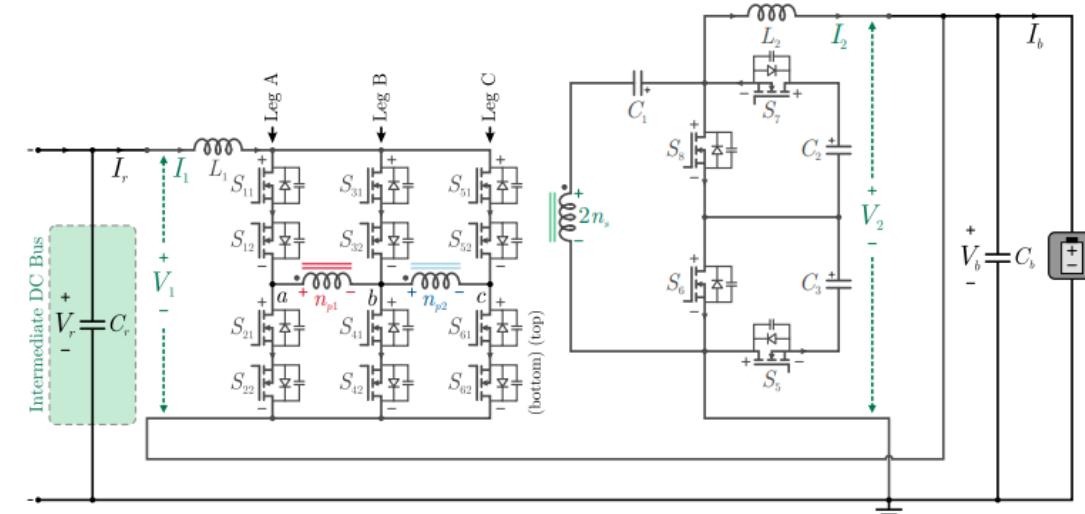
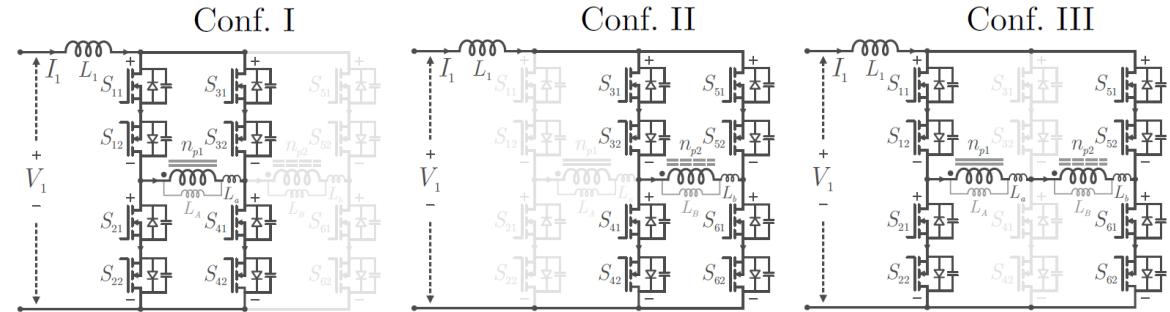
- Adjustable transformer turns ratio

- PWM strategies (fixed-frequency)

- Full-range soft-switching

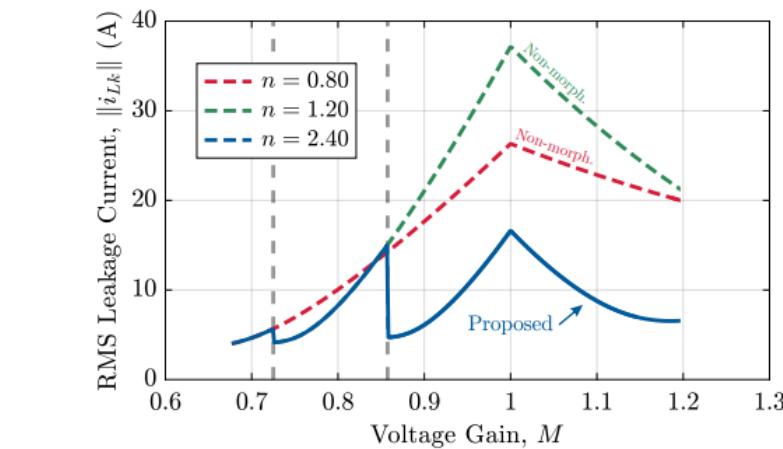
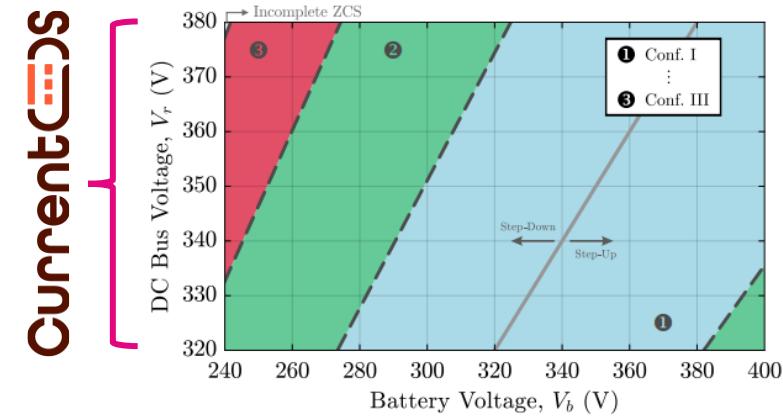
- Bidirectional** current-fed (CF) ports

- Snubberless **without** voltage spikes



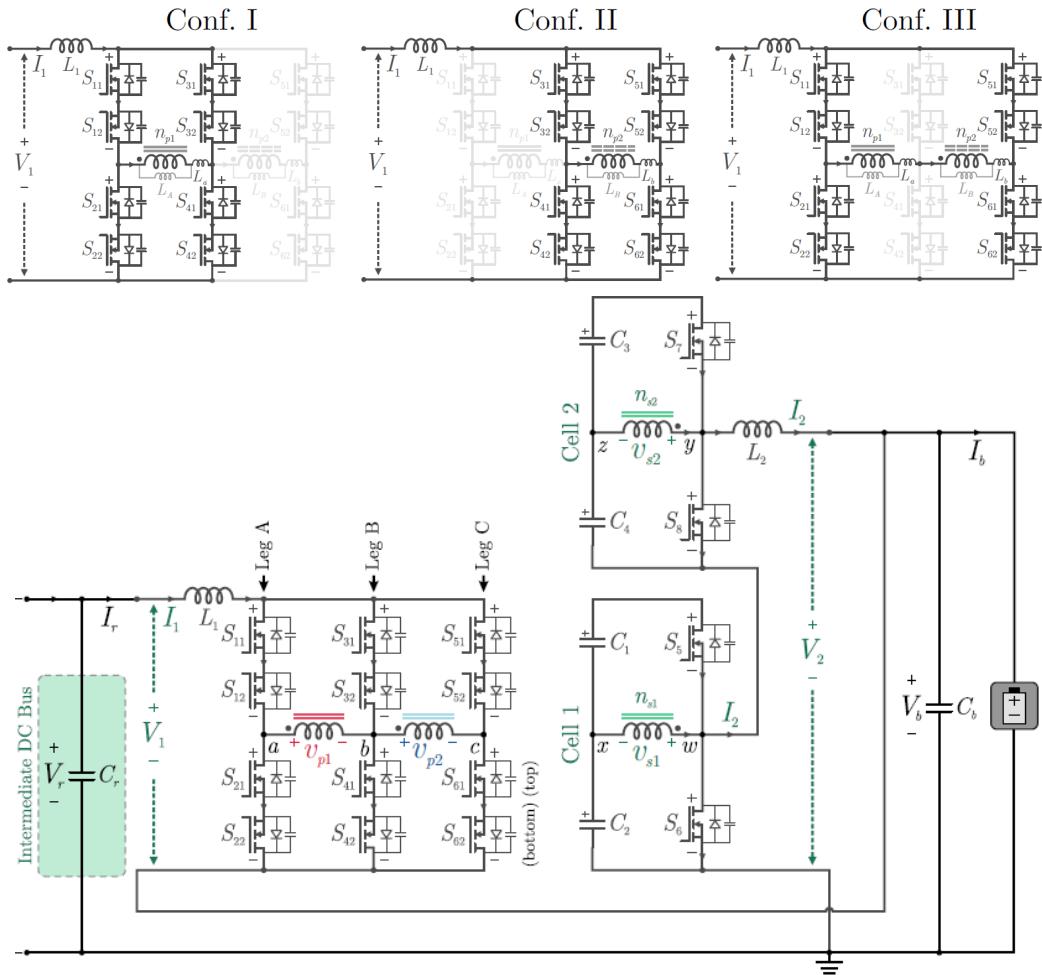
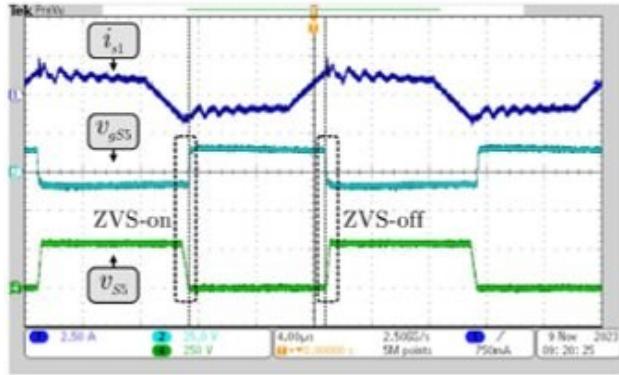
RECONFIGURABLE S-PPCs (OBC)

- **Advanced Topologies** for PPCs:
 - Reconfigurable PPCs
 - Achieve an optimal balance between power processing, performance, and voltage regulation range
 - The **soft-switching** absorbs all the energy stored in the **leakage inductance**
 - The **S-PPC** operates predominantly within a range where the **turns ratio is higher (Conf. I)**, which reduces conduction losses by minimizing the circulating currents



RECONFIGURABLE S-PPCs (OBC)

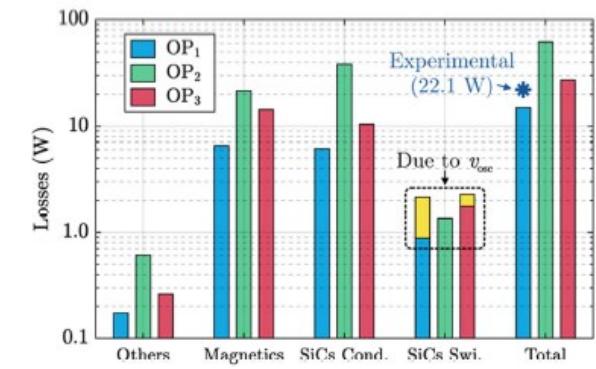
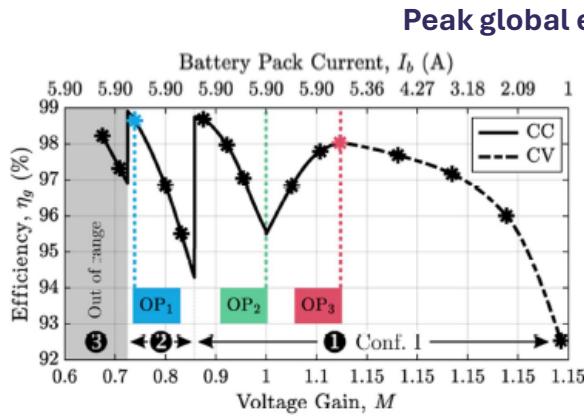
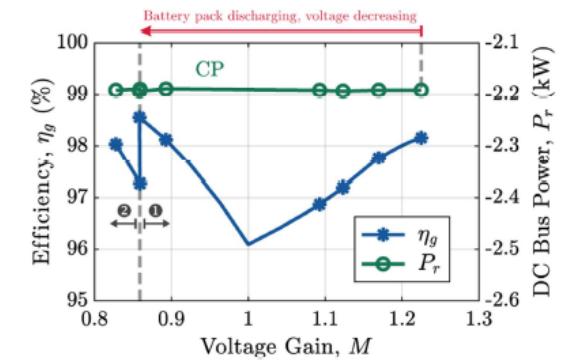
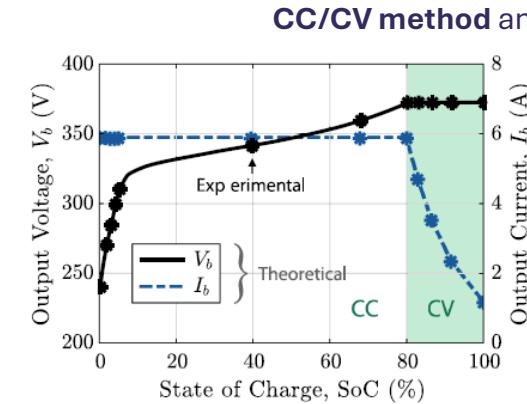
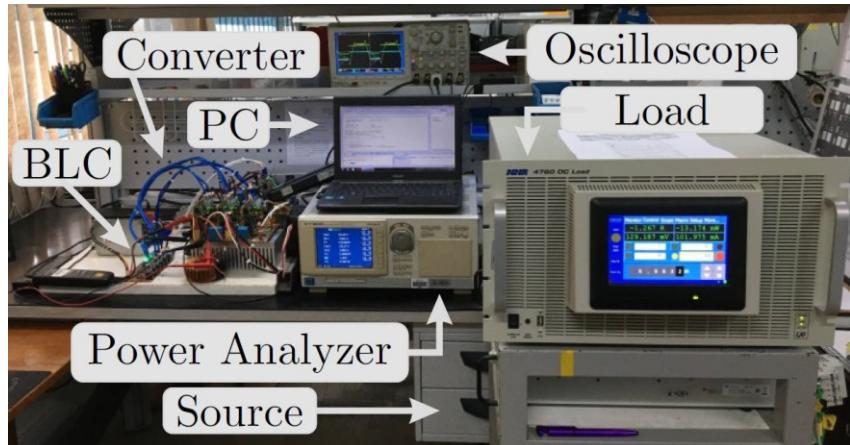
- Advanced Topologies for PPCs:
 - Reconfigurable PPCs: **Option 2**
 - Wide voltage regulation range
 - Adjustable transformer turns ratio
 - **Bidirectional** current-fed (CF) ports
 - **LC** resonance



N. G. F. dos Santos, J. R. R. Zientarski, and M. L. S. Martins, "A ZCS/ZVS DC-DC partial power converter with reconfigurable H-bridge and variable turns ratio for an integrated on-board charger," *IEEE Trans. Power Electron.*, vol. 39, no. 10, pp. 13916–13933, Oct. 2024.

RECONFIGURABLE S-PPCs

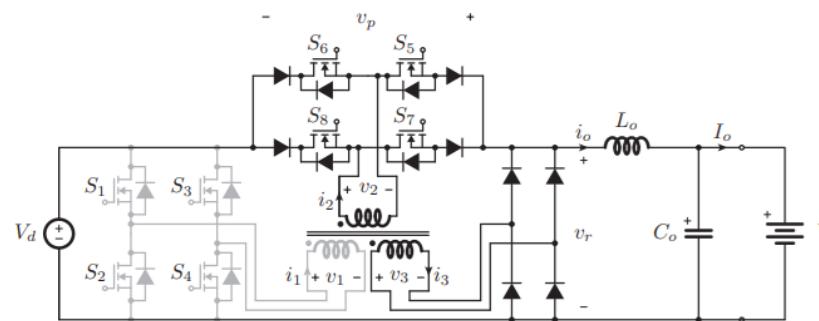
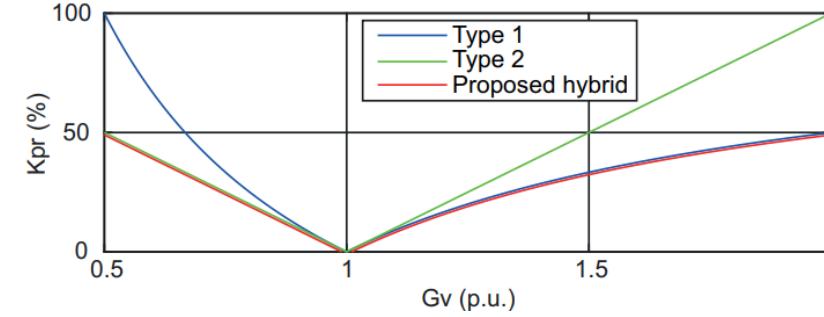
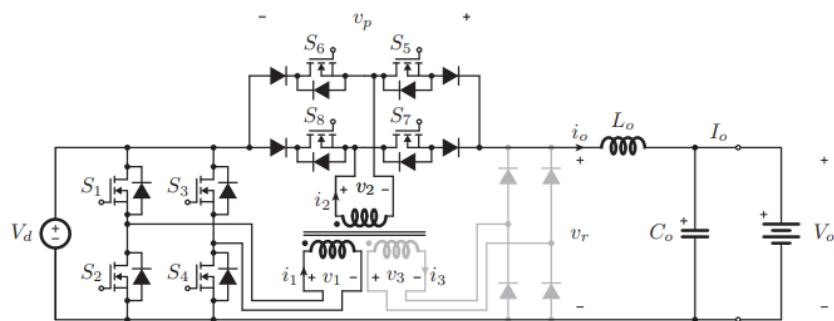
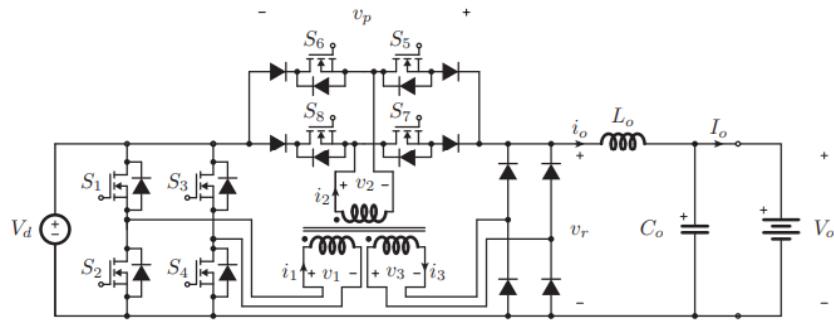
- Advanced Topologies for PPCs:
 - Reconfigurable PPCs: **Option 2**
 - Optimized turns ratio** ensures a good compromise between power processing, efficiency, and voltage range (**LEAF®**).



RECONFIGURABLE S-PPCs (FAST CHARGING)

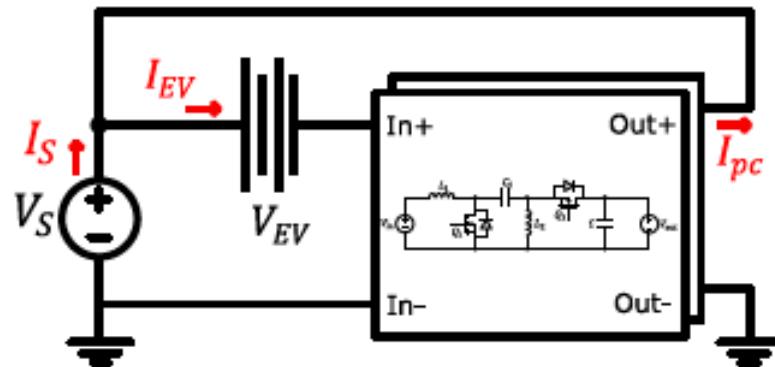
- Advanced Topologies for PPCs:

- Reconfigurable PPCs: The S-PPC can be reconfigured as **Type I** or **Type II**.



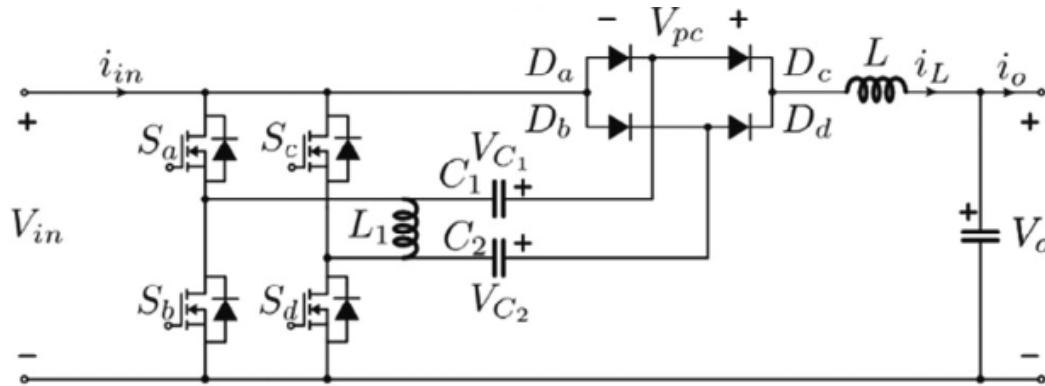
TRANSFORMERLESS S-PPCs (FAST CHARGING)

- **Advanced Topologies for PPCs:**
 - Transformerless PPCs: The idea is to **avoid transformers** due to their **losses, size, cost, slow response, and EMI issues**.



SIPO S-PPC:

Non-isolated DC-DC converter with a non-grounded battery pack [1].



PISO S-PPC

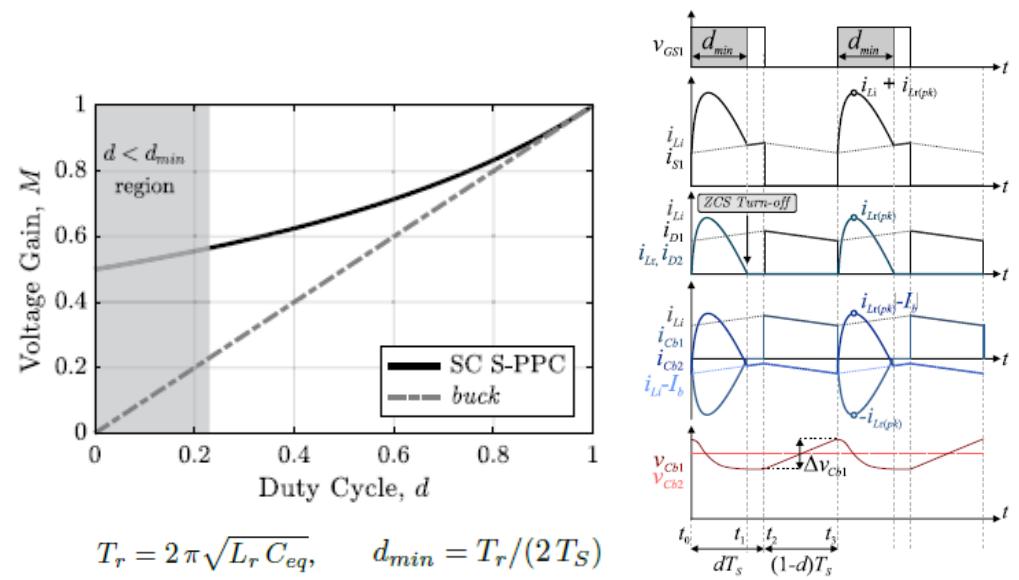
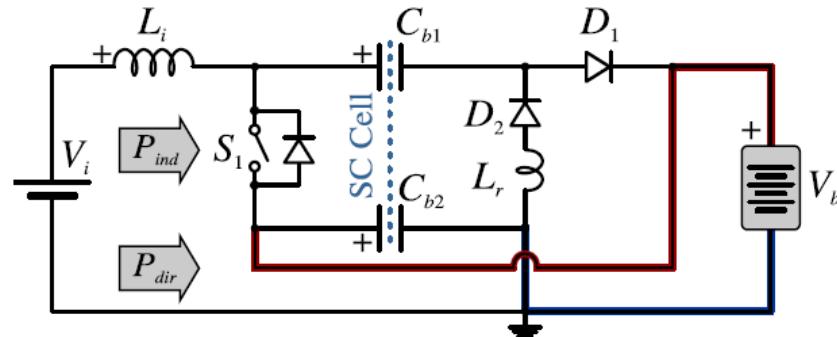
Capacitively isolated DC–DC converter with a grounded battery pack [2].

[1] J. Anzola, I. Aizpuru, and A. Arruti, "Non-isolated partial power converter for electric vehicle fast charging stations," in *Proc. 2020 IEEE 11th Int. Symp. Power Electron. Distrib. Gener. Syst. (PEDG)*, Dubrovnik, Croatia, 2020.

[2] D. Pesantez, H. Renaudineau, S. Rivera, A. Peralta, A. M. Alcaide, and S. Kouro, "Transformerless partial power converter topology for electric vehicle fast charge," *IET Power Electron.*, vol. 17, pp. 970–982, 2024.

TRANSFORMERLESS S-PPCs (OBC)

- Advanced Topologies for PPCs:
 - Transformerless PPCs
 - ✓ Switched-capacitor (capacitive isolation)
 - ✓ Single-Switch step-down SIPO S-PPC
 - ✓ Only **three** operating stages
 - ✓ PWM strategy (fixed-frequency)
 - ✓ Nearly full-range ZCS-off for D_2
 - ✗ Unidirectional
 - ✗ LC resonance stage
 - ✗ **NO** turns ratio to minimize N



$$T_r = 2\pi\sqrt{L_r C_{eq}}, \quad d_{min} = T_r/(2T_S)$$

TRANSFORMERLESS S-PPCs

■ Advanced Topologies for PPCs:

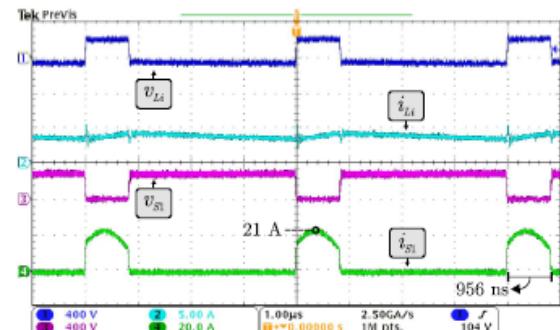
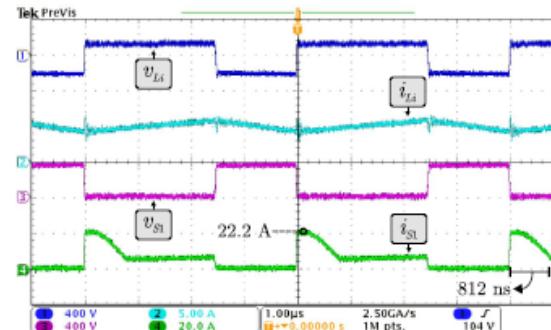
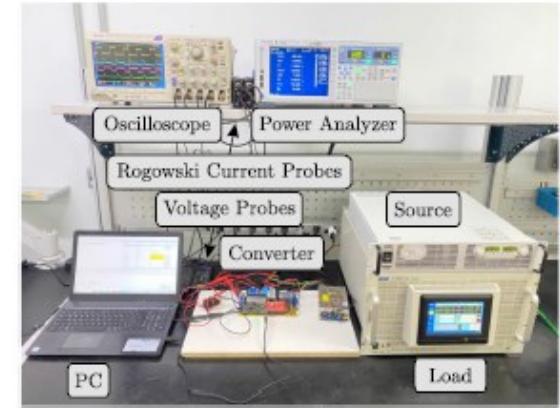
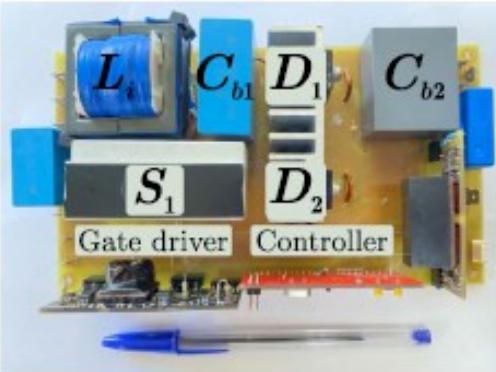
- Transformerless PPCs
 - **Low complexity, losses, volume, and cost.**

Parameter	Part	Parameter	Part
Controller	TMS320F280037	P_b	up to 3 kW
V_i	450 V	V_b	250–400 V
f_S	250 kHz	L_i	220 μ H
L_i turns	27 (250×37 AWG)	L_i core	NEE-42/21/20
C_{b1}	1 μ F (1000 V) B32656A0105	C_{b2}	36 μ F (500 V) C4AQLLW5360A36K
S_1	UJ4C075023K4S 23 m Ω (750 V)	Diodes	FFSH2065A 1.5 V (650 V)
C_{eq}	973 nF	L_r *	95 nH \circ
d_{min}	$\approx 0.23^\circ$	d	0.2–0.875

* Comprises the inductance of both the printed circuit board (PCB) tracks and the circuit devices terminals in the loop.

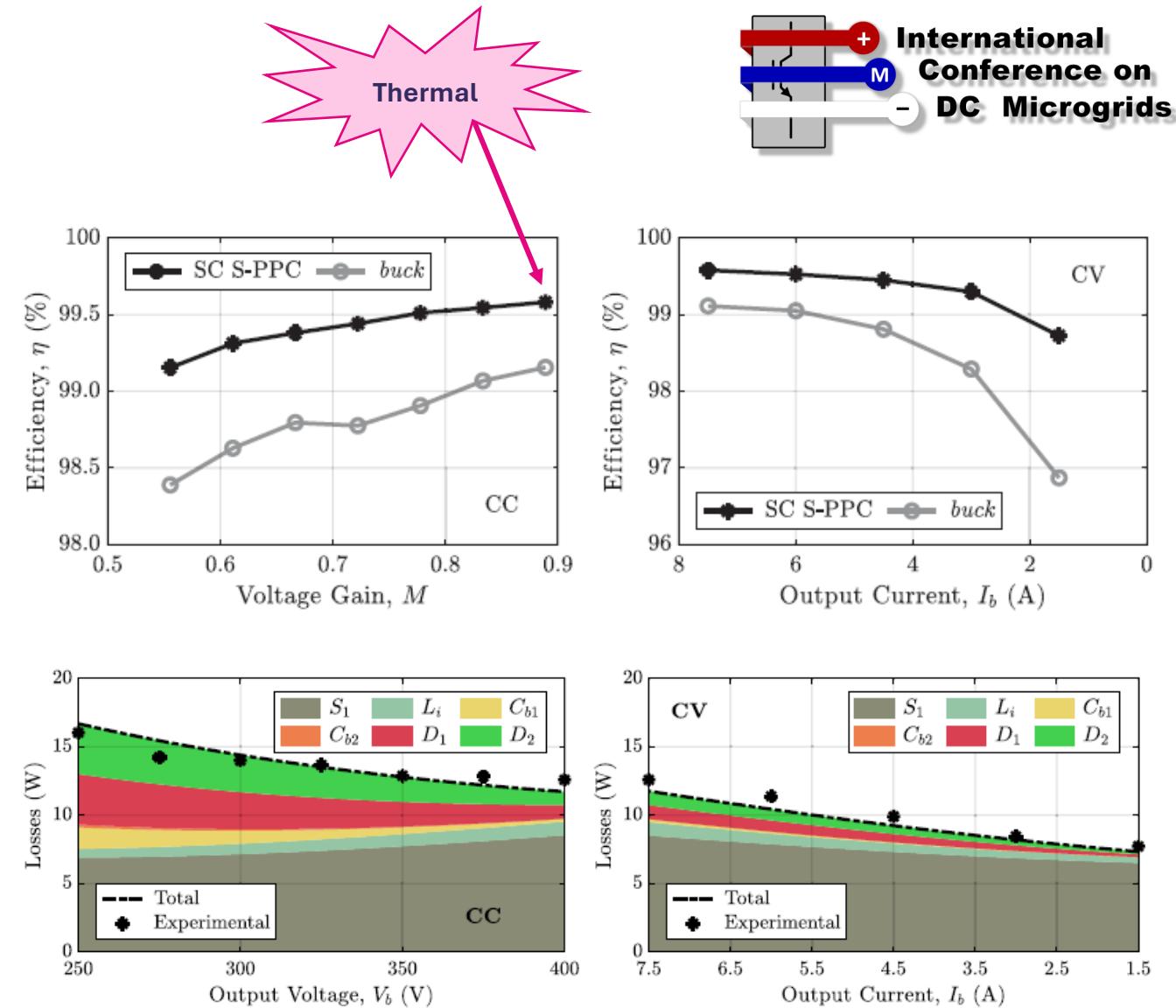
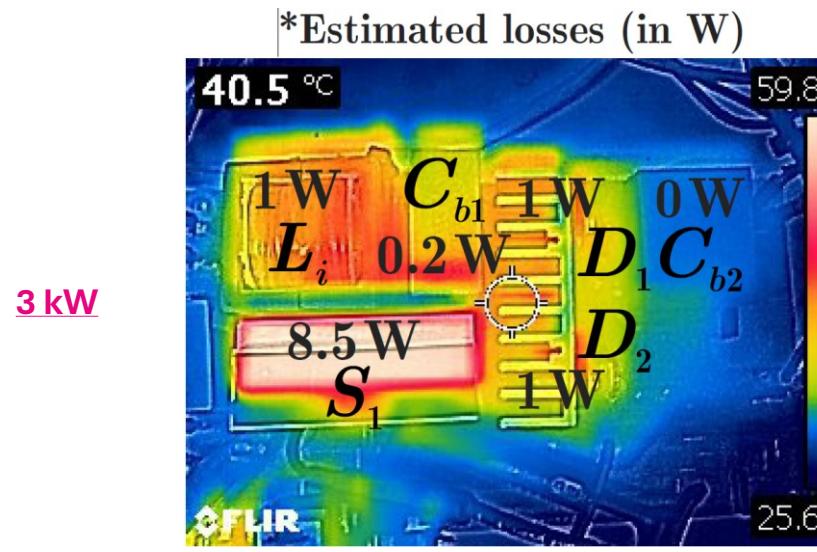
° Measured at 0% SoC, for $V_b = 250$ V and $I_b = 7.5$ A.

$$P_{ind} = \text{PPF} \times V_b \times I_b = 0.44 \times 250 \times 7.5 = 825 \text{ W},$$



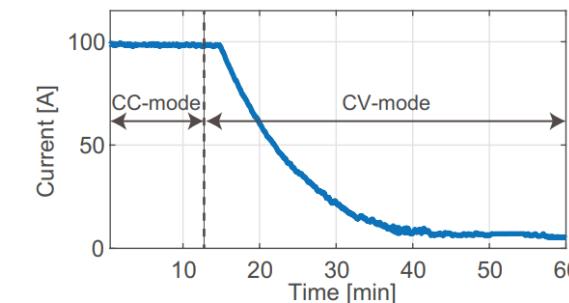
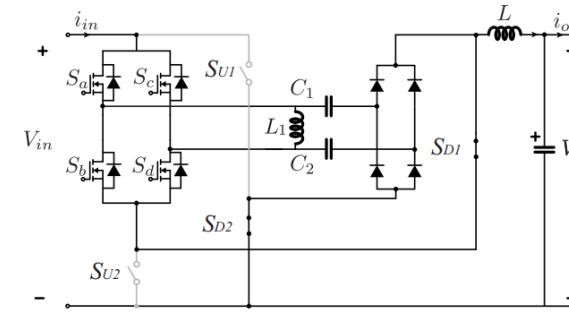
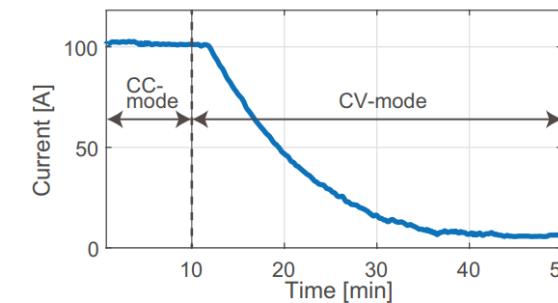
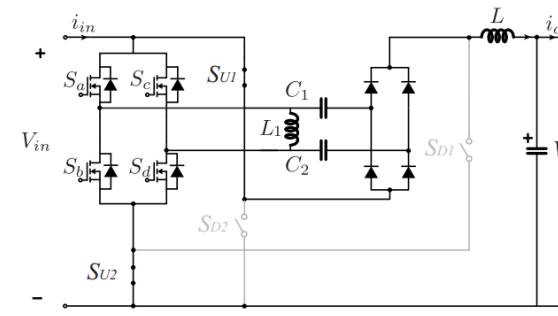
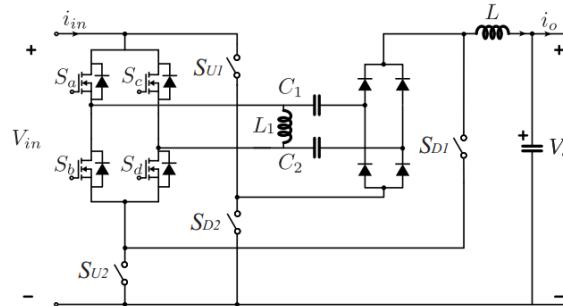
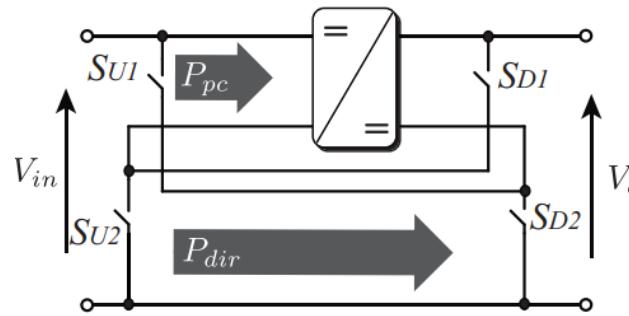
TRANSFORMERLESS S-PPCs

- Advanced Topologies for PPCs:
 - Transformerless PPCs
 - Minimum and maximum efficiencies around 98.7% and 99.6%.



TRANSFORMERLESS S-PPCs (FAST CHARGING)

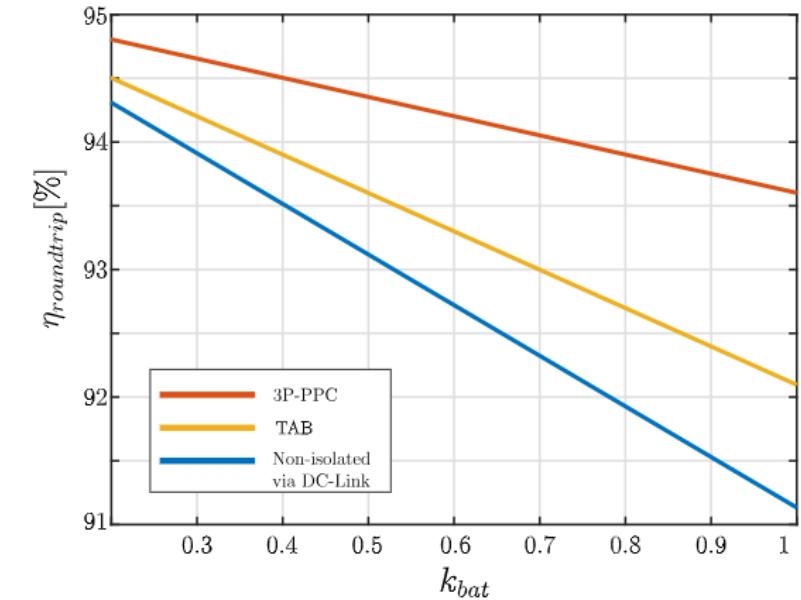
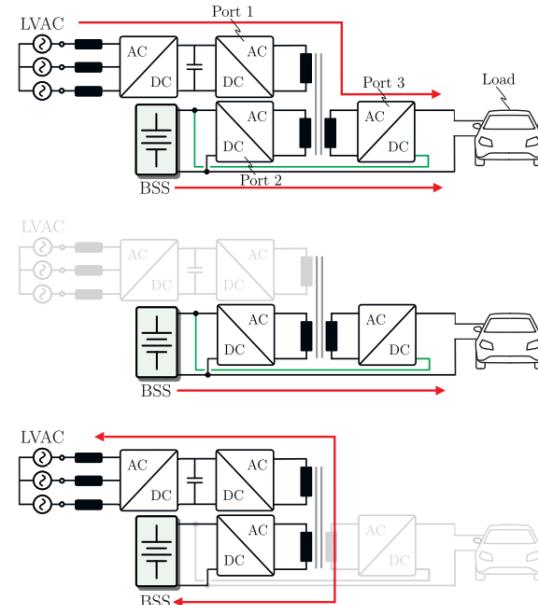
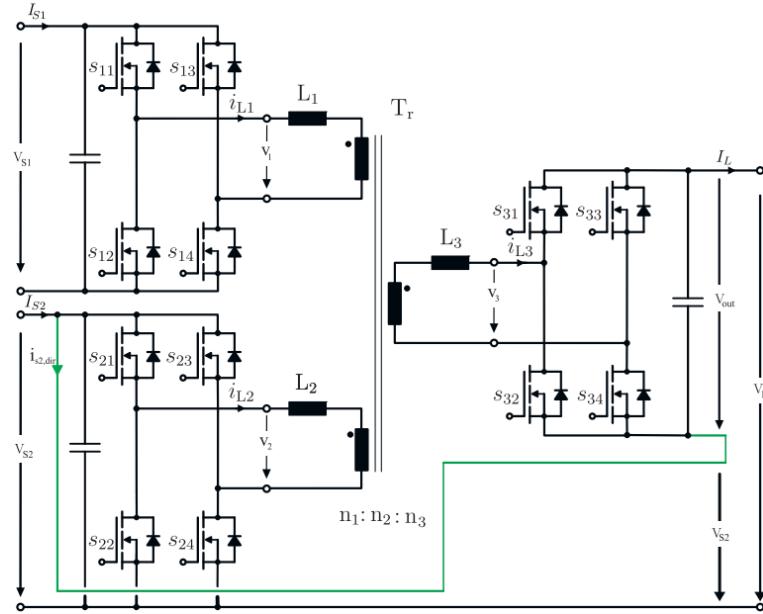
- Advanced Topologies for PPCs:
 - The transformerless S-PPC can be reconfigured as Type I or Type II.



ADVANCED TOPOLOGIES FOR FAST CHARGING

- Advanced Topologies for PPCs:

- Multi-Port PPCs: The architecture allows the **integration** of a **battery storage system** in **fast charging stations**, which can also be used for **DC buildings**.

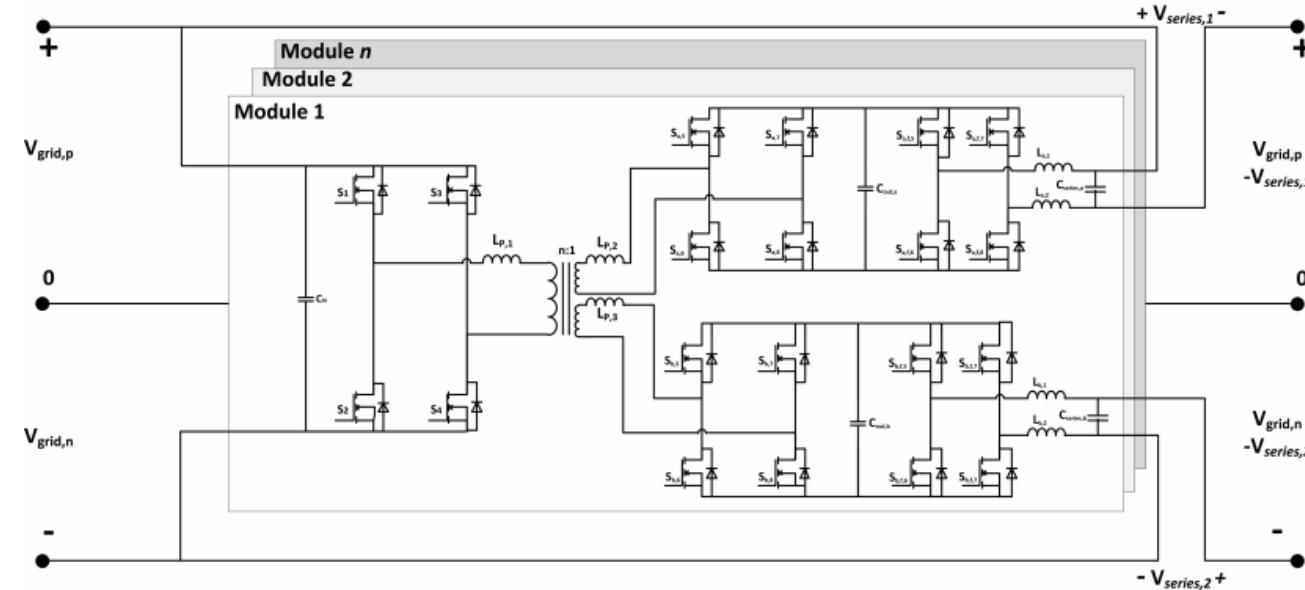


ADVANCED TOPOLOGIES

▪ **Emerging Features in PPCs: Moving forward with technology**

1. Bipolar DC distribution grid (concept)

- This concept can be used to implement a bipolar DC distribution grid using S-PPCs, enabling the **charging of either 400 V or 800 V EVs**.



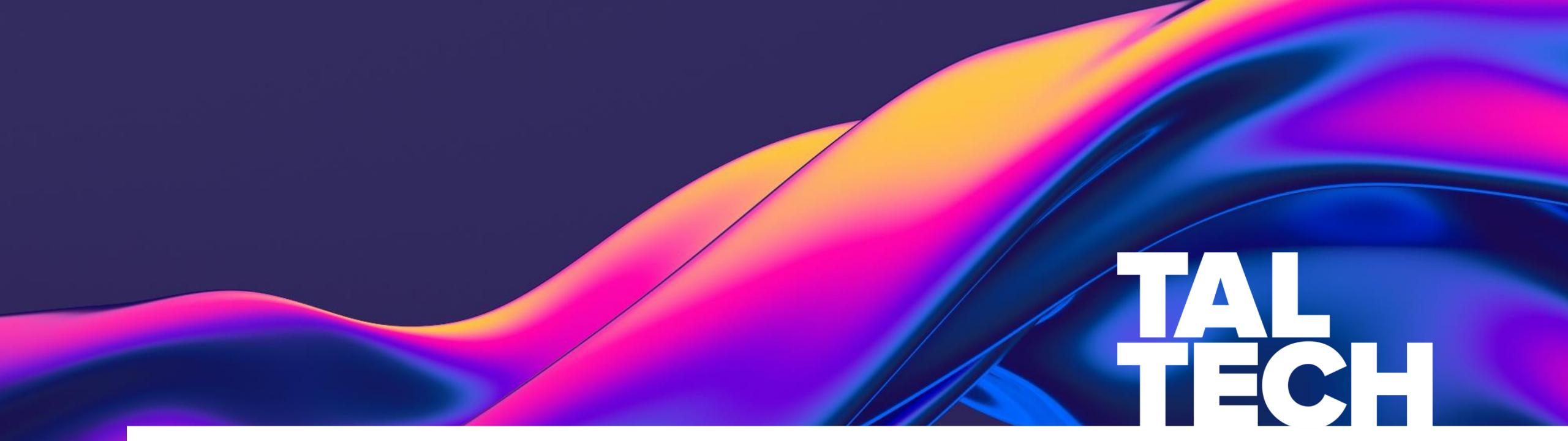
GENERAL REMARKS

- **AC-grid integration**
 - AC grid integration is still needed
 - AC-DC converter should provide services for both, AC and DC grids
 - Standardization is a challenge
- **Wide voltage range power converters**
 - Topology morphing control (TMC) based
 - Seamless integration with ELVDC applications
 - Full compatible with different types of DC grids (350/700 Vdc)
- **Breaking Limits with Partial Power Processing**
 - Higher efficiency for non-isolated applications (99.5%)
 - Applied for 2nd life battery
 - SC/OC Protection
- **Partial Power Processing for EVs Integration**
 - Emerging application for V2B
 - Easily integrated with DC buildings
 - Advanced topologies can cover a wide range of application



i³ DC
Accelerates Energy Transition





**TAL
TECH**

EMERGING POWER CONVERTERS TOPOLOGIES FOR DC BUILDINGS APPLICATION

Tutorial 3

